**Clark County Wind Tunnel Study** 

# Section II

Estimation of Valley-Wide PM<sub>10</sub> emissions using UNLV 1995 wind tunnel-derived emission factors, 1998-1999 emission factors, revised vacant land classifications, and GIS-based mapping of vacant lands

September 13, 2000 – Draft Final Report

#### CLARK COUNTY COMPREHENSIVE PLANNING

Estimation of Valley-Wide PM-10 emissions using UNLV 1995 wind tunnelderived emission factors, 1998-1999 emission factors, revised vacant land classifications, and GIS-based mapping of vacant lands

> David James, Ph.D., P.E. Johan Pulgarin Srinivas Pulugurtha, Ph.D. Sherrie Edwards, B.S., B.S. Jon Becker, B.S., M.S. Monte Park, B.S., M.S.

Civil and Environmental Engineering Department University of Nevada, Las Vegas 4505 Maryland Parkway Las Vegas NV 89154-4015

### **DRAFT Final Report DRAFT**

for

Clark County Department of Comprehensive Planning Clark County Government Center 500 S Grand Central Parkway Box 551741 Las Vegas NV 89155 - 1741

September 13, 2000

### **Executive Summary**

This final report addresses in detail several subject areas specifically requested by the client, Clark County Comprehensive Planning, as essential for proper documentation of the Valley-wide PM-10 vacant land estimate that is part of the Clark County's PM-10 State Implementation Plan (SIP) submission to US EPA. It is understood that this report, will be an Appendix in the SIP.

- I. The methodology used for developing the estimate of 151,189 acres of vacant land within the BLM Land Disposal Boundary is discussed. The acreage is generated by processing a database comprised of Clark County Assessor's information, dated 11/29/99, about vacant land parcels larger than ½ acre that have a zero integer value for land use codes. The Assessor's database shows 148,575 acres vacant within the Land Disposal Boundary. The process of assigning the land to Thiessen polygons and dividing shared grid cells among polygons introduces a +2,624 acre (+1.8%) error into the vacant land estimate when it is ready to be used for PM-10 valley wide estimate.
- II. The rationale for selection of a 20 mph minimum wind-speed for initiation of a Valley-wide PM-10 erosion event is described and explained. The 20 mph threshold corresponds to the 10<sup>th</sup> percentile PM-10 threshold as determined from the 1995 UNLV wind tunnel field study database. Use of a 20 mph threshold is conservative, producing high estimates of PM-10 emissions, in that only a small percentage of Valley sites are likely to be eroding PM-10 at that velocity. The 50<sup>th</sup> %ile velocity is about 27 mph.
- III. PM-10 emissions factors, corrected for the presence of initial spikes of loose PM-10, are presented for unstable lands, stable lands, stabilized lands (with suppressant freshly applied – not torn up), and stabilized lands with degraded suppressant (torn up). Emission factor values for unstable and stable lands are similar to those reported in the February 22, 2000 Draft report. Stabilized land emission factors have been revised to incorporate the effects of initial PM-10 spikes since the March 28 Draft report. This revision has a very small effect on the valley-wide emissions of PM-10 from a mixture of stable and stabilized (formerly unstable, but now treated with suppressant) lands.
- IV. Field survey data are presented demonstrating the feasibility of classifying vacant parcels as stable or unstable, based on the proposed Clark County rule 41. UNLV visited 69 sites, mostly in the south and west parts of the Valley, and found that 63 of 69 visited sites would be rated as "stable" under the proposed rule. If additional site visits to

the north and east of the Valley were made, it is anticipated that the relative number of unstable sites would increase. UNLV developed a flow-chart to ease application of the rule in the field, and proposed an improvement to the rule procedure for measuring rock cover by collecting with a dust pan, then squaring up in a single layer in a cake pan and measuring the squared area.

V. UNLV analyzed 54 aerial orthophotos to determine standing shrubsized vegetative densities on vacant lands. The arithmetic mean vegetative density was 9.7%, geometric mean 4.6%. If these observed densities were to hold for larger areas, it appears that, in general, there is insufficient standing shrub-sized vegetation on most desert lands to attenuate wind stress and reduce wind erosion.

Keywords: PM-10, wind erosion, emissions factors, Valley-wide, dust suppressants, GIS, Clark County

### Acknowledgments

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The following UNLV faculty a	and staff contributed to this project.
Shashi Nambisan	Jon Becker
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	Monte Park
	Johan Pulgarin

Any errors and omissions are the sole responsibility of the author and Principal Investigator, David James

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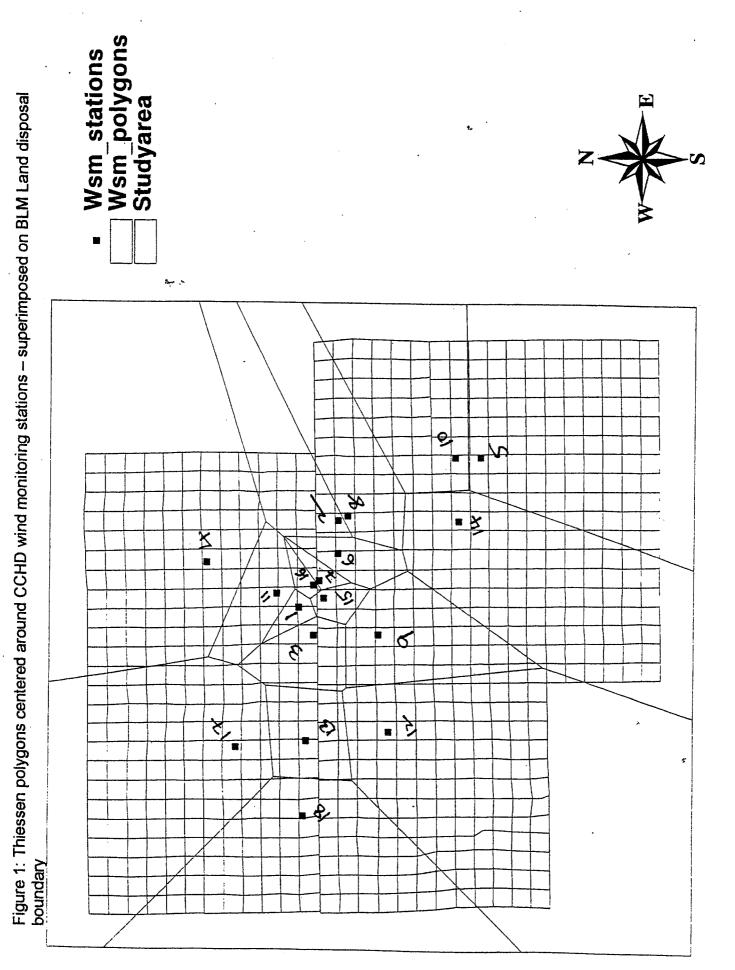
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#### I. Methodology For Computing The Number Of Acres Of Vacant Land Used In The Valley-Wide Estimate Of Wind-Eroded PM-10 Emissions.

- A. Vacant land estimates in each township, range and section were obtained by the following method (Khater, personal communication, Sept 2000)
  - 1. The Clark County Assessor's database, effective date, November 1999 was used to develop information about the number of acres of vacant land in each township, range and section.
  - 2. Queries were run on the database for parcels with any non-zero land use code. Land use codes are assigned integer values. For non-zero land use codes, the entire parcel corresponding to a nonzero code was assumed to be developed, or not vacant.
  - 3. A zero value in the land-use code indicates that the assessor is not aware of any development on the parcel, and the parcel was classified as vacant.
  - 4. This methodology of land use classification introduces some inaccuracies into vacant land estimates. For example, a non-zero code could be assigned to a 2.5-acre residential parcel. However, the parcel could have 0.5 acres that have been developed (with house, driveway and yard) and the remaining 2.0 acres would be undeveloped (vacant). The assessor's database will only change for this parcel if it is subdivided and sold.
  - 5. For a particular township, range and section, the total number of acres of parcels with non-zero land use codes was determined, and subtracted from the total area of the section to develop an estimate of the number of acres of vacant land in that section.
  - 6. On November 29, 1999, UNLV obtained from Clark County Comprehensive Planning (via Rodney Langston), the output from a query to this database to produce a summary of the vacant land areas within the Bureau of Land Management (BLM) Land Disposal Boundary. The query produced a file containing records comprised of the following fields: township, range, section, and vacant land area (acres). The total vacant land area within the Land Disposal Boundary identified by this query was 148,575 acres. A listing of all grid cells identified by this query is displayed in Table B-1 in the Appendix.
- B. Locations of Clark County Health District (CCHD) Air Quality Division (AQD) monitoring stations were converted to UTM coordinates and overlaid on a Clark County grid comprised of the sections within the BLM Land Disposal Boundary (Figure 1).
- C. An ARCInfo® macro was written to create a set of Thiessen polygons using the CCHD AQD monitoring station locations as the origins. Straight lines were drawn to connect monitoring station locations.



. 2

Perpendicular bisectors were then drawn outward from the lines connecting the monitoring stations. The lines were extended until they intersected another perpendicular bisector, then stopped. These perpendicular bisectors comprise the boundaries of the Thiessen polygons. Bisectors that extended to the BLM boundary stop at the BLM boundary. These Thiessen polygons became a layer in the ARCInfo® Geographic Information Systems (GIS) database.

- D. A database query was developed and run to find all grid cells (sections) touched or contained by each Thiessen polygon. The total vacant land area associated with each Thiessen polygon was then computed by summing the vacant land areas for all grid cells touched by or contained within each Thiessen polygon.
- E. The method described in step D leads to vacant land areas in grid cells straddling a Thiessen polygon boundary being counted on each side of the boundary. As a result of this "double-counting," vacant land areas associated with each polygon would be overestimated if the "double-counting" were not corrected. Because of the duplication of grid cells, total vacant land area associated with the Thiessen polygons, prior to correction, was 183,345 acres. A listing of all grid cells associated with each polygon is contained in Table B-2 in the Appendix.
- F. The following technique was developed to correct the double-counting error.
  - 1. A Microsoft Access97<sup>®</sup> database was developed by UNLV's Srinivas Pulugurtha that labeled each township, range and section with a unique record identifier.
  - 2. After assignment of grid cells to the Thiessen polygons, and entry of this information into the database. A query was run to find all records that contained duplicates of the unique identifier. Duplicate records indicated grid cells that were associated with more than one polygon.
  - 3. It was assumed that all duplicate grid cells associated with each polygon, were, on average, half in the polygon, and half out of the polygon. Vacant land areas for duplicated cells associated with each polygon were summed, divided by two and subtracted from the original total vacant area computed for the polygon to obtain a corrected vacant land area estimate. A hypothetical example might clarify this technique.
- G. Hypothetical example, with rounded numbers:
  - 1. Thiessen Polygons A and B are generated from the ARCInfo macro. All grid cells touched by or contained in Polygon A have a total of 5,000 acres of vacant land. All grid cells touched by or contained in

Polygon B, which is adjacent to Polygon A, have a total of 8,000 acres of vacant land.

- 2. A find duplicates query shows that there are 10 grid cells associated with the polygon that are duplicated (associated with other polygons). The 10 grid cells have a total of 500 acres of vacant land.
- 3. It is assumed that these bordering grid cells lie half in Polygon A and half in other polygons. So, the 500 acre total is divided by 2, and subtracted from the total for A. Polygon A's corrected vacant land area is then 5000 250 = 4750 acres.
- H. This correction process is repeated for all polygons that have duplicated grid cells.
- I. Corrected vacant land areas for were summed over all Thiessen polygons to generate the total area of vacant land to be used in computing the Valley-wide estimate. The total value, after correction, generated for use in the vacant land PM-10 calculations is 151,189 acres. A tabular summary of the corrected land areas for each polygon is shown in Table 1. A listing of duplicated grid cells for each polygon may be found in Table B-3 in the Appendix.
- J. This total area, because of a correction process that assumes half the area in each polygon, is 2,624 acres (1.8%) higher than the raw area data provided by Clark County from the Assessor's database.
- K. Summary discussion of Sources of Error in determination of the number of acres of vacant land
  - 1. Development of vacant land estimates in each section from Clark County Assessor's land use codes. As previously discussed, this technique tends to over-estimate the number of acres of developed land at parcel scale, because it does not have information about the amount of development within each parcel. As a result, it tends to underestimate the number of acres of vacant land in each section.
  - 2. Development of number of acres of vacant land in each polygon. Error is introduced in the assumption that all grid cells straddling a polygon boundary are equally shared between the two adjacent polygons. This assumption may be approximately correct for large polygons containing lots of cells, but may be less accurate for polygons that contain only a few grid cells. The outcome of processing the grid cell data in this manner to prepare it for use in the PM-10 emissions estimate, introduced a 1.8% overestimate of in the number acres of vacant land used in the PM-10 vacant land emissions estimates.

U.	id lettercode	latitetter code	vacant land (acres)	adjustment (acres)	vacant land (acres) adjustment (acres). Invivacant land (acres) bordening polygons comment	comment
-	SC		635	318	318 3,11,15,16	vacant land
3	ww		2,497	923	1,574 4,6,8,11	comprises
ო	sl		2,510	1,195	1,315 1,9,11,12,13,17	all grid cells
4	bs	cr	25,920	3,551	22,369 2,11,17	contained in
5	Ы	se	10,862	2,574	8,288 10,14	or touched by
စ	mc	es	722	301	422 2,7,8,9,14,15	the boundary
2	ms	ec	339	170	170 6,15,16	for each
ω	dm		3,276	1,084	2,192 2,6,10,14	polygon
0	A		11,574	3,742	7,833 3,6,12,14,15	
9	pt		8,544	1,781	6,764 5,8,14	adjustment
7	jd		5,365	2,250	3,116 1,2,3,4,16,17	is 1/2 the
12	pm		34,568	3,906	30,662 3,9,13,18	total area
13	wj		2,177	655	1,523 3,12,17,18	of grid cells
4	gv		30,558	4,538	26,021 5,6,8,9,10	that cross
15	СW		369	177	192 1,3,6,7,9,16	a boundary
10	Sa		414	207	207 1,7,11,15	
17	lo		28,958	2,857	26,102 3,4,11,13,18	rev vacant =
18 PV	p۷		14,057	1,932	12,125 12,13,17	vacant -
	Total		183,345	32,157	151,189	adjustment

Table 1: Summary of area corrections for shared grid cells in each polygon

Table 2:

Statistical summary - 10 meter threshold wind velocity distributions 

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	Disturbed sites (new cla	(new classification) $n = 29$		
		computed	extrapolated	
category	aero roughness (cm)	spike velocity @ 7.5 cm (mph) spike velocity @ 10 m (mph)	spike velocity @ 10 m (mph)	Comment
minimum	0.0027	9.6	18.2	
arithm. 10th %ile			19.9 inter	19.9 interpolated from plot
geom. mean-1 s.dev	0.0139	11.3	22.2	
geometric mean	0.0514	13	26.4	
geom. mean+1 s.dev	0.1898	14.9	31.3	
arithm. 90th %ile			33.4 inter	33.4 interpolated from plot
maximum	0.4099	17.3	37.1	

	Undistuided sues (new	es (new classification) _n = 56		
		computed	extrapolated	
category	aero roughness (cm)	spike velocity @ 7.5 cm (mph)	spike velocity @ 10 m (mph) C	Comment
minimum	0.0001	6.7	12.4	
arithm. 10th %ile			20.4 interpol	20.4 interpolated from plot
geom. mean-1 s.dev	0.0124	10.9	21.8	
geometric mean	0.0712	12.7	27.0	
geom. mean+1 s.dev	0.4106	14.7	33.4	
arithm. 90th %ile			32.7 interpol	32.7 interpolated from plot
maximum	0.4899	19.1	39.1	

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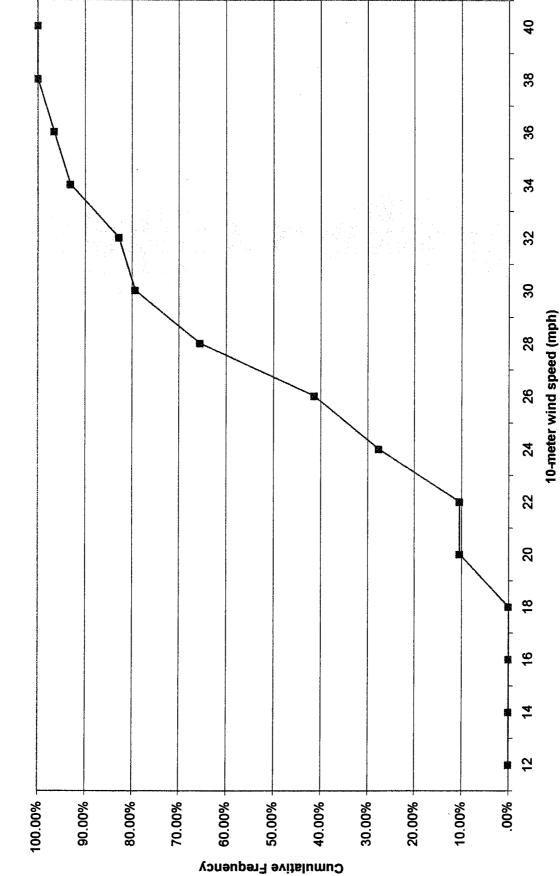
#### II. Determination of minimum wind velocity for erosion of PM-10 from vacant land surfaces

A. Wind Tunnel Data source. UNLV used data from the 1995 Wind tunnel field survey in the Las Vegas Valley to compute aerodynamic roughness heights, and velocities for initiation of PM-10 erosion. Wind tunnel flow velocity was gradually increased, and the centerline pitot tube pressure drop was recorded when the TSI Dust-Trak first measured a "spike" in PM-10 concentration exceeding 1 mg/m3 in the wind tunnel. Using site photos from UNLV's 1995 field data book, the field sites were reclassified as "stable" or "unstable" by UNLV according to criteria in the proposed Maricopa County / Clark County rules. Evidence of crusting, presence of flat vegetation and sizes of sheltering elements in the photographs were used to estimate stability of the photographed 1995 sites. In 1995, the sites had been subjectively classified as disturbed or undisturbed on the basis of evidence of human activity (debris, tire tracks, broken crust) at the field sites.

B. Wind tunnel data processing. The centerline pitot tube pressure drops corresponding to the initial PM-10 spike were converted to tunnel centerline (7.5-cm height) spike velocities. The aerodynamic roughness, determined from a series of velocity profile measurements over the soil surface, was used with the 7.5 cm data to extrapolate the spike velocities to a height of 10 meters, the global standard for measurement of wind speeds. Statistical analyses were performed on the extrapolated 10-meter spike velocities to determine a value that could be used for initiation of Valley-wide PM-10 erosion.

C. *Results.* Table 2 presents a statistical summary of the disturbed (unstable) and undisturbed (stable) 1995 wind tunnel datasets. Geometric mean 10 meter PM-10 spike velocity was 26.4 mph for the unstable sites, and 27.0 mph for stable sites. The 10<sup>th</sup> percentile interpolated value for unstable sites was 19.9 mph. The 10<sup>th</sup> percentile interpolated value for stable sites was 20.4 mph. Figure 2 (29 sites) shows a rapid jump from 10<sup>th</sup> %ile to 28<sup>th</sup> %ile between 22 and 24 mph for unstable (disturbed) sites. Figure 3 (56 sites) shows a smooth increase from 10th %ile at 20 mph, to 14th %ile at 22 mph to 21st %ile at 24 mph for stable lands.

D. *Discussion*. The author (James) used a 20 mph threshold for unstable, stable in the Feb 22 and March 28 computations of Valley-wide PM-10 vacant land estimates. This is "conservative", in that we assume the whole valley starts to emit PM-10 at 20 mph, when in fact, only 10% of the sites may be emitting PM-10 at that velocity. As a result, a 20 mph threshold tends to overestimate the amount of emitted PM-10. Effects of rain on windy

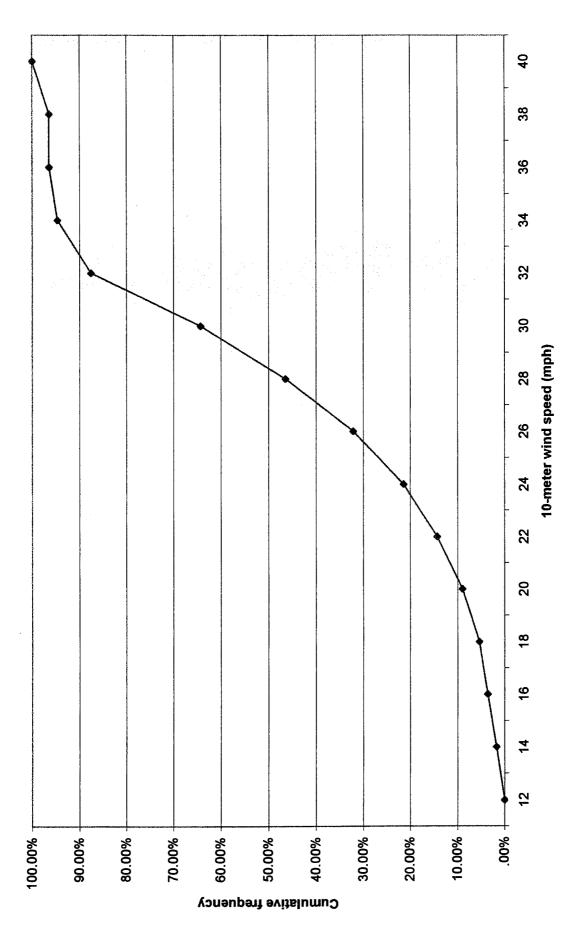


Disturbed (Unstable) threshold velocity frequency distribution

Figure 2







days were neglected in these reports. As a result, the Feb 22 and March 28 estimates were likely too high.

Uniform use of wind speeds 25 mph or higher in computing Valley-wide estimates would give disproportionate weight to stable land emissions, because, winds 25 mph or higher generate emissions from 100% - 25% = 75%of stable, undisturbed land sites (Figure 3), but only 100 - 35 = 65% of unstable land sites (Figure 2). A lower wind speed threshold is needed for unstable sites. Winds 20 mph or higher for unstable lands would generate emissions from 100 - 10 = 90% of unstable sites. Windy days with rain should be excluded from PM-10 Valley-wide emissions estimates, as wet soil does not emit PM-10, and PM-10 emitted just before a rain would be rapidly rained out of the atmosphere.

The amount of land area that could be associated with the potential to emit in the 20-22, 22-24, 24-26 mph speed ranges is currently unknown. It might be possible to correlate UNLV wind tunnel data to US Natural Resource Conservation Service soil classification and wind erosion databases, but that effort was beyond the scope of this project.

E. Wind data source. 1999 Hourly average wind observations from 18 Clark County monitoring stations (Table A.1.1 – Figure A1) were used in the computation of Valley-wide estimates. Wind-speeds for a particular station (for example Lone Mountain, LO, Polygon 17) were assumed to be valid over the entire polygon. This approach introduces error into the PM-10 estimate, as varying terrain and the presence of sheltering urban infrastructure in at least part of each polygon will contribute to variation of wind speeds within each polygon.

F. Wind data processing. ASCII wind data files containing hourly average wind speeds for 18 CCHD monitoring stations were obtained by UNLV February 2000 and imported into a MS Access97 database. The database was queried to develop new computer files containing records corresponding only to sustained hourly wind speeds greater than or equal to 20 mph. These records were used to compute hour-by hour PM10 emissions for each Thiessen polygon corresponding to a CCHD monitoring station. The database was also queried for missing records to determine the %availability of CCHD monitoring stations during 1999.

A summary of results is shown in Table 3. The table shows that the CCHD stations had, on average, 95.2% of the year's wind hours recorded. Two stations, Green Valley (GV) and Winterwood (WW) had much lower than average availability. The 70% availability of Winterwood does not introduce significant error because it is associated with a small polygon. The 83%

	Shaded cells	Shaded cells exceed average						
	<b>COHD Station</b> Site Name		Wind hours < 15 mph	5.mph   Wind hours 15-19.99 mph   Wind hours > 20 mph   hours unavailable total hours   % available	Wind hours > 20 mph	<b>Inours unavailable</b> To	otal hours.   %	available
	AP	Apex	7344	6/8	2her-1- and	137	8760	94.9%
	BS	Craig Road	8301	244	48	167	8760	98.1%
		City Center	7951	34	3	112	8760	91.2%
	сw	Crestwood	8603	16	20	121	8760	98.6%
	DM	Dime III	8392	134	16	218	8760	97.5%
	FL	Flamingo	8296	315 A. 1997	59	06	8760	<b>%0.66</b>
	GV	Green Valley	6689	102	33	152 <b>1</b>	8760	82.6%
	D	J D Smith	8368	151	12	229	8760	97.4%
	N	Jean	7980	96 <u>9</u>	691 · · · · · · · · · · · · · · · · · · ·	. 15	8760	99.8%
	LF	Laughlin	7245			0993	8760	92.7%
	ΓO	Lone Mountain	7917	066	96 · · · · · · · · · · · · · · · · · · ·	358	8760	95.9%
	MC	East Sahara	8110	135	14	109	8760	94.3%
	MS	Microscale	8497			76	8760	99.1%
	PL	S.E. Valley	7914	4/8 - 10 - 10 - 10 - 10 - 10 - 10 - 10 - 1	6L Contraction of the second second	393	8760	95.5%
	РМ	Paul Meyer Park	8417	274	56	43	8760	99.5%
	РТ	Pittman	8505	183	26	46	8760	99.5%
11	PV	Palo Verde	8016			09	8760	<b>99</b> .3%
L	SA	Sunrise Acres	8270	<b>686</b>	35	72	8760	99.2%
	SL	Shadow Lane	8606	85	2	64	8760	99.3%
	ſM	Walter Johnson	8189	224	50	327	8760	96.3%
	w	Winterwood	5938	146	18	892 No. 1	8760	69.7%
		averages	7988	281	20	420		95.2%
		totals (incl AP, JN, LF)	167,758	5	1,480	8,822	183,960	
		Valley totals	145,189		694	7,716	157,680	

Table 3

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1999 Wind frequency summary

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Table 3 (continued)

1999 Wind frequency summary

Shaded cells	Shaded cells exceed average					
<b>GOHD/Station/Site Name</b>		% unavailable	% <15 mph	valiable) % < 15 mpt = % 15-19.99 mpb   % >20 mph   Agresvaciand	Acres 0 and	Acres vac land
АР	Apex	X13 100	83.8%	William Contraction		4.0% not in valley
BS	Craig Road	1.9%	94.8%	2.8%	0.5%	22,369
cc	City Center	WOB	90.8%	0.4%	%0.0	318
CW	Crestwood	1.4%	98.2%	0.2%	0.2%	192
DM	Dime III	2.5%	95.8%	1.5%	0.2%	2,192
FL	Flamingo	1.0%	94.7%	3.0%	%2.0	7,833
GV	Green Valley	Not I Taken	78.8%	MATERIA STATE	0.4%	26,021
۵ſ	J D Smith	2.6%	95.5%	1.7%	0.1%	3,116
N	Jean	0.2%	91.1%	9679		1.9% not in valley
LF	Laughlin	NEL:	82.7%	2000		3 1% not in valley
ΓO	Lone Mountain	4.1%	90.4%	No. No.	X11	26,102
MC	East Sahara	12 N. 27%	92.6%	1.5%	0.2%	422
MS	Microscale	0.9%	%0.76	1.9%	%£'0	170
PL	S.E. Valley	4.5%	90.3%	WAR IN ANY	0.9%	8,288
PM	Paul Meyer Park	0.5%	96.1%	3.1%	%6.0	30,062
ΡŢ	Pittman	0.5%	97.1%	2.1%	0.3%	6,764
ΡV	Palo Verde	0.7%	91.5%	803	1,8%	12/125
SA	Sunrise Acres	0.8%	94.4%	MAX - CAR	0.4%	207
SL	Shadow Lane	0.7%	98.2%	1.0%	0.1%	1,315
٢M	Walter Johnson	3.7%	93.5%	2.6%	0.2%	1,523
ww	Winterwood	30.3%	67.8%	1.7%	0.2%	1,574

averages totals (incl AP,JN,LF) Valley totals

151,193

0.8%

3.2%

91.2%

4.8%

availability of Green Valley does introduce some error into the calculation, as Green Valley is associated with the third largest Thiessen polygon (26,021 acres). The effect of the omission is to reduce the magnitude of estimated PM-10 eroded from vacant lands.

Table 4 shows that the Green Valley station is missing records for four of the Valley-wide 1999 wind events exceeding 20 mph, February 25, March 30, March 31, and December 7. Inclusion of these records would lead to an increase the amount of estimated PM-10 in both the design day estimate (probably by about 50-100 tons, 10-20% of total)) and the 1999 design year estimate, (perhaps by 500-1000 tons, 3-5% of total).

Table 3 shows that selection of a 20 mph threshold for initiation of PM-10 yields 694 total erosive hours, about 0.8% of the 157,680 total hours of record for all 18 Valley monitoring stations. If a 15-mph threshold was used, then 4,081 erosive hours would contribute to PM-10 erosion, about 3.2% of the total hours of record for the Valley stations. At the two windiest sites in the network, Palo Verde (PV), recorded 1.8% of its wind hours over 20 mph, and Lone Mountain (LO) recorded 1.1% of its wind hours over 20 mph.

In conclusion, winds exceeding a 20 mph threshold for PM-10 erosion occurred 0.8% of the time in 1999, and engage 10% or more of the 1995 wind tunnel sites in the emission of PM-10.

### III. Final Version of PM-10 Emission Factors

The February 22, 2000 draft report presented emissions factors for unstable desert lands and stable desert lands, corrected for the presence of "spikes" in the data during the initial one to two minutes of wind erosion. The draft contained computed Valley-wide 1999 Design Year and February 25, 1999 design day Valley-wide emissions for varying ratios of stable and unstable vacant lands. The emissions factors were computed from 1995 UNLV wind tunnel data collected over the entire Las Vegas Valley.

The March 28, 2000 Draft report presented additional emissions factors for lands stabilized with commercial dust suppressants, not corrected for spikes. The emissions factors came from Phase II of the 1998-1999 UNLV wind tunnel study of the comparative performance of different commercial dust suppressants. Tests of the dust suppressants were performed on treated land on the east side of the Las Vegas Valley, a location where uncrusted, untreated soil was an extremely high dust emitter.

In this report, final emissions factors are presented in six categories:

4
Table

1999 Windy day tally - CCHD AQD monitoring stations

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1999 Windy day tally - CCHD AQD monitoring stations

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balb a	5/8/1999	5/12/1999	5/13/1999	5/14/1999	5/26/1999	5/30/1999	6/1/1999	6/2/1999	6/3/1999	6/6/1999	6/16/1999	6/20/1999	6/21/1999	6/25/1999	7/3/1999	7/4/1999	7/6/1999	7/7/1999	7/9/1999	7/14/1999	7/15/1999	7/27/1999	7/28/1999	7/29/1999	8/6/1999	8/10/1999	8/14/1999	8/30/1999	9/1/1999	9/18/1999	9/27/1999	9/28/1999	10/6/1999	10/15/1999	10/16/1999	10/21/1999	10/29/1999	10/31/1999

Table A – Unstable vacant lands – spike corrected. Emissions factors are the same as in the February 22, 2000 report

Table B – Stable vacant lands – spike corrected. Emissions factors are the same as in the February 22, 2000 report

Table C – Phase II treated sites - not spike corrected and not torn up by truck tire. Emissions factors are the same as in the March 28, 2000 report.

Table D - Phase II treated sites – spike corrected and not torn up by truck tire. These are new emissions factors, not previously presented, and should be used when estimating initial benefits of satisfactory application of dust suppressants

Table E – Phase II treated sites – not spike corrected, and torn up by truck tire. These factors are presented only for comparison to Table F, to demonstrate the need for using spike corrected data, and should not be used in computing Valley-wide estimates.

Table F – Phase II treated sites- spike corrected and torn up by truck tire. These factors are presented for use when estimating end of design life benefits for dust suppressants after they have experienced some mechanical degradation.

Tabulated data are presented as geometric means +/- one standard deviation to illustrate the large degree of variability in the wind tunnel data and also the asymmetric nature of the wind tunnel data sets. Emissions factors for stable and unstable desert lands are presented as averages across all soil groups, and hence, have large uncertainties in each wind-speed range.

Spike correction is defined as correction of the undue influence of the "spike" in PM-10 emissions that is usually observed by the TSI Dust Trak monitor in the first one to two minutes of a wind tunnel run. If not corrected, extrapolation of the observed PM-10 mass in a 10-minute run to an hourly average PM-10 flux estimate would overestimate an hourly average PM-10 emissions factor.

A typical spike is shown in Figure 4 for a 10-minute computer run. The spike is removed from the 10-minute data by computer processing. The spikeremoved data are converted to a 60-minute steady state value (ton/acre/hour). The spike data are converted to ton/acre and added only to the first hour of any erosive wind event. It is assumed that the PM-10 reservoir takes a minimum of 1 day to renew, so spikes are incorporated into PM-10 emissions estimates only for the first hour of wind events whose onsets that are separated by more than 24 hours.

mg/m3 - Integrated xul-140.0 200.0 180.0 160.0 120.0 100.0 60.0 40.0 20.0 80.0 + 0.0 600 Figure 4: Example of spike in 10 minute wind tunnel run - surface treated with Magnesium chloride 500 MgCl Torn Up - 12/11/98 ID:19 (TEST #2) 400 COUNT 300 200 100 RAW DATA 0 1.0 0.9 0.8 0.0 0.5 0.3 0.2 0.0 0.4 0.7 Flux 0.1 IST - ɛm\pm

	Unstable sites	CORRECTED FOR	EFFECTS OF SPIKE	DF SPIKE				
		SIC STATES OF	Disturbed Sites (new classification) $n = 68$	assection) n=60				
Wind Speed	Geom mean flux	Geom mean fi	Geom mean flux	Geom mean flux Geom mean spike Geom mean spike Geom mean spike	Geom mean spike	Geom mean spike	Number	Number
(hqm)	-1 Std. Dev		+1 Std. Dev	-1 Std. Dev		+1 Std. Dev	of flux	of spike
	(ton/acre/hr)	(ton/acre/hr)	(ton/acre/hr)	(ton/acre)	(ton/acre)	(ton/acre)	Runs	Runs
10-14.9	N/A	N/A	N/A	N/A	N/A	N/A		
15-19.9	1.50E-03	4.95E-03	1.63E-02	1.47E-04	9.65E-04	6.33E-03	3	e
20-24.9	1.23E-03	5.21E-03	2.21E-02	1.14E-04	8.16E-04	5.82E-03	4	4
25-29.9	1.18E-03	6.40E-03	3.48E-02	2.80E-04	1.94E-03	1.35E-02	12	11
30-34.9	1.21E-03	4.62E-03	1.76E-02	3.43E-04	1.41E-03	5.82E-03	13	13
35-39.9	8.96E-04	7.05E-03	5.54E-02	4.37E-04	3.80E-03	3.31E-02	19	11
40-44.9	2.37E-03	1.13E-02	5.41E-02	9.40E-04	3.45E-03	1.27E-02	6	œ
45-49.9	9.71E-04	7.12E-03	5.22E-02	1.43E-03	4.50E-03	1.42E-02	7	5
50-54.9	N/A	3.69E-03	N/A	NA	1.30E-03	N/A	-	-
55-59.9								
60-64.9								
65-69.9								
total runs							68	56

CUMULATIVE RESULTS - Method B (sum individual runs then average) Table A

	Table B	CUMULATIVE RESU	JLTS - Method B (su	CUMULATIVE RESULTS - Method B (sum individual runs then average)	ו average)			
	oldbie slies	CORRECTED FOR	Shares	errectio Of Stine unbed Sites (new classification) n = 169	6			
Wind Speed	Geom mean flux	Geom mean flux	Geom mean flux	Geom mean spike	Geom mean spike	Geom mean flux Geom mean spike Geom mean spike Geom mean spike Number	Number	Number
(hqm)	-1 Std. Dev		+1 Std. Dev	-1 Std. Dev		+1 Std. Dev	of flux	of spike
	(ton/acre/hr)	(ton/acre/hr)	(ton/acre/hr)	(ton/acre)	(ton/acre)	(ton/acre)	Runs	Runs
10-14.9								
15-19.9	N/A	1.95E-03	N/A	NA	4.00E-04	N/A	+	-
20-24.9	3.16E-04	1.38E-03	6.07E-03	2.39E-05	2.12E-04	1.88E-03	4	e
25-29.9	9.46E-04	2.57E-03	7.00E-03	1.52E-04	4.90E-04	1.58E-03	11	10
30-34.9	7.81E-04	3.16E-03	1.28E-02	1.62E-04	5.88E-04	2.14E-03	23	22
35-39.9	9.17E-04	2.99E-03	9.73E-03	2.84E-04	9.24E-04	3.01E-03	28	27
40-44.9	2.08E-03	5.92E-03	1.68E-02	6.40E-04	1.70E-03	4.53E-03	34	33
45-49.9	3.02E-03	7.58E-03	1.90E-02	9.57E-04	2.20E-03	5.05E-03	30	29
50-54.9	5.94E-03	1.10E-02	2.02E-02	1.21E-03	2.58E-03	5.48E-03	22	22
55-59.9	9.03E-03	1.69E-02	3.15E-02	1.51E-03	3.32E-03	7.29E-03	12	12
60-64.9	9.99E-03	1.66E-02	2.76E-02	1.62E-03	4.03E-03	1.00E-02	4	4
6.69-39								
total runs							169	163

	Table C	STABILIZED LAND E	EMISSION FACTORS	MISSION FACTORS - averaged over 7 tested suppressants	ted suppressants		
	treated sites	NOT CORRECTED F	<b>-OR EFFECTS OF SI</b>	NOT CORRECTED FOR EFFECTS OF SPIKE - NOT TORN UP			
Wind Speed	Geom mean flux	Geom mean flux	Geom mean flux	Geom mean spike	Geom mean spike	Geom mean spike	Number
(hdm)	-1 Std. Dev.		+1 Std. Dev.	-1 Std. Dev.		+1 Std. Dev.	of runs
	(ton/acre/hr)	(ton/acre/hr)	(ton/acre/hr)	(ton/acre)	(ton/acre)	(ton/acre)	
10-14.9							
15-19.9	2.14E-04	4.20E-04	8.26E-04	N/A	N/A	N/A	22
20-24.9	1.22E-04	3.42E-04	9.60E-04	N/A	N/A	N/A	36
25-29.9	5.26E-05	1.94E-04	7.15E-04	N/A	N/A	N/A	20
30-34.9	N/A	N/A	N/A	N/A	N/A	N/A	N/A
35-35.9	N/A	N/A	N/A	N/A	N/A	N/A	N/A
40-44.9	N/A	N/A	N/A	N/A	N/A	N/A	N/A
45-49.9	N/A	N/A	N/A	N/A	N/A	N/A	N/A
50-54.9	N/A	N/A	N/A	N/A	N/A	N/A	N/A
55-59.9	N/A	N/A	N/A	N/A	N/A	N/A	N/A
60-64.9	N/A	N/A	N/A	N/A	N/A	N/A	N/A
65-69.9	N/A	N/A	N/A	N/A	N/A	N/A	N/A
total runs							78

	Table D	STABILIZED LAND E	EMISSION FACTORS	MISSION FACTORS - averaged over 7 tested suppressants	ted suppressants		
	treated sites	CORRECTED FOR E	EFFECTS OF SPIKE - NOT TORN UP	- NOT TORN UP			
Wind Speed	Geom mean flux	Geom mean flux	Geom mean flux	Geom mean spike	Geom mean spike	Geom mean spike	Number
(hdm)	-1 Std. Dev.		+1 Std. Dev.	-1 Std. Dev.		+1 Std. Dev.	of runs
	(ton/acre/hr)	(ton/acre/hr)	(ton/acre/hr)	(ton/acre)	(ton/acre)	(ton/acre)	spike corrected
10-14.9							
15-19.9	1.00E-04	2.65E-04	7.04E-04	7.26E-07	5.03E-06	3.48E-05	18
20-24.9	5.24E-05	1.38E-04	3.65E-04	1.74E-06	4.59E-06	1.21E-05	32
25-29.9	1.92E-05	1.09E-04	6.19E-04	N/A	NA	N/A	18
30-34.9	N/A	N/A	N/A	N/A	N/A	N/A	2
35-35.9	N/A	N/A	N/A	N/A	N/A	NA	NA
40-44.9	N/A	N/A	N/A	N/A	N/A	NA	N/A
45-49.9	N/A	N/A	N/A	N/A	N/A	N/A	N/A
50-54.9	N/A	N/A	N/A	N/A	N/A	NA	N/A
55-59.9	N/A	N/A	N/A	N/A	NA	N/A	NA
60-64.9	N/A	N/A	N/A	N/A	N/A	N/A	N/A
65-69.9	N/A	N/A	N/A	N/A	N/A	N/A	N/A
total runs							70

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4	4

ECTED FOR EFFECTS OF SPIKE - TORN UP BY TR       an flux     Geom mean flux     Geom mean spike       an flux     Geom mean flux     Geom mean spike       an flux     Geom mean flux     Geom mean spike       an flux     Geom mean spike     -1 Std. Dev.       an flux     Thr)     (ton/acre/hr)     (ton/acre)       an flux     Con/acre/hr)     N/A     N/A       an in flux     Size-02     N/A     N/A       an in flux     N/A     N/A     N/A       an in flux     Size-03     N/A     N/A       an in flux     N/A     N/A     N/A	Table E STABILIZED LAND EMISSION FACTORS - averaged over 7 tested suppressants	ON FACTORS	<ul> <li>averaged over 7 tes</li> </ul>	sted suppressants		
Geom mean flux         Geom mean flux         Geom mean flux         Geom mean spike           -1 Std. Dev.         -1 Std. Dev.         -1 Std. Dev.         -1 Std. Dev.           -1 Std. Dev.         (ton/acre/hr)         (ton/acre/hr)         (ton/acre/hr)         (ton/acre/hr)           N/A         N/A         N/A         N/A         N/A           N/A         2.18E-03         9.39E-03         5.22E-02         N/A           1.69E-04         2.17E-03         1.15E-02         N/A         N/A           N/A         8.14E-04         2.57E-03         N/A         N/A           N/A         8.14E-04         2.57E-03         N/A         N/A           N/A         N/A         N/A         N/A         N/A           N/A         N/A<		FECTS OF SP	IKE - TORN UP BY T	RUCK TIRE		
-1 Std. Dev.         +1 Std. Dev.         -1 Std. Dev.           -1 Std. Dev.         (ton/acre/hr)         (ton/acre/hr)         (ton/acre/hr)           (ton/acre/hr)         (ton/acre/hr)         (ton/acre/hr)         (ton/acre)           N/A         2.18E-03         9.39E-03         5.22E-02         N/A         N/A           1.69E-03         9.39E-03         5.22E-02         N/A         N/A         N/A         N/A           1.1692-04         2.17E-03         1.15E-02         N/A         N/A         N/A         N/A           N/A         8.14E-04         2.57E-03         N/A         N/A         N/A         N/A           N/A         N/A         N/A         N/A         N/A         N/A           N/A         N/A         N/A         N/A         N/A         N/A           N/A         N/A         N/A         N/A         N/A         N/A	Geom mean flux		Geom mean spike	Geom mean spike	Geom mean spike	Number
(ton/acre/hr)         (ton/acr			-1 Std. Dev.		+1 Std. Dev.	of runs
N/A         2.18E-03         N/A         N/	(ton/acre/hr)	/acre/hr)	(ton/acre)	(ton/acre)	(ton/acre)	spike corrected
N/A         2.18E-03         N/A         N/A         N/A           1.69E-03         9.39E-03         5.22E-02         N/A         N/A           4.10E-04         2.17E-03         1.15E-02         N/A         N/A           2.58E-04         8.14E-04         2.57E-03         N/A         N/A           N/A         N/A         1.15E-03         N/A         N/A           N/A         N/A         2.57E-03         N/A         N/A           N/A         N/A         1.15E-03         N/A         N/A           N/A         N/A         N/A         N/A         N/A     <						
1.69E-03         9.39E-03         5.22E-02         N/A         N/A           4.10E-04         2.17E-03         1.15E-02         N/A         N/A           2.58E-04         8.14E-04         2.57E-03         N/A         N/A           N/A         8.14E-03         1.15E-02         N/A         N/A           N/A         N/A         N/A         N/A         N/A      <		N/A	N/A	N/A	N/A	2
4.10E-04         2.17E-03         1.15E-02         N/A         N/A           2.58E-04         8.14E-04         2.57E-03         N/A         N/A           N/A         3.61E-03         N/A         N/A         N/A           N/A         3.61E-03         N/A         N/A           N/A         N/A         N/A         N/A	9.39E-03	22E-02	N/A	N/A	N/A	22
2.58E-04         8.14E-04         2.57E-03         N/A	2.17E-03	15E-02	N/A	N/A	N/A	58
N/A     3.61E-03     N/A     N/A     N/A       N/A     N/A     N/A     N/A     N/A	8.14E-04	57E-03	N/A	N/A	N/A	46
N/A     N/A     N/A     N/A		N/A	N/A	N/A	N/A	2
NIA		N/A	N/A	N/A	N/A	N/A
NIA		N/A	N/A	N/A	N/A	N/A
NIA		N/A	N/A	N/A	N/A	N/A
NIA		N/A	N/A	N/A	N/A	N/A
N/A N/A N/A N/A N/A N/A N/A N/A		N/A	N/A	N/A	N/A	N/A
		N/A	N/A	N/A	N/A	N/A
	A N/A	N/A	N/A	N/A	N/A	N/A
total runs						130

	Table F	STABILIZED LAND E	EMISSION FACTORS	STABILIZED LAND EMISSION FACTORS - averaged over 7 tested suppressants	ted suppressants		
	treated sites	CORRECTED FOR E	EFFECTS OF SPIKE	CORRECTED FOR EFFECTS OF SPIKE - TORN UP BY TRUCK TIRE	K TIRE		
Wind Speed	Geom mean flux	Geom mean flux	Geom mean flux	Geom mean spike	Geom mean spike	Geom mean spike	Inumber
(uduu)	-1 Std. Dev.		+1 Std. Dev.	-1 Std. Dev.		+1 Std. Dev.	of runs
	(ton/acre/hr)	(ton/acre/hr)	(ton/acre/hr)	(ton/acre)	(ton/acre)	(ton/acre)	spike corrected
10-14.9	N/A	1.87E-03	N/A	N/A	4.05E-03	N/A	2
15-19.9	7.20E-04	3.80E-03	2.01E-02	2.10E-05	2.67E-04	3.40E-03	22
20-24.9	1.04E-04	8.89E-04	7.60E-03	9.09E-06	5.64E-05	3.50E-04	58
25-29.9	1.01E-04	4.70E-04	2.19E-03	2.56E-06	1.63E-05	1.04E-04	46
30-34.9	NA	3.57E-03	N/A	N/A	9.68E-06	N/A	2
35-35.9	N/A	N/A	NA	N/A	N/A	N/A	N/A
40-44.9	N/A	NA	N/A	N/A	N/A	N/A	N/A
45-49.9	N/A	N/A	N/A	N/A	N/A	N/A	N/A
50-54.9	N/A	N/A	N/A	N/A	N/A	N/A	N/A
55-59.9	N/A	N/A	N/A	N/A	N/A	N/A	N/A
60-64.9	N/A	NA	N/A	N/A	N/A	N/A	N/A
65-69.9	NA	NA	N/A	N/A	N/A	N/A	N/A
total runs							130

Spike corrections are significant for stable and unstable, untreated desert lands, and for torn up, treated desert lands. Spike corrections are not significant for treated, not-torn up desert lands.

The following table briefly summarizes mean spike-corrected PM-10 emissions factors for all categories, without uncertainties:

Table 5. Summary of geometric mean-spike corrected PM-10 emissions factors

Source Wind speed range (mph)	Table A Unstable land	Table B Stable land	Table D Treated not torn up	Table F Treated torn up
	ton/acre/hr	ton/acre/hr	ton/acre/hr	ton/acre/hr
15-19.9	4.95x10-3	$1.95 \times 10-3$	$2.65 \times 10-4$	3.80x10-3
20-24.9	5.21x10-3	1.38x10-3	1.38x10-4	8.89x10-4
25-29.9	6.40x10-3	$2.57 \times 10-3$	1.09x10-4	4.70x10-4
30-34.9	4.62x10-3	3.16x10-3		
35-39.9	7.05x10-3	2.99x10-3		
40-44.9	1.13x10-2	5.92x10-3		

Emissions factors reported in Tables A and B have not changed since the February 22, 2000 report, and should match the values used in the Dames and Moore microinventory. Tables A and B show the sample sizes used to compute geometric means, and also report the uncertainties of the estimates.

The following table briefly summarizes mean PM-10 emissions spikes for all categories, without uncertainties:

Table 6. Summary of geometric mean spike factors for use in emissions calculations

Source Wind speed	Table A Unstable	Table B Stable	Table D Treated	Table F Treated
range (mph)	land	land	not torn up	torn up
	ton/acre	ton/acre	ton/acre	ton/acre
15-19.9	9.65x10-4	$4.00 \times 10-4$	5.03x10-6	2.67x10-4
20-24.9	8.16x10-4	$2.14 \times 10-4$	4.59x10-6	5.64x10-5
25-29.9	$1.94 \times 10-3$	$4.90 \times 10-4$		$1.63 \times 10-5$
30-34.9	$1.41 \times 10-3$	5.88x10-4		9.68x10-6
35-39.9	3.80x10-3	9.24x10-4		
40-44.9	3.45x10-3	$1.70 \times 10-3$		

The effects of removing spikes from the Phase II not torn up data was small, since the spikes themselves are of low magnitude for intact, treated surfaces (see column entry Table D in Table 6, above).

The following table compares Phase II mean not torn-up emission factors, again omitting uncertainties, for the not spike corrected and spike-corrected cases.

Table 7. Not spike-corrected and spike-corrected emissions factors for	not
torn up Phase II treated surfaces	

Source	Table C	Table D
Wind speed	Treated - not torn up	Treated - not torn up
range (mph)	not spike-corrected	spike-corrected
	ton/acre/hour	ton/acre/hour
15-19.9	4.20x10-4	2.65x10-4
20-24.9	3.42x10-4	1.38x10-4
25-29.9	1.94x10-4	1.09x10-4
30-34.9		
35-39.9		
40-44.9		

If standard deviations are considered, the differences between the factors in Tables C and D are not statistically significant

Valley-wide emissions estimates for various scenarios of stabilized land, computed and reported for Phase II not-spike corrected, not torn up emission factors (Table C, this report) in the March 28, 2000 report, have been recomputed for the spike-corrected emission factor data in Table D. The results are presented in Appendix A of this report.

The results for Valley-wide PM-10 emissions from a mixture of stable and stabilized lands using spike-corrected Phase II values differ slightly from the results reported in March. Results are summarized in Tables 8 and 9. The September 13, 2000 report column in Tables 8 and 9, using spike-corrected stabilized lands should be considered the definitive estimate for stabilized lands newly treated with dust suppressant. Table 8 – 1999 Annual emissions estimates using revised, Phase II spikecorrected values for newly treated surfaces. September 13, 2000 data are in Appendix A of this report

Ratio stable/	March 28, 2000	Sept 13, 2000
stabilized	non-spike corrected	spike corrected
	not torn up	not torn up
	tons	tons
70/30	12,144	11,661
80/20	13,424	13,102
90/10	14,705	14,544

Table 9 – February 25, 1999 Design day emissions estimates using revised, Phase II spike-corrected values for newly treated surfaces. September 13, 2000 data are in Appendix A of this report

Ratio stable/ stabilized	March 28, 2000 non-spike corrected not torn up	Sept 13, 2000 spike corrected not torn up
	tons	tons
70/30	478	457
80/20	529	516
90/10	580	583

Effects of the degradation of stabilized surface can be modeled by using spike-corrected emissions factors from Table D, for stabilized, not-torn up, and from Table F, for stabilized, torn up. The effects of degradation are shown below in Tables 10 and 11

Table 10 - 1999 Annual emissions estimates using revised, Phase II spikecorrected values for not-torn up and for torn up surfaces

Table D spike corrected	Table F spike corrected
not torn up	torn up
tons	tons
11,661	13,600
13,102	14,395
14,544	15,190
	spike corrected not torn up tons 11,661 13,102

Table 11 – February 25, 1999 Design day emissions estimates using revised,Phase II spike-corrected values for not-torn up and for torn up surfaces. Ratiostable/Table DTable F

stabilized	spike corrected	spike-corrected
	not torn up	torn up
	tons	tons
70/30	457	534
80/20	516	567
90/10	583	609

IV. Field surveys to assess feasibility of using methodologies contained in the proposed Maricopa County Rule and Proposed Clark County Rule 41 for determining susceptibility of land parcels to wind erosion.

A. Data source. Copies of the proposed draft Maricopa County rule and the proposed Clark County Rule 41 were obtained on September 2, 1999 from Rodney Langston of Clark County Comprehensive Planning. The proposed rules are principally intended to require control measures for disturbed vacant land, and establish criteria for when a vacant land parcel requires control measures. The proposed rules also contain procedures for determining susceptibility of vacant lands to wind erosion. The proposed Clark County Rule 41 is a modification of the draft Maricopa County rule, was under consideration for adoption in Clark County.

B. Procedure development and modification. After initial field trials of the proposed procedures in proposed Clark County rule 41, a flow chart was developed by graduate student Sherrie Edwards to aid field crews in the rapid testing of vacant land parcels for susceptibility to wind erosion.

The flow chart, comprised of a series of if-then statements, allowed for efficient sampling of sites under consideration. In essence the flow chart guides a field inspector through the following flow of tests.

- Using a 1-foot square sampling quadrat tossed at random into the site, perform drop ball test using a 5/8" stainless steel ball bearing from 1-foot height, and observe effects of ball impact on soil surface. The ball dimensions and drop height are specified in section 41.9.3. Repeat the test three times inside the randomly cast quadrat.
  - a. If there is no damage to the soil crust, or no splashing of particles from the surface in two or more of the three samples inside the randomly-cast quadrat, the test result is classified

as a "pass", and that quadrat is classified as resistant to wind erosion.

- b. If there is damage to the crust (formation of a distinct indentation), or splashing of particles from the surface, in two or more of the three samples inside the randomly-cast quadrat, then the result is classified as a "fail" inside that quadrat.
- c. The quadrat is then cast into the site several (a minimum of six) more times, and the tests are repeated.
  - (1) If a majority of ball drop determinations in the cast quadrats are passes, then the parcel is classified as not susceptible to wind erosion. No further testing need be done if the parcel passes the ball-drop test.
  - (2) If a majority of ball drop determinations are "fail", then the parcel is potentially susceptible to wind erosion, and testing proceeds to the next stage.
- 2. A 100 foot string count is conducted at the site to measure the frequency distribution of flat vegetation, debris and rocks larger than 1 centimeter in diameter (all classified as non-erodible elements). Note that the procedure described in the draft Maricopa County rule specifies that only flat vegetation be counted. The procedure identified in the draft Clark County rule specifies that flat vegetation, debris (such as pieces of glass) and rocks > 1 centimeter be counted. UNLV followed the draft Clark County rule, section 41.9.5.
  - a. The string count was conducted by using a US Natural Resource Conservation Service soil erosion test kit containing at 50-foot string with 1 centimeter diameter plastic beads attached at 6-inch intervals along the string. Every other bead was used to conform to the 1-foot spacing specified in the Maricopa County rule. Alternate beads were marked with stripes from a permanent felt-tip marker to generate easily recognizable beads at 1-foot intervals.
  - b. The 50-foot string was extended twice in the same direction to generate a 100-foot transect.
  - c. Transect directions were, where possible, chosen using a table of random numbers.
  - d. Any object 1-centimeter in diameter or larger underneath any portion of the bead was counted as covering the soil at that bead. The object could be a pebble, a twig, a tuft of grass, any anthropogenic trash, or an overhanging branch of a large bush.
  - e. A rapid fill-in table was developed by graduate student Sherrie Edwards to ease the process of counting non-erodible elements, with + signs indicating a non-erodible element,

and – signs indicating absence of non-erodible elements. After 2 counts using the 50-foot string, the number of + signs in the table was summed, and divided by 100 to give the percentage frequency of flat vegetation + non-erodible elements.

- f. Interpretation of test results:
  - (1) If the frequency of flat vegetation + non-erodible elements at the site exceeded 50%, the parcel was rated as stable on that transect.
  - (2) If the frequency was  $\leq 50\%$ , then the threshold friction velocity test (TFV) was performed.
- g. The TFV test requires sampling of the top layer of soil with a dust pan, and pouring the soil through a set of sieves, per section 41.9.4.1. Retained sieve soil volumes are measured in a 250-mL plastic graduate cylinder, and a TFV is assigned based on the predominant volume (mode) of soil retained on one of the sieves.
- h. Interpretation of TFV test results:
  - If sieve analysis test shows TFV > 100 centimeters per second (cm/sec), then the sample is rated as "stable".
  - (2) If the sieve analysis shows a TFV < 100 cm/sec, then the Rock Test is needed.
  - (3) Several more samples are collected and sieved, and the majority of TFV determinations are used in determining the stability of the parcel.
- i. Rock Test. The method used by UNLV does not conform to the Rock Test Method proposed in the September 2, 1999 draft of Clark County proposed rule 41 or the June draft of the proposed Maricopa County rule. In December of 1999, UNLV attempted to develop a faster, more quantitative procedure than that described in 41.9.7 of the draft Clark County Rule. The proposed UNLV test method is as follows:
- j. Using a metal dustpan, sample all rocks to a depth of 1 cm from a random cast of a 1-foot square quadrat. Pour the sample through a 1-centimeter (1 cm) sieve. Pour rocks retained on the 1 cm sieve into a metal cake pan, and shake the pan gently, holding at a slight angle, to move the rocks into a single closely packed layer in one corner of the pan. Lay the pan flat and square up the rock layer with a ruler, and measure its dimensions with the ruler. Compute the area of the rock layer in square inches and divide by 144 square inches (1 square foot), and multiply by 100 to determine the percentage coverage by rocks on the tested site. Divide the percentage coverage by 2 to determine the percent frontal area occupied by rocks on that site.

- k. Interpretation of test results
  - (1) If rock frontal area exceeds 10%, then the site is stable.
  - (2) If rock frontal area is less than 10%, then adjust the TFV using the percent frontal area per the table shown in section 41.9.4.1 in the draft Clark County rule.
  - (3) If adjusted TFV exceeds 100 cm/sec, the tested site is stable
  - (4) If adjusted TFV is less than 100 cm/sec, the tested site is not stable.
  - (5) Repeat the rock test from several other randomly chosen sites on the parcel to determine the stability of the parcel.
- C. Results of UNLV field work. UNLV carried out field sampling between October 1999 and March 2000, with the bulk of the sampling conducted in January and February. Where available, aerial orthophotos were used to guide the selection of field parcels and plan access to sites.

All fieldwork was performed during the near-record 140-day dry spell experienced in the Las Vegas Valley in the early winter and spring of 2000.

1. Of 69 sites studied, ball drop data are available for 60 sites. Of these 60 sites, 33 (55%) passed ball drop and 27 (45%) failed. All 27 failed sites were tested for % non-erodible elements using the string count.

2. Four parcels with no ball drop data have %non-erodible data, giving a total of 27 + 4 = 31 that can be studied for %non-erodible cover. Of these 31 sites, 16 (52%) passed the 50% non-erodible criterion, and 15 (48%) failed (had less than 50% non-erodible elements).

3. Of 15 parcels failing %non-erodible, 12 were tested for TFV (threshold friction velocity). Of these 12 sites, 8 (67%) passed the TFV criterion (TFV > 100 cm/sec) and four (33%) failed the TFV criterion (< 100 cm/sec).

4. Of 27 parcels with records that show failing ball drop, 9 passed TFV (one more parcel than in #3 because one site that passed non-erodible was also tested for TFV and passed, as we expected it to do). The actual ratio should be 8 of 27 (30%), because the one additional parcel that passed the non-erodible cover criterion wouldn't ordinarily have been tested for TFV.

5. Parcels failing all three tests were all located in just one of the three sections that have been studied on the east side of the Valley. Locations are identified in Table B-4, Field Sampling Summary.

6. After a visit to the parcel for field tests, its land area was measured on the digitized aerial orthophotos and recorded in square feet. See Table B-4, Field Sampling Summary.

7. Six of 69 visited parcels were rated as unstable (9% of total tested parcels). The land area of the unstable parcels was 870,000 ft2. The measured land area of all tested parcels was 87,000,000 ft2, and at the time of this writing the land area determinations had not been completed. The percentage land area rated as unstable in the UNLV tests was 1%. It should be noted that UNLV's site visits north of the Summerlin Parkway, US 95, Bonanza Road alignment were limited, and a definitive value for percentage unstable land by the proposed Clark County rule would require a more extensive set of field observations.

Of these 6 sites, 4 were identified by the sequence of three tests ball drop -%non-erodible - TFV). Please note that these six sites comprise 9% of tested parcels, not 9% of tested parcel area. The six disturbed parcels represent less than 1% of the land area tested by UNLV.

8. For comparison, Dames and Moore's intensive microscale study around five CCHD monitors estimated 10% to 59%% unstable, with an overall average of 15%.

9. Clark County Health District's dust inspectors (McDonnell-Canan and Wallenmeyer, personal communication 2000) gave a qualitative estimate of %unstable land from their field observations at 20%.

10. UNLV obtained a copy of Clark County Health District's dust permit database in MS-Access97 format. A query of this database showed a total of 40,243 acres permitted in Clark County sometime during 1999. The query searched for all dust permits granted for periods ranging from Jan 1, 1998 -Jan 1, 1999 to December 29, 1999 to December 29, 2000, and produced 3991 records. Some of these permits were for projects outside the BLM Land Disposal boundary. Although there is no way to tell when the construction regulated by the permits took place, if one estimates that the activity was spread uniformly through time, with a two-year time interval in Jan 1, 1998 through December 29, 1999, then the estimate of the number of acres under construction with potential to emit wind-blown dust would be 40.243 / 2 = 20, 122 acres as an average value for calendar year 1999. If all this activity took place inside the BLM boundary, this would give a potential % unstable value of 20,122 / 148,575 = 13%. Given that contractors will apply control measures, the actual number of acres from construction with potential to emit wind blown dust would be less than 20,122, so the 13% value should be considered a maximum estimate for this method.

Results from the different methods used to estimate percent unstable vacant land are summarized below in Table 12.

Table 12. Summary of Percent Unstable Vacant land estimates obtained by different methods

Source	Method	Ave. value
Clark County dust inspectors	Visual estimate	20%
Dames & Moore microinventory	Clark County rule	15%
UNLV analysis CCHD dust database	Permitted area	13%
UNLV field inspections	Clark County rule	1%*

The \* indicates that land area measurements for UNLV-visited parcels are incomplete; when completed, the percent unstable area from UNLV field tests is <1%. The UNLV field visits included sites on the West site of the Valley where had been little human activity. UNLV did not sample the northern and northeastern parts of the valley with the same intensity as it sampled the south. Sampling of sites in these areas, especially in developed areas might raise UNLV's estimate.

The Dames & Moore microinventory was carried out around several monitors in the urban core of the valley, where a higher percentage of disturbed (unstable) land might be expected as a result of human activity. Several group consultations featuring participation by Clark County Comprehensive Planning, Clark County Health District, Dames and Moore, and EPA were performed between October 1999 and July 2000 to demonstrate UNLV flow chart and proposed modifications to the rule.

## V. Determination of Vegetative Densities on Vacant Lands by Examination of Aerial Photos.

A. *Data source*: In Spring 1999, Clark County conducted a complete aerial orthophoto survey of the Las Vegas Valley. An aerial orthophoto database was generated that contained images corresponding to each township, range and section (approximately 1 square mile). Photos are available in digitized format at levels of 1-foot, 2-foot and 4-foot resolution. The photo edges slightly exceeded the section boundaries.

B. Image generation: A set of 54 orthophotos digitized at 1-foot resolution from within the Clark County land disposal boundary was requested by UNLV from Clark County Comprehensive Planning from October 1999 through January 2000. The aerial photos, digitized with pixel resolutions of 1 foot, were printed in large A-size format at a scale of 1 inch = 200 feet (200 linear pixels to the inch), producing images approximately 26 inches x 26 inches for a 1 square mile section. Printing, performed by Clark County Comprehensive Planning, was on a HP DesignJet 755 large-format color inkjet printer with a resolution of 600 dots per inch, giving a printer resolution of 3 dots per linear pixel (or, 9 dots per square pixel). Printer output switches were set by Majed Khater (Clark County Comp Planning, 1999-2000) to give fairly accurate color rendition and high contrast.

At 1-foot pixel resolution, objects on the order of 2 feet in diameter can be resolved with the naked eye, occupying a physical dimension on the printed photos of 0.010 inch x 0.010 inch. This dimension corresponds approximately to the canopy diameter of desert vegetation such as *Larrea divaricata*, creosote bush. Printer contrast settings were determined that allowed desert vegetation, including creosote bush and trees, to appear in contrast to the background desert soil surface.

C. Image examination: Each selected aerial photo was manually inspected for vegetation densities. A transparent grid, of resolution 20 squares to the linear inch (0.05 linear inch per square), 400 squares to the square inch, was overlaid on a subregion of each aerial photo, and the number of grids containing contrasting vegetation was counted. The percentage area covered by vegetation was then determined by dividing the number of vegetation grids by the total number of grids in the sampled region. This process was repeated on 10 subsections of the aerial photo, and an average percentage areal cover was computed and reported for that photo.

## D. Results of analysis:

- 1. Of 54 photos examined by UNLV between November 1999 and January 2000, 52 could be analyzed for percent coverage by large shrubs and trees. Two contained terrain that was too steep to permit accurate estimation of vegetative coverage. Plants on steep slopes falling away from the camera lens will appear at a denser coverage than if they were on flat ground.
- 2. The raw vegetation coverages for the 52 photos inspected by UNLV is tabulated in Table B-5. A summary is shown below in Table 13:

10	Veg cover		Frequency	Cumulative %	Indiv%
		0	4	8%	8%
:		2	15	37%	29%
		4	3	42%	6%
		6	7	56%	13%
		8	3	62%	6%
		10	3	67%	6%
		12	4	75%	8%
		14	2	79%	4%
		16	0	79%	0%
		18	2	83%	4%
		20	0	83%	0%
		25	3	88%	6%
		30	2	92%	4%
		40	2	96%	4%
		50	1	98%	2%
		60	1	100%	2%
A	rithmetic mean				9.7%
G	eometric mean			444	4.6%

Table 13. Frequency distribution of Vegetative cover data from Aerial Photo Analysis

The vegetation distribution in the sampled photos is bimodal, with peaks at 0-2% and 4-6% vegetative coverage. It is strongly right-skewed, with a few photos showing fairly high densities. As a result, a geometric mean is a better measure of central tendency, giving a value of about 5% coverage.

## E. Sources of measurement error:

Resolution of the photos (1 foot per pixel) is not sufficient to resolve objects smaller than two feet in diameter, so individual small plants and individual tufts of grass will not be detected by this method. Dense carpets of grass and small plants can be detected, if contrast is sufficient, and areas with developed lawns, such as golf courses, could be detected in the photos. However, light or scattered carpets of short-statured grasses, often found on desert soil surfaces, could not be detected by manual orthophoto inspection. As a result, the vegetation coverage determined by visual inspection of areal photos will tend to *underestimate* the total fraction of land area covered by vegetation compared to site visits. Appendix A – Valley-wide emissions estimates using stabilized soil, spikecorrected emissions factors

Religins	ele los en ma	Sile Names 2019	Approximate crossing streets of location a
1	CC	City Center	Bonanza & 7th street
2	WW	Winterwood	E Sahara & Nellis
3	SL	Shadow Lane	Alta & Shadow Ln
4	BS	Craig Road	Craig Road & I15
5	PL	S.E. Valley	W Lake Mead Drive & Van Wagenen
6	MC	East Sahara	Maycliff Storage - E Sahara & I-515
7	MS	Micro-scale	E Charleston & 28th St.
8	DM	Dime III	~1/2 mile south of Winterwood station
9	FL	East Flamingo	E Flamingo & Swenson
10	PT	Pittman	Boulder Highway & Pabco Rd
11	JD	J.D. Smith	Bruce & Tonopah
12	PM	Paul Meyer Park	W Flamingo & Tenaya
13	WJ	Walter Johnson	W Alta & Buffalo
14	GV	Green Valley	Arroyo Grande & Santiago
15	CW	Crestwood	E Charleston & 17th St
16	SA	Sunrise Acres	Sunrise Acres E.S Sunrise & N. Eastern
17	LO	Lone Mountain	W. Gowan and Buffalo
18	PV	Palo Verde	Palo Verde H.S W Alta & Hulalapai

Table A.1.1 - Correspondence of GIS Polygons to Clark County Health District Monitoring stations

Table 1-III 1999 PM-10 Valley-wide emissions estimate Assuming fixed stable/stabilized ratio

Phase II stabilized land geometric means 9/10/2000 spike corrected, not torn up

やいいいに、 オービスには、レート・ドラインドレードに、 アイアンドレード・ドラインド				and down which we are a soluted to all the	いたからないためのためであると	State of the second second
8	3	318	%06	10%	1.7	0.0%
2 ww	18	1,574	%06	10%	38.3	0.3%
3 s	5	1,315	%06	10%	9.0	0.1%
4 bs	48	22,369	%06	10%	2,548.9	17.5%
50	79	8,288	%06	10%	876.9	6.0%
6 mc	14	422	%06	10%	8.5	0.1%
7 ms	23	170	%06	10%	5.5	0.0%
8 dm	16	2,192	%06	10%	46.6	0.3%
91	59	7,833	%06	10%	636.2	4.4%
10 pt	26	6,764	%06	10%	239.7	1.6%
11 id	12	3,116	%06	10%	57.8	0.4%
12 lom	26	30,662	%06	10%	1,148.7	7.9%
13 Wi	20	1,523	%06	10%	44.9	0.3%
14 av	33	26,021	%06	10%	1,216.5	8.4%
15 CW	20	192	%06	10%	27.3	0.2%
16 sa	35	207	%06	10%	9.9	0.1%
17 10	95	26,102	%06	10%	4,515.0	31.0%
18 DV	162	12,125	%06	10%	3,112.3	21.4%
Total	ROA	151 189			14 543.8	100.0%

Table 2-III 1999 PM-10 Valley-wide emissions estimate Assuming fixed stable/stabilized ratio

Phase II stabilized land geometric means 9/10/2000 spike corrected, not torn up

	three winds == 26 mph (rev vacanti and (acres) % stable) % stable % stable 260 mph (rous) % 0. total	mt land (acres) % s	table % stabili	Zeel PM-10 (TOPS)	X610110101
		318	80% 2	20% 1.6	0.0%
3	18	1.574	80% 2	20% 34.5	5 0.3%
Z WW	2	1.315		20% 8.1	0.1%
3 SI	48	22,369	80% 2	20% 2,284.3	
	<u></u>	8.288	80% 2	20% 789.5	
1010	14	422	80% 2	20% 7.7	7 0.1%
0	23	170	80%	20% 4.9	0.0%
/ UIS	16	2.192	80% 2	20% 41.9	9 0.3%
0 411	59	7.833	80% 2	20% 572.6	
10 01	26	6,764		20% 215.8	
10 01	12	3.116	80%	20% 51.9	
	26	30.662		20% 1,033.4	
12 Dili	20	1.523	80%	20% 40.5	
13 WJ	33	26,021	80%	20% 1,094.4	
14 UV 46 arr	20	192	80%	20% 26.7	
10 CW	35	207	80%	20% 8.9	
17 10	95	26,102	80%	20% 4,086.3	
14 10	162	12,125	80%	20% 2,799.5	
	694	151.189		13,102.5	5 100.0%

Table 4-III 1999 PM-10 Valley-wide emissions estimate Assuming fixed stable/stabilized ratio

Phase II stabilized land geometric means 9/12/2000 spike corrected, not torn up

% of						0.1%						7.9%		3 8.3%	0.2%	0.1%	3 31.4%		2 100.0%
ENHIO (tons)	1.4	30.7	7.2	2,019.6	702.2	6.8	4.4	37.3	508.9	191.8	46.1	918.0	36.2	972.3	26.1	8.0	3,657.6	2,486.8	11,661.2
% stabilized	30%		30%		30%		30%	30%	30%		30%	30%	30%	30%	30%		30%	30%	
s) % stable	318 70%	74 70%			88 70%				33 70%		3.116 70%								
nev vacantiland (acre	<b>.</b>	1.574	1.315	2	8.288			5				C					36		-
# hours wind >= 20 moh Tev vacant land (acres) % stable % stabilized PM+10 (tons)		100		48	6 <u>/</u>		100		20	290	10	1. 80		33		20	20	162	TO1
a thread the truth of the			Z WW	3 SI		1 d c	e mc	Sm /				D( 11	12 pm	13 WJ	14 gv	15 CW	16 Sa	17 10	

Table 5-III Design day PM-10 Valley-wide emissions estimate Assuming fixed stable/stabilized ratio

Phase II stabilized land geometric means spike-corrected, not torn up

	Man Calar	<u>%0 0</u>	20.0	0.4%	1.5%	10.4%	5.6%	0.3%	0.2%	0.5%	7.0%	4.6%	0.8%	38.7%	1.6%	<b>%0</b> .0%	%0.0	0.2%	23 4%	708 1	F	×0.001
	M. COVINS			2.3	9.0	60.5	32.8	1.7	1.1	3.2	40.8	26.8	4.5	225.4	9.3	0.0	0.0	1.1	126.1	100	20.1	1.285
•	a live at the state of the		201	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%		10%	10%	2001	2,00 1	% <u>0</u> 1	
			%0 <u>8</u>	%06	%06	%06	%06	%06	%06	%06	%06	%06	%06	%06	%06	%06	%06	200V	2000	80%	%06	
,		//vacamiang (acies)	318	1,574	1,315	22,369	8,288	422	170	2.192	7.833	6.764	3.116	30,662	1 523	28 021	192	201	102	26,102	12,125	151,189
		#hours wind >= 20 mph rev vacam (and (acres) vasiature resident term in $\frac{1}{2}$ 0.0 m $\frac{1}{2}$	0		0	2	1 ന	5	4		• •		> -						4	4	3	39
Assuming lixed	25-Feb-99	Polygon id letter code	166	2 WW	2 61	2 31 A hr	4 100	1410	7 200	0 4m			10101	D(   1	ud ZL	13 WJ	14 gv	15 CW	16 sa	17 10	18 DV	Total

Table 6-III Design day PM-10 Valley-wide emissions estimate Assuming fixed stable/stabilized ratio

Phase II stabilized land geometric means spike-corrected, not torn up

	6 of lotal	%0.0	0.4%	0.0%	10.6%	5.7%	0.3%	0.2%	0.6%	7.1%	4.7%	0.8%	39.2%	1.6%	%0.0	%0.0	700 0	0.2.0	23.8%	4.9%	100.0%	
·	<u>4-10 (tons) 9</u>	0.0	2.1	0.0	54.4	29.6	1.5	1.0	2.9	36.8	24.1	4.1	202.0	8.3	0.0			<u>-</u>	122.6	25.2	515.6	
	stelolized BA	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	202	202	%NZ	20%	20%		
•	% stable %	80%	80%	80%	80%	80%	80%	80%	80%	80%	80%	80%			80%	200	8 DO	80%	80%	80%		
	A VEIGEN BILLE A BOLESN	318	1.574	1.315	22.369	8,288	422	170	2.192	7.833	6.764	3 116	30.662	1 523	1,020,1	100	182	207	26,102	12.125	151 189	
	athorse and se of much leaving and factes) 1% stable 1% stabilized PM-10 (tons) 1% of total				0	1.60	0	4	•	Ā	~~~	7	- <		0		0	4	4	. 6.	200	100
Assuming inter	20-LEU-89			MM V	0 01	4 05	0 DI 6 m C	7	ر ااای 0 ماسی	HID O		Id DL	D/ LL	12 pm	13 WJ	14 gv	15 CW	16 ca	17 15	01 71	19 00	I otal

Table 7-III Design Day PM-10 Valley-wide emissions estimate Varving stable/stabilized ratio

Phase II stabilized land geometric means spike-corrected, not tom up

			0.0	1,574 70% 30% 1.9 0.4%	1,315 60% 40% 0.0 0.0%	22,369 80% 20% 54.4 10.6%	8,288 80% 20% 29.6 5.8%	422 60% 40% 1.2 0.2%	170 60% 40% 0.8 0.2%	2,192 70% 30% 2.7 0.5%	7,833 80% 20% 36.8 7.2%	6.764 80% 20% 24.1 4.7%	3.116 60% 40% 3.8 0.7%			60% 40% 0.0	207 60% 40% 0.8 0.2%	26,102 80% 20% 122.6 23.9%	12,125 80% 20% 25.2 4.9%	<u>13.4</u> 100.0%
Varying stable/stabilized ratio	25-FeD-99	Polygon (d) letter code  # hours wind >= 20 mph  1	1 cc 0	1 www.c	3 61 0					and a state of the	04			- 1 Ju 	12 0111	15 ~~ 0		17 10 4	18 01/ 3	20

Table 8-III Design day PM-10 Valley-wide emissions estimate

Phase II stabilized land geometric means spike-corrected, not tom up

	Assuming fixed 25-Feb-99	d stable/stabilized ratio 14 mms wind 5-20 mmb inv vacantiland (acres) (% stable % stabilized PM 10 (tons) (% of total	nev vacanti and (acres)	spike-coi % stable	spike-corrected, not torn up % stabile % stabilized PM 10	PM-10 (tens)	% of total
1			318	%02	30%	0.0	%0.0
	2 1000	<b>F</b>	1,574	%02	30%	1.8	0.4%
1 0	3.5	0	1,315	%02		0.0	%0.0
4	4 hs	2	22,369	20%	30%	48.4	10.6%
. 5	5 01	3	8,288	%02		26.3	5.7%
	6 mc	2	422	%02	30%	1.3	0.3%
2	7 ms	4	170	%02	%0E	0.9	0.2%
~ 00	8 dm		2,192	%0/	30%	2.5	0.6%
σ	9 fl	4	7,833	%02	30%	32.7	7.2%
101	12	3	6,764	%02	30%	21.5	4.7%
11 id	id I		3,116		30%	3.6	0.8%
	12 nm	4	30,662	%0/	30%	178.7	39.1%
13	13 wi	3	1,523	%0/	30%	7.4	1.6%
14	14 OV	0	26,021	%0/	30%	0.0	0.0%
5	15 CW	0	192	%02		0.0	%0.0
16	16 sa	4	207	%01	30%		0.2%
17	17 In	4	26,102	%02	30%	109.1	23.9%
	18 nv	3	12,125	%02	30%		4.9%
2	Total	39	151,189			457.3	100.0%
	I CIGI						

Table 9-III 1999 PM-10 Valley-wide emissions estimate Assuming fixed stable/stabilized ratio

Phase II stabilized land geometric means 9/10/2000 spike corrected, not torn up

0.0000	0.0%	0.3%	0.1%	17.5%	6.0%	0.1%	0.0%	0.3%	4.4%	1.6%	0.4%	700 4	0/R./	0.3%	8.4%	0.2%	0.1%	31 1%	24 40	Z1.4%	100.0%
79101(016)) <u>9</u> 4	1.6	36.0	8.5	2,390.1	824.5	8.0	5.2	43.8	598.0	225.3	543		1,0/9.5	42.3	1,143.2	26.9	9.3	A 257 8	0.102,4	2,924.0	13,679.0
<b>Stabilized PN</b>	16%	16%	16%	16%	16%	16%	16%	16%	16%	16%	2027	R 01	16%	16%	16%	16%	16%	1001	<u>%</u> 0	16%	
% stable   %	84%	84%			84%	84%	84%						84%	84%						84%	
vanania ano (acres)	318	1 574	1 315	22.369	8.288	422	170	2 192	7 833	000'1	0'/04	3,116	30,662	1 523	26 021	102	200	102	26,102	12,125	151,189
rest in the stabilized PM-10 (tons) % stable % stabilized PM-10 (tons) % oftotal		10	0	48	24			23	0	RC	26	12	26	00	02	200	77	GE	95	162	694
		1 66	2 ww	3 SI	1000	Id c	6 mc	7 ms	8 dm	9 fl	10 pt	1111		md 21	13 WJ	14 gv	15 CW	16 Sa	17110	10 10	Total

Table 10-III Design day PM-10 Valley-wide emissions estimate Assuming fixed stable/stabilized ratio

Phase II stabilized land geometric means spike-corrected, not torn up

	and the second	Yor OF LOUGH	0.0%	0.4%	0.0%	10.4%	7.1%	0.3%	0.2%	0.5%	7.0%	4.6%	0.8%	38.7%	1.6%	%0.0	0.0%	0.2%	23.4%	4.8%	100.0%
		A Ston of Ma	0.0	2.1	0.0	56.9	38.9	1.6	1.0	3.0	38.4	25.2	4.2	211.4	8.7	0.0	0.0	1.0	128.0	26.4	546.7
		% stabilized	16%	16%	16%	16%	16%	16%	16%	16%	16%	16%	16%	16%	16%	16%	16%	16%	16%	16%	
		% stable	84%	84%	84%	84%	84%	84%	84%	84%		84%	84%		84%		84%	84%	84%	84%	
		revivacant land (acres)	318	1,574	1,315	22,369	8,288	422	170	2.192	7,833	6.764	3.116	30,662	1 523	26.021	192	207	26.102	12.125	-
D Stable/Stablited Latio		#hours wind >= 20 mph /rev vacant and (acres) % stable % stabilized PM=10 (tons)			0	2	3	2	4		4			× ·				4	4	. 6.	39
Assuming lixed	25-Feb-99	Dally are is also fertier and also fer a	100	- 00	2 61	4 hc	5 DI	e re	7 me	2 dm		10 11		11 10	12 pill	1.0 WJ	14 UV 45 Qu	10 CW	10 30	10	Total
		a Data ta																			

Table 1-IV 1999 PM-10 Valley-wide emissions estimate Assuming fixed stable/stabilized ratio

Phase II stabilized land geometric means 9/10/2000 spike corrected, torn up

	0.0%	0.3%	0.1%	17.4%	6.1%	0.1%	0.0%	0.3%	4.4%	1.7%	0.4%	8.0%	0.3%	8.4%	0.2%	0.1%	30.9%	21.5%	100.0%
MARCH (GIRS) = 8/	1.8	40.5	9.5	2,638.0	926.3	0.6	5.8	49.3	6699	253.0	60.4	1.208.4	47.0	1.279.4	27.3	10.5	4,687.1	3,267.0	15,190.0
% stabilized P	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	
% stable	%06	%06	%06	%06	%06	%06													
	318	1 574	1 315	22.369	8.288	422	170	2 192	7.833	6 764	2,116	30.62	1 532	1,020 26 001	197	207	26 102	12.125	151,189
athor serving ser of much revivacant land actes % stable % stabilized PM-10 (tons) % of total		20	) <b>v</b>	48	6 <u>/</u>		23	16	202	20		2	07	07	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	20	33	162	694
1000		3	× 2	3 SI		Id c	6 mc	Sm /	ED 2		10 pt	11 jd	12 pm	13 wj	14 gv	15 cw	16 sa	1/10	18 pv Total

Table 2-IV 1999 PM-10 Valley-wide emissions estimate Assuming fixed stable/stabilized ratio

Phase II stabilized land geometric means 9/10/2000 spike corrected, torn up

ļ

)  <b>26 05 1019</b> ]	1.7 0.0%	.9 0.3%		4 17.1%	.4 6.2%	8.6 0.1%	5.5 0.0%	.3 0.3%			.1 0.4%	.8 8.0%	.7 0.3%	.2 8.5%	.7 0.2%	.0 0.1%		.9 21.6%	.9 100.0%
PM-10 (tons	1.	38.9	9.1	2,462.4	888.4			47.3	639.9	242.3	57.1	1,152.8	44.7	1,220.2	26.7	10.0	4,430.5	3,108.9	14,394.9
% stabilized	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	
% stable	80%	80%	80%	80%	80%	80%	80%	80%	80%	80%	80%	80%	80%	80%	80%	80%	80%	80%	
rev vacant (and (acres)	318	1,574	1,315	22,369	8,288	422	170	2,192	7,833	6,764	3,116	30,662	1,523	26,021	192	207	26,102	12,125	151.189
##nours wind >= 20 mph   rev vacant (and (acres) % stable % stabilized PM-10 (tons) % of total	3	18	5	48	62	14	23	16	59	26	12	26	20	33	20	35	95	162	694
aforate l'efferter sorte service	1 cc	2 ww	<u>3</u> SI	4 hs	5 01	6 mc	7 ms	8 dm	9.6	10 pt	11 id		13 wi	14 OV	15 CW	16 Sa	17 10	18 DV	Total
E CAN ( ) ( )	のないで、そんでいたの																		

Table 4-IV 1999 PM-10 Valley-wide emissions estimate Assuming fixed stable/stabilized ratio

Phase II stabilized land geometric means 9/12/2000 spike corrected, torn up

318
1,574
1,315
22,369
8,288
422
170
2,192
7,833
6,764
3,116
30,662
1,523
26,021
192
207
26,102
12,125
151 189

Table 5-IV Design day PM-10 Valley-wide emissions estimate Assuming fixed stable/stabilized ratio

Phase II stabilized land geometric means spike-corrected, torn up

	% of total	0.0%	0.4%	1.6%	10.5%	5.7%	0.3%	0.2%	0.6%	7.1%	4.7%	0.8%	38.2%	1.6%	0.0%	0.0%	0.2%	23.7%	4.7%	100.0%
2	(suot) ot-ma	0.0	2.4	9.5	63.9	34.7	1.7	1.1	3.4	43.2	28.3	4.7	232.4	9.5	0.0	0.0	1.1	144.1	28.6	608.7
	% stabilized	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	10%	
	% stable	%06	%06	%06	%06	%06	%06	%06	%06	%06	%06	%06	80%	%06	%06	%06	%06	%06	%06	
	rev vacant land (acres)	318	1,574	1,315	22,369	8,288	422	170	2,192	7,833	6,764	3,116	30,662	1,523	26,021	192	207	26,102	12,125	151,189
	# hours wind >= 20 mph   fev vacant/land (acres) % stable   % stabilized PM=10 (tons);  % off total	0	L	0	2	8	2	4	1	4	3	1	4	3	0	0	4	4	3	39
25-Feb-99	a olvoina ol lietter solde	1 66	2 WW	3 si	4 bs	5 pi	6 mc	7 ms	8 dm	9 fl	10 pt	11 jd	12 pm	13 Wj	14 gv	15 cw	16 sa	17 10	18 pv	Total
	POINS																			

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Table 6-IV Design day PM-10 Valley-wide emissions estimate Assuming fixed stable/stabilized ratio

Phase II stabilized land geometric means soike-corrected. torn up

% of total	%0 <sup>.0</sup>	0.4%	%0.0	10.8%	5.9%	0.3%	0.2%	<b>%9</b> .0	7.3%	4.8%	0.8%	38.1%	1.5%	0.0%	%0.0	0.2%	24.4%	4.6%	100.0%
FM-10 (tons)	0.0		0.0	61.4	33.4	1.6	1.1	3.2	41.6	27.2	4.5	216.0	8.8	0.0	0.0	1.1	138.6	26.1	566.8
% stabilized	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	20%	
% stable		80%	80%	%08	80%	80%	80%	%08	80%	80%	80%	80%	80%	80%	80%	80%	80%	80%	
rev vacant land (acres)	318	1,574	1,315	22,369	8,288	422	170	2,192	7,833	6,764	3,116	30,662	1,523	26,021	192	207	26,102	12,125	151,189
# hours wind >= 20 mph	0	1	0	2	3	2	4	1	4	3	1	4	3	0	0	4	4	3	39
yon id lettereede	1 cc	2 ww	3 SI	4 bs	5 pl	6 mc	7 ms	8 dm	9 fl	10 pt	11 jd	12 pm	13 wj	14 gv	15 cw	16 sa	17 lo	18 pv	Total
	Polygon.id letter code ##hours.wind >= 20 mph (rev vacant land (acres) % stable % stabilized PM-10 (tons) % of total	# hours wind >= 20 mph frev vacant land (acres) % stabilized PM-10 (tons) % of 318 80% 20% 0.0	# hours wind >= 20 mph         rev vacant land (acres) % stabile         % stabilized PW-10 (tons) % of           0         318         80%         20%         0.0           1         1,574         80%         20%         2.3	# hours wind >= 20 mph         rev vacant land (acres) % stable         % stable         % stable         % stable         % stable         % of         0 0.0         0         0.0         0         0.0         0         0.0         0.0         0.0         0         0.0 <th># hours wind &gt;= 20 mph         rev vacant land (acres) % stable         % stabilized PM-10 (tons)         % of           0         318         80%         20%         0.0           1         1,574         80%         20%         2.3           0         0         1,315         80%         20%         2.3           1         1,315         80%         20%         0.0         2.3           2         22,369         80%         20%         61.4         1</th> <th># hours wind ≥= 20 mph         rev vacant land (acres)         % stable         % stabilized         PM-10 (tons)         % of           0         318         80%         20%         0.0         0</th> <th># hours wind ≥= 20 mph         rev vacant land (acres) % stabile         % stabilized PM=10 (fons) % of           0         318         80%         20%         0.0           1         1,574         80%         20%         2.3           0         1,574         80%         20%         2.3           1         1,574         80%         20%         2.3           2         22,369         80%         20%         61.4         1           3         8,288         80%         20%         33.4         1.6           2         422         80%         20%         1.6         1.6         1.6</th> <th># hourswind &gt;= 20 mph         rev vacant land (acres)         % stabilized         PM-10 (tons)         % 01           0         318         80%         20%         0.0         0</th> <th># hours wind &gt;= 20 mph         rev vacant land (acres)         % stabilized         PM-10 (tons)         % 01           0         318         80%         20%         0.0         0</th> <th># hours wind <math>2 = 20</math> mph         rev vacant land (acres)         % stabilized         PM-10 (tons)         % 01           0         0         318         80%         20%         0.0           1         1,574         80%         20%         2.3         2.3           1         1,574         80%         20%         2.3         2.3           1         1,574         80%         20%         0.0         0           2         2         22,369         80%         20%         61.4         1           3         8,288         80%         20%         33.4         1.6         1.6         1.6         1.6         1.6         1.6         1.6         1.1         1.6         1.6         1.1         1.6         1.6         1.6         1.6         1.1         1.6         1.1         1.6         1.1         1.6         1.1         1.6         1.1         1.1         1.6         1.1         1.1         1.6         1.1         1.1         1.6         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1<th># hourswind <math>\geq 20</math> mph         rev vacant land (acres)         % stabilized         PM-10 (tons)         % of           0         0         318         80%         20%         0.0           1         1,574         80%         20%         2.3           0         0         1,315         80%         20%         2.3           1         1,315         80%         20%         0.0         0           2         2         22,369         80%         20%         61.4         1           3         8,288         80%         20%         33.4         16           1         2         80%         20%         33.4         16           1         2         80%         20%         16         16           1         2,192         80%         20%         3.2         3.2           1         2,192         80%         20%         41.6         3.2           1         3         6,764         80%         20%         41.6         3.2</th><th># hourswind <math>\geq 20</math> mph         rev vacant land (acres) % stabilized PM-10 (tons) % of           0         318         <math>80\%</math> <math>20\%</math> <math>0.0</math>           1         1,574         <math>80\%</math> <math>20\%</math> <math>0.0</math>           0         0         1,574         <math>80\%</math> <math>20\%</math> <math>2.3</math>           1         1,574         <math>80\%</math> <math>20\%</math> <math>0.0</math> <math>0.0</math>           1         1         1,574         <math>80\%</math> <math>20\%</math> <math>0.0</math> <math>0.0</math>           2         2         <math>20\%</math> <math>20\%</math> <math>2.3</math> <math>0.0</math> <math>0.0</math>           2         2         <math>2.369</math> <math>80\%</math> <math>20\%</math> <math>0.0</math> <math>0.0</math>           2         2         <math>2.369</math> <math>80\%</math> <math>20\%</math> <math>0.0</math> <math>0.0</math>           2         2         <math>2.2369</math> <math>80\%</math> <math>20\%</math> <math>1.6</math> <math>1.6</math>           2         2         <math>2.20\%</math> <math>2.0\%</math> <math>1.6</math> <math>3.2.4</math> <math>1.6</math>           2         2         <math>422</math> <math>80\%</math> <math>20\%</math> <math>2.0\%</math> <math>3.2</math>           2         2         <math>423</math> <math>80\%</math> <math>2.0\%</math> <math>2.1.6</math></th><th># hourswind <math>2 = 20</math> mph         rev vacant land (acres) % stabilized PM-10 (tons) % of 318         % stabilized PM-10 (tons) % of 318         80%         20%         0.0         90%         0.0         90%         0.0         90%         0.0         90%         0.0         90%         0.0         90%         0.0         90%         0.0         0.0         90%         20%         0.0         0.0         90%         2.0         0.0         90%         2.0         0.0         90%         2.0         0.0         90%         2.0         0.0         90%         2.0         0.0         90%         2.0         0.0         90%         0.0         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         20%         41.6         90%         21.6         90%         21.6         90%         21.6         90%         21.6         90%         21.6         90%         90%         21.6         90%         21.6         90%         90%         21.6         90%         21.6         90%         21.6         90%         21.6         90%         21.6         90%         21.6</th><th># hourswind <math>2 = 20</math> mph         rev vacant land (acres)         % stabilized         PM-10 (tons)         % 01           0         0         0         318         80%         20%         0.0           1         1,574         80%         20%         2.3         2.3           1         1,574         80%         20%         0.0         0           1         1,574         80%         20%         0.1         1           2         2         23,569         80%         20%         61.4         1           2         2         22,369         80%         20%         1.6         1.1           2         2         22,369         80%         20%         3.4         1.6           1         2         2         22,369         80%         20%         1.6         1.6           1         2         2         2         2         2         3.3.4         1.6         1.1           1         2         2         2         2         2         3         2         2         2         2         2         2         2         2         2         2         2         2         2</th><th># hours wind &gt;= 20 mph         rev vacant land (acres) % stable % stablized PM 10 (fons) % of           0         0         318         80%         20%         0.0           1         1,574         80%         20%         2.3           2         2         23.69         80%         20%         61.4         1           1         1,574         80%         20%         0.0         0         0           2         2         22,369         80%         20%         61.4         1           2         3         8,288         80%         20%         61.4         1           2         1         2         80%         20%         33.4         1.6           2         1         1         2,192         80%         20%         3.1         4.1.6           2         3         6,764         80%         20%         3.2         4.5         3.2           3         6,764         80%         20%         20%         4.5         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2</th><th># hours wind &gt; 20 mph         rev vacant land (acres)         % stable         % stablized         PM 400 (tonis)         % sol           <math>1</math> <math>1</math> <math>1,574</math> <math>80\%</math> <math>20\%</math> <math>0.0</math> <math>0.0</math> <math>1</math> <math>1</math> <math>1,574</math> <math>80\%</math> <math>20\%</math> <math>0.0</math> <math>0.0</math> <math>0</math> <math>0</math> <math>1,315</math> <math>80\%</math> <math>20\%</math> <math>0.0</math> <math>0.0</math> <math>2</math> <t< th=""><th># hours winds         Z0 mph         rev vacantiand (acres)         % stablized         PM f0(tons)         % stablized         PM f0         0.0         0&lt;</th><th># hours wind &gt; 20 mph         rev vacant land (acres)         % stable         % stablized PM 10 (tons)         % of           1         1         1,574         80%         20%         0.0           1         1,574         80%         20%         0.0           2         2         23.8         80%         20%         0.1           1         1,574         80%         20%         0.0         0.0           2         2         22,369         80%         20%         61.4         1           1         2         80%         20%         0.0         0.0         0.0           2         3         80%         20%         61.4         1           1         2         80%         20%         3.1.6         3.2.2           1         2,192         80%         20%         41.6         3.2.2           1         2,192         80%         20%         2.7.2         3.2.2           1         3,116         80%         20%         2.7.2         3.2.2           1         3,116         80%         20%         2.16.0         3.2           1         3,116         80%         20%</th><th># hours wind &gt; 20 mb(t)         Tev vacant land (acres)         % stable         % stable</th></t<></th></th>	# hours wind >= 20 mph         rev vacant land (acres) % stable         % stabilized PM-10 (tons)         % of           0         318         80%         20%         0.0           1         1,574         80%         20%         2.3           0         0         1,315         80%         20%         2.3           1         1,315         80%         20%         0.0         2.3           2         22,369         80%         20%         61.4         1	# hours wind ≥= 20 mph         rev vacant land (acres)         % stable         % stabilized         PM-10 (tons)         % of           0         318         80%         20%         0.0         0	# hours wind ≥= 20 mph         rev vacant land (acres) % stabile         % stabilized PM=10 (fons) % of           0         318         80%         20%         0.0           1         1,574         80%         20%         2.3           0         1,574         80%         20%         2.3           1         1,574         80%         20%         2.3           2         22,369         80%         20%         61.4         1           3         8,288         80%         20%         33.4         1.6           2         422         80%         20%         1.6         1.6         1.6	# hourswind >= 20 mph         rev vacant land (acres)         % stabilized         PM-10 (tons)         % 01           0         318         80%         20%         0.0         0	# hours wind >= 20 mph         rev vacant land (acres)         % stabilized         PM-10 (tons)         % 01           0         318         80%         20%         0.0         0	# hours wind $2 = 20$ mph         rev vacant land (acres)         % stabilized         PM-10 (tons)         % 01           0         0         318         80%         20%         0.0           1         1,574         80%         20%         2.3         2.3           1         1,574         80%         20%         2.3         2.3           1         1,574         80%         20%         0.0         0           2         2         22,369         80%         20%         61.4         1           3         8,288         80%         20%         33.4         1.6         1.6         1.6         1.6         1.6         1.6         1.6         1.1         1.6         1.6         1.1         1.6         1.6         1.6         1.6         1.1         1.6         1.1         1.6         1.1         1.6         1.1         1.6         1.1         1.1         1.6         1.1         1.1         1.6         1.1         1.1         1.6         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1 <th># hourswind <math>\geq 20</math> mph         rev vacant land (acres)         % stabilized         PM-10 (tons)         % of           0         0         318         80%         20%         0.0           1         1,574         80%         20%         2.3           0         0         1,315         80%         20%         2.3           1         1,315         80%         20%         0.0         0           2         2         22,369         80%         20%         61.4         1           3         8,288         80%         20%         33.4         16           1         2         80%         20%         33.4         16           1         2         80%         20%         16         16           1         2,192         80%         20%         3.2         3.2           1         2,192         80%         20%         41.6         3.2           1         3         6,764         80%         20%         41.6         3.2</th> <th># hourswind <math>\geq 20</math> mph         rev vacant land (acres) % stabilized PM-10 (tons) % of           0         318         <math>80\%</math> <math>20\%</math> <math>0.0</math>           1         1,574         <math>80\%</math> <math>20\%</math> <math>0.0</math>           0         0         1,574         <math>80\%</math> <math>20\%</math> <math>2.3</math>           1         1,574         <math>80\%</math> <math>20\%</math> <math>0.0</math> <math>0.0</math>           1         1         1,574         <math>80\%</math> <math>20\%</math> <math>0.0</math> <math>0.0</math>           2         2         <math>20\%</math> <math>20\%</math> <math>2.3</math> <math>0.0</math> <math>0.0</math>           2         2         <math>2.369</math> <math>80\%</math> <math>20\%</math> <math>0.0</math> <math>0.0</math>           2         2         <math>2.369</math> <math>80\%</math> <math>20\%</math> <math>0.0</math> <math>0.0</math>           2         2         <math>2.2369</math> <math>80\%</math> <math>20\%</math> <math>1.6</math> <math>1.6</math>           2         2         <math>2.20\%</math> <math>2.0\%</math> <math>1.6</math> <math>3.2.4</math> <math>1.6</math>           2         2         <math>422</math> <math>80\%</math> <math>20\%</math> <math>2.0\%</math> <math>3.2</math>           2         2         <math>423</math> <math>80\%</math> <math>2.0\%</math> <math>2.1.6</math></th> <th># hourswind <math>2 = 20</math> mph         rev vacant land (acres) % stabilized PM-10 (tons) % of 318         % stabilized PM-10 (tons) % of 318         80%         20%         0.0         90%         0.0         90%         0.0         90%         0.0         90%         0.0         90%         0.0         90%         0.0         90%         0.0         0.0         90%         20%         0.0         0.0         90%         2.0         0.0         90%         2.0         0.0         90%         2.0         0.0         90%         2.0         0.0         90%         2.0         0.0         90%         2.0         0.0         90%         0.0         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         20%         41.6         90%         21.6         90%         21.6         90%         21.6         90%         21.6         90%         21.6         90%         90%         21.6         90%         21.6         90%         90%         21.6         90%         21.6         90%         21.6         90%         21.6         90%         21.6         90%         21.6</th> <th># hourswind <math>2 = 20</math> mph         rev vacant land (acres)         % stabilized         PM-10 (tons)         % 01           0         0         0         318         80%         20%         0.0           1         1,574         80%         20%         2.3         2.3           1         1,574         80%         20%         0.0         0           1         1,574         80%         20%         0.1         1           2         2         23,569         80%         20%         61.4         1           2         2         22,369         80%         20%         1.6         1.1           2         2         22,369         80%         20%         3.4         1.6           1         2         2         22,369         80%         20%         1.6         1.6           1         2         2         2         2         2         3.3.4         1.6         1.1           1         2         2         2         2         2         3         2         2         2         2         2         2         2         2         2         2         2         2         2</th> <th># hours wind &gt;= 20 mph         rev vacant land (acres) % stable % stablized PM 10 (fons) % of           0         0         318         80%         20%         0.0           1         1,574         80%         20%         2.3           2         2         23.69         80%         20%         61.4         1           1         1,574         80%         20%         0.0         0         0           2         2         22,369         80%         20%         61.4         1           2         3         8,288         80%         20%         61.4         1           2         1         2         80%         20%         33.4         1.6           2         1         1         2,192         80%         20%         3.1         4.1.6           2         3         6,764         80%         20%         3.2         4.5         3.2           3         6,764         80%         20%         20%         4.5         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2</th> <th># hours wind &gt; 20 mph         rev vacant land (acres)         % stable         % stablized         PM 400 (tonis)         % sol           <math>1</math> <math>1</math> <math>1,574</math> <math>80\%</math> <math>20\%</math> <math>0.0</math> <math>0.0</math> <math>1</math> <math>1</math> <math>1,574</math> <math>80\%</math> <math>20\%</math> <math>0.0</math> <math>0.0</math> <math>0</math> <math>0</math> <math>1,315</math> <math>80\%</math> <math>20\%</math> <math>0.0</math> <math>0.0</math> <math>2</math> <t< th=""><th># hours winds         Z0 mph         rev vacantiand (acres)         % stablized         PM f0(tons)         % stablized         PM f0         0.0         0&lt;</th><th># hours wind &gt; 20 mph         rev vacant land (acres)         % stable         % stablized PM 10 (tons)         % of           1         1         1,574         80%         20%         0.0           1         1,574         80%         20%         0.0           2         2         23.8         80%         20%         0.1           1         1,574         80%         20%         0.0         0.0           2         2         22,369         80%         20%         61.4         1           1         2         80%         20%         0.0         0.0         0.0           2         3         80%         20%         61.4         1           1         2         80%         20%         3.1.6         3.2.2           1         2,192         80%         20%         41.6         3.2.2           1         2,192         80%         20%         2.7.2         3.2.2           1         3,116         80%         20%         2.7.2         3.2.2           1         3,116         80%         20%         2.16.0         3.2           1         3,116         80%         20%</th><th># hours wind &gt; 20 mb(t)         Tev vacant land (acres)         % stable         % stable</th></t<></th>	# hourswind $\geq 20$ mph         rev vacant land (acres)         % stabilized         PM-10 (tons)         % of           0         0         318         80%         20%         0.0           1         1,574         80%         20%         2.3           0         0         1,315         80%         20%         2.3           1         1,315         80%         20%         0.0         0           2         2         22,369         80%         20%         61.4         1           3         8,288         80%         20%         33.4         16           1         2         80%         20%         33.4         16           1         2         80%         20%         16         16           1         2,192         80%         20%         3.2         3.2           1         2,192         80%         20%         41.6         3.2           1         3         6,764         80%         20%         41.6         3.2	# hourswind $\geq 20$ mph         rev vacant land (acres) % stabilized PM-10 (tons) % of           0         318 $80\%$ $20\%$ $0.0$ 1         1,574 $80\%$ $20\%$ $0.0$ 0         0         1,574 $80\%$ $20\%$ $2.3$ 1         1,574 $80\%$ $20\%$ $0.0$ $0.0$ 1         1         1,574 $80\%$ $20\%$ $0.0$ $0.0$ 2         2 $20\%$ $20\%$ $2.3$ $0.0$ $0.0$ 2         2 $2.369$ $80\%$ $20\%$ $0.0$ $0.0$ 2         2 $2.369$ $80\%$ $20\%$ $0.0$ $0.0$ 2         2 $2.2369$ $80\%$ $20\%$ $1.6$ $1.6$ 2         2 $2.20\%$ $2.0\%$ $1.6$ $3.2.4$ $1.6$ 2         2 $422$ $80\%$ $20\%$ $2.0\%$ $3.2$ 2         2 $423$ $80\%$ $2.0\%$ $2.1.6$	# hourswind $2 = 20$ mph         rev vacant land (acres) % stabilized PM-10 (tons) % of 318         % stabilized PM-10 (tons) % of 318         80%         20%         0.0         90%         0.0         90%         0.0         90%         0.0         90%         0.0         90%         0.0         90%         0.0         90%         0.0         0.0         90%         20%         0.0         0.0         90%         2.0         0.0         90%         2.0         0.0         90%         2.0         0.0         90%         2.0         0.0         90%         2.0         0.0         90%         2.0         0.0         90%         0.0         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         90%         20%         41.6         90%         21.6         90%         21.6         90%         21.6         90%         21.6         90%         21.6         90%         90%         21.6         90%         21.6         90%         90%         21.6         90%         21.6         90%         21.6         90%         21.6         90%         21.6         90%         21.6	# hourswind $2 = 20$ mph         rev vacant land (acres)         % stabilized         PM-10 (tons)         % 01           0         0         0         318         80%         20%         0.0           1         1,574         80%         20%         2.3         2.3           1         1,574         80%         20%         0.0         0           1         1,574         80%         20%         0.1         1           2         2         23,569         80%         20%         61.4         1           2         2         22,369         80%         20%         1.6         1.1           2         2         22,369         80%         20%         3.4         1.6           1         2         2         22,369         80%         20%         1.6         1.6           1         2         2         2         2         2         3.3.4         1.6         1.1           1         2         2         2         2         2         3         2         2         2         2         2         2         2         2         2         2         2         2         2	# hours wind >= 20 mph         rev vacant land (acres) % stable % stablized PM 10 (fons) % of           0         0         318         80%         20%         0.0           1         1,574         80%         20%         2.3           2         2         23.69         80%         20%         61.4         1           1         1,574         80%         20%         0.0         0         0           2         2         22,369         80%         20%         61.4         1           2         3         8,288         80%         20%         61.4         1           2         1         2         80%         20%         33.4         1.6           2         1         1         2,192         80%         20%         3.1         4.1.6           2         3         6,764         80%         20%         3.2         4.5         3.2           3         6,764         80%         20%         20%         4.5         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2	# hours wind > 20 mph         rev vacant land (acres)         % stable         % stablized         PM 400 (tonis)         % sol $1$ $1$ $1,574$ $80\%$ $20\%$ $0.0$ $0.0$ $1$ $1$ $1,574$ $80\%$ $20\%$ $0.0$ $0.0$ $0$ $0$ $1,315$ $80\%$ $20\%$ $0.0$ $0.0$ $2$ <t< th=""><th># hours winds         Z0 mph         rev vacantiand (acres)         % stablized         PM f0(tons)         % stablized         PM f0         0.0         0&lt;</th><th># hours wind &gt; 20 mph         rev vacant land (acres)         % stable         % stablized PM 10 (tons)         % of           1         1         1,574         80%         20%         0.0           1         1,574         80%         20%         0.0           2         2         23.8         80%         20%         0.1           1         1,574         80%         20%         0.0         0.0           2         2         22,369         80%         20%         61.4         1           1         2         80%         20%         0.0         0.0         0.0           2         3         80%         20%         61.4         1           1         2         80%         20%         3.1.6         3.2.2           1         2,192         80%         20%         41.6         3.2.2           1         2,192         80%         20%         2.7.2         3.2.2           1         3,116         80%         20%         2.7.2         3.2.2           1         3,116         80%         20%         2.16.0         3.2           1         3,116         80%         20%</th><th># hours wind &gt; 20 mb(t)         Tev vacant land (acres)         % stable         % stable</th></t<>	# hours winds         Z0 mph         rev vacantiand (acres)         % stablized         PM f0(tons)         % stablized         PM f0         0.0         0<	# hours wind > 20 mph         rev vacant land (acres)         % stable         % stablized PM 10 (tons)         % of           1         1         1,574         80%         20%         0.0           1         1,574         80%         20%         0.0           2         2         23.8         80%         20%         0.1           1         1,574         80%         20%         0.0         0.0           2         2         22,369         80%         20%         61.4         1           1         2         80%         20%         0.0         0.0         0.0           2         3         80%         20%         61.4         1           1         2         80%         20%         3.1.6         3.2.2           1         2,192         80%         20%         41.6         3.2.2           1         2,192         80%         20%         2.7.2         3.2.2           1         3,116         80%         20%         2.7.2         3.2.2           1         3,116         80%         20%         2.16.0         3.2           1         3,116         80%         20%	# hours wind > 20 mb(t)         Tev vacant land (acres)         % stable         % stable

Table 7-IV Design Day PM-10 Valley-wide emissions estimate Varving stable/stabilized ratio

Phase II stabilized land geometric means spike-corrected. torn up

	6 of total	0.0%	0.3%	%0.0	10.9%	5.9%	0.2%	0.1%	0.5%	7.4%	4.8%	0.7%	38.4%	1.3%	%0.0	%0.0	0.1%	24.6%	4.6%	100.0%
dn	6 (Suot) of Me	0.0	1.9	0.0	61.4	33.4	1.2	0.8	2.7	41.6	27.2	3.8	216.0	7.5	0.0	0.0	0.8	138.6	26.1	562.9
spike-correctea, torn up	% stabilized	40%	30%	40%	20%	20%	40%	40%	30%	20%	20%	40%	20%	30%	20%	40%	40%	20%	20%	
spike-cor	% stable	%09	%02	%09	80%	80%	%09	%09	%02	80%	80%	%09	80%	20%	80%	%09	%09	80%	80%	
	rev vacant land (acres)	318	1,574	1,315	22,369	8,288	422	170	2,192	7,833	6,764	3,116	30,662	1,523	26,021	192	207	26,102	12,125	151,189
/stadilized fatio	#hours wind >= 20 mph frev vacant land (acres) % stable: % stabilized PM-10 (tons) % of (otal	0	1	0	2	3	2	4	1	4	3	ŀ	4	3	0	0	4	4	3	39
varying stable/s 25-Feb-99	Polygon id listick code	1 00	2 ww	3 SI	4 bs	5 pl	6 mc	7 ms	8 dm	9 fi	10 pt	11 jd	12 pm	13 wj	14 gv	15 CW	16 sa	17 lo	18 pv	Totai

.

Table 8-IV Design day PM-10 Valley-wide emissions estimate Assuming fixed stable/stabilized ratio

Phase II stabilized land geometric means spike corrected, torn-up

plilzed ratio spike corrected, torn-up	# nonrewind $\geq 20$ mole tex vacant and factes) % stable 1% stabilized PM-10 (tons). % of total	0 318 70% 30% 0.0%	1 1,574 70% 30% 2.2 0.4%	0 1,315 70% 30% 0.0 0.0%	2 22,369 70% 30% 58.9 11.0%	3 8,288 70% 30% 32.0 6.0%	2 422 70% 30% 1.5 0.3%		1 2,192 70% 30% 3.1 0.6%	4 7,833 70% 30% 39.9 7.5%	3 6,764 70% 30% 26.1 4.9%	1 3,116 70% 30% 4.3 0.8%	30% 199.6 3	3 1,523 70% 30% 8.0 1.5%	0 26,021 70% 30% 0.0 0.0%	0 192 70% 30% 0.0 0.0%	4         207         70%         30%         1.1         0.2%	<b>4</b> 26,102 70% 30% 133.0 24.9%	3 12,125 70% 30% 23.5 4.4%	39 151 189 151 180 151 100 0%
	Bind Acres 1	318	1,574	1,315	22,369	8,288	422	170	2,192	7,833	6,764	3,116	30,662	1,523	26,021	192	207	26,102	12,125	151 189
	The Viole and	0	-	0	2	e	2	4	F	4	3	1	4	3	0	0	4	4	3	σ
d stadie/stadilized fatio																				C
Assuming fixed	2014001 in lietter code	8	2 ww	sl	4 bs	pl	6 mc	7 ms	8 dm	A	pt	þį	12 pm	wj	٥v	CW	sa	0	pv	Total
	UNION STEP	1	2	3 5	4	5 pl	9	7	Ø	9 8	10 pt	11 jd	12	13 Wj	14 gv	15 CW	16 sa	17 10	18 pv	

,

Table 9-IV 1999 PM-10 Valley-wide emissions estimate Assuming fixed stable/stabilized ratio

Phase II stabilized land geometric means 9/10/2000 spike corrected, torn up

S	318	84% 16%	6 1.7	0.0%
18	1,574	84% 16%	6 39.5	0.3%
5	1,315	84% 16%	6 9.3	0.1%
48	22,369	84% 16%	2,532.6	17.2%
62	8,288	84% 16%	6 903.6	6.1%
14	422	84% 16%	6 8.7	0.1%
23	170	84% 16%	5.6	0.0%
16	2,192	84% 16%	6 48.1	0.3%
59	7,833	84% 16%	651.9	4.4%
26	6,764	84% 16%	246.6	1.7%
12	3,116	84% 16%	58.4	0.4%
26	30,662	84% 16%	6 1,175.0	8.0%
20	1,523	84% 16%	6 45.6	0.3%
33	26,021	84% 16%	6 1,243.9	8.5%
20	192	84% 16%	6 26.9	0.2%
35	207	84% 16%	6 10.2	0.1%
95	26,102	84% 16%	6 4,533.1	30.8%
162	12,125	84% 16%	6 3,172.1	21.6%
604	151 180		14 712 9	100 0%

Table 10-IV Design day PM-10 Valley-wide emissions estimate Assuming fixed stable/stabilized ratio

Phase II stabilized land geometric means spike-corrected, torn up

25-Feb-99						
Polygon id letter code	# hourswind >= 20 mph [rev/vacant land (acres)]% stable [% stable/PM-10 (tons)]% of total	Fev vacant land (acres)	% stable	% stabilized	(suot) of Mc	6 of total
8	0	318	84%	16%	0.0	0.0%
2 ww	L I	1,574	84%	16%	2.3	0.4%
3 SI	0	1,315	84%	16%	0.0	%0.0
4 bs	8	22,369	84%	16%	62.4	10.8%
5 pl	8	8,288	84%	16%	33.9	5.8%
6 mc	2	422	84%	16%	1.7	0.3%
7 ms	4	170	84%	16%	1.1	0.2%
8 dm	L	2,192	84%	16%	3.3	0.6%
9 fl	4	7,833	84%	16%	42.2	7.3%
10 pt	8	6,764	84%	16%	27.7	4.8%
11 jd	1	3,116	84%	16%	4.6	0.8%
12 pm	4	30,662	84%	16%	222.5	38.4%
13 wj	3	1,523	84%	16%	9.1	1.6%
14 gv	0	26,021	84%	16%	0.0	0.0%
15 CW	0	192	84%	16%	0.0	0.0%
16 sa	4	207	84%	16%	1.1	0.2%
17 10	4	26,102	84%	16%	140.8	24.3%
18 pv	3	12,125	84%	16%	27.1	4.7%
Total	39	151,189			579.8	100.0%

lized		0.16	3579.04		Emission: Total	ton tons	0.02 30.42	0.02 30.42	26.42	26.42	26.42	26.42	0.02 30.42	26.42	26.42	26.42	26.42	26.42	26.42	26.42	26.42		0.02 30.42		0.02 30.42		0.02 30.42	26.42	61.10		0.02 30.42		0.02 30.42	26.42				0.02 30.42	26.42	0.02 30.42		0.36 58.25
Stabilized Stabilized			35			230	4.59E-06	4.59E-06					4.59E-06									4.59E-06	4.59E-06		4.59E-06		4.59E-06			_	4.59E-06		4.59E-06			4.59E-06	4.59E-06	4.59E-06		4.59E-06		1.00E-04
Stabilized Stat		0.16	3579.04				0.49 4.5	0.49 4.5	0.49	0.49	0,49	0.49	0.49 4.5	0.49	0.49	0.49	0.49	0.49	0.49	0.49	0.49	0.49 4.5		0.49				0.49	1.73		0.49 4.5			0.49	0.49					0.49 4.5		0.39 1.0
Stabilized Sta				Steady S			1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	4.83E-04	1.09E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.09E-04
Stable S		0.84	18789.96	Spike			3.98	3.98					3.98	•		•				-		3.98	3.98		3.98	-	3.98		-		3.98		3.98					3.98		3.98		9.21
Stable				Spike		1.50	2.12E-04	2.12E-04					2.12E-04									2.12E-04	2.12E-04		2.12E-04		2.12E-04				2.12E-04		2.12E-04			2.12E-04	2.12E-04	2.12E-04		2.12E-04		A ODF-DA
Stable		0.84	18789.96	Steady	Emission	ton	25.93	25.93	25.93	25.93	25.93	25.93	25.93	25.93	25.93	25.93	25.93	25.93	25.93	25.93	25.93	25.93	25.93	25.93	25.93	25.93	25.93	25.93	59.38	48.29	25.93	25.93	25.93		25.93	25.93	25.93	25.93	25.93	25.93	25.93	48.20
Stable				Steady	A.Factor	(ton/acthr)	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03		1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03		3.16E-03	2.57E-03	1.38E-C3		1.38E-03	1.38E-03	1.365-03	1.38E-03	1.38E-03		1.38E-03	1.38E-03	1.38E-03	2 57E_03
		fraction	Area (acres)		A STATE OF A	(itam) brite	20	21.5	22.20001	23.20001	21.9	21.6	21.299999	20.799999	22.299999	21.700001	22.9	22.9	22	23	20.1	20.5	20.4	20.1	21.5	21	20.799999	24.1	31.9	28	21.5	21.9	20.799999	20.20001	21	20.1	21.1	23	20	20.4	21	77 200000
	acres		1			CUT DOI		492	493	494	495 85	496	<b>36</b> 2	67	886 86	696 0	970	126	679	974	975	1239	1333	1334	2125	2126	2150	2151	2152	2153	2270	2271	2355	2358	2360	2441	3502	4558	4559	4676	4678	CVC9
		0.84	0.16			Hour		12	13	14	15	16	2	7	80	6	10	11	13	14	15	15	13	14	13	14	14	15	16	17	14	15	e	9	8	17	ន	ន	ន	8	ឌ	6
1999	vacant land area	stable fraction	unstable fraction			Dave Dave and a local second		21	21	21	21	21	10	10	10	10	10	10	10	9	10	21	8	25	ଚ	30	31	31	31	31	5	2	5	6	o	12	26	ס	0	4	14	18
	Polygon 4 V					Manth	1	-	-	-	1	-	2	2	2	2	7	2	7	2	N	7	2	2	n	3	e	3	e	3	4	4	4	4	4	4	5	2	7	7	7	o

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Stabilized soil, spike-corrected emission factors

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Table A.2 - Polygon CCHD Station bs

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Station
CHD
<b>.</b>
Polygon ;
-2-
Table A

101	24	P	7036	34 599998	3.16E-03	59.38	5.88E-04	11.05	4.83E-04	1.73	1.00E-04	0.36	72.51
2	3	0	7785	20.5	1.38E-03	25.93	2.12E-04	3.98	1.38E-04	0.49	4.59E-06	0.02	30.42
	3	¢ ¢	7786	21 700001	1.38E-03	25.93			1.38E-04	0.49			26.42
	17	14	8030	23.799999	1.38E-03	25.93	2.12E-04	3.98	1.38E-04	0.49	4.59E-06	0.02	30.42
10	+-	15	8031	20.9	1.38E-03	25.93			1.38E-04	0.49			26.42
1 5	- 6.	8	8072	20.700001	1.38E-03	25.93	2.12E-04	3.98	1.38E-04	0.49	4.59E-06	0.02	30.42
15	) er	σ	8073	21.1	1.38E-03	25.93			1.38E-04	0.49			26.42
12	2	200	8180	25.4	2.57E-02	482.90	4.90E-04	9.21	1.09E-04	0.39		0.00	492.50
10		38	8182	25 799999	2.57E-02	482.90			1.09E-04	0.39			483.29
4 4	-	318	8183	20.6	1 38F-03	25,93			1.38E-04	0.49			26.42
12		24		21	1.38E-03	25.93			1.38E-04	0.49			26.42
	•	i											
	_												2390.14
Total													

					Total	tons	0.82	0.38	0.43	1.63			
Stabilized		0.16	50.8	Spike	Emission	ton ⇒	0.00		0.00	 			
Stabilized Stabilized Stabilized Stabilized				Spike	Factor	(ton/ac)			4.59E-06				
Stabilized		0.16	50.8	Steady	Emission	tion .	0.01	0.01	0.01				
Stabilized				Steady	Factor	(ton(achr)	1.09E-04	1.38E-04	1.38E-04				
Stable		0.84	266.7	Spike	Factor Emission Factor	tot	0.13		0.06				
Stable				Spike	Factor	(ton/ac)	4.90E-04		2.12E-04				
Stable		0.84	266.7	Steady	12.15	- ton	0.69	0.37	0.37				
Stable				Steady	Factor	(ton/ac/hr)	2.57E-03	1.38E-03	1.38E-03				
		fraction	Area (acres)		の対象ななない。	wind (mph) [(top)acht] (on [(onlac)] ton [(toplacht)] ton [(toplacht)]	25.200001	21.5	20.6				
	acres				and the state of the second second		2152	2153	8180				
	317.5 acres	0.84	0.16			Hour	16	17	ଷ				
1999	vacant land area	stable fraction	unstable fraction			A Day and	31	31	7				
CC PM-10	Polygon 1					Month	e	e	12	Total			

Table A.3. - Polygon 1 - CCHD Station cc

1999				Stable	Stable	Stable	Stable	Stabilized	Stabilized	Stabilized Stabilized Stabilized Stabilized	Stabilized	
vacant land area		acres									1	
stable fraction	0.84		fraction		0.84		0.84		0.16		0.16	
unstable fraction	0.16		Area (acres)		161.28		161.28		30.72		30.72	
				Steady	Steady	Spike	Spike	Steady	Steady	Spike	Spike	
A CONTRACTOR			の行うのないないないないない	Eactor	Enission		Emission	Factor	Emission	( )Eactor	Emission	Total
Dav	Hour	Cum hour	Mind (mph)	(torvac/hr)	ton	(ton/ac)	ton	(tion/ac/hr)	on in	((job/jec))	ton -	tons
2	20	2924	35.90002	2.99E-03	0.48	9.24E-04	0.15	3.32E-04	0.01		0	0.64
2		2925	50	F	1.77			6.30E-03	0.19			1.97
2	22	2926	50	1.10E-02	1.77			6.30E-03	0.19			1.97
2		2927	49.599998	7.58E-03	1.22			6.30E-03	0.19			1.42
กี		2928	48.900002	1	1.22			6.30E-03	0.19			1.42
6		2929	47.700001	7.58E-03	1.22			6.30E-03	0.19			1.42
e	2	2930	47.099998	7.58E-03				6.30E-03	0.19			1.42
B	8	2931	47	7.58E-03	1.22			6.30E-03	0.19			1.42
e		2932	46.099998	7.58E-03	1.22			6.30E-03	0.19			1.42
6			45.799999	7.58E-03	1.22			6.30E-03	0.19			1.42
3	9		45.799999	7.58E-03	1.22			6.30E-03	0.19			1.42
ю Ю			45.900002	7.58E-03	1.22			6.30E-03	0.19			1.42
ю́	8	2936	45.5	7.58E-03	1.22			6.30E-03	0.19			1.42
3	6	2937	45.299999		1.22			6.30E-03	0.19			1.42
3	10		45.400002	7.58E-03	1.22			6.30E-03	0.19			1.42
3	11	2939	45.20001	7.58E-03	1.22			6.30E-03	0.19			1.42
3	12		44.200001	5.92E-03	0.95			6.30E-03	0.19			1.15
3	13	2941	43.90002	5.92E-03	0.95			6.30E-03	0.19			1.15
3	14		43.299999	5.92E-03	0.95			6.30E-03	0.19			1.15
3	15		39.90002	2.99E-03	0.48			3.32E-04	0.01			0.49
												26.92

Table A.4 - Polygon 15 CCHD Station cw

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					Daily	25-Feb	2.98																
					Total 1	tons	2.98	2.98	2.98	2.59	2.59	2.59	2.98	2.59	2.98	2.59	2.59	2.59	2.59	2.59	2.59	2.98	43.78
Stabilized		0.16	350.72	Spike	Emission	A not	0.00	00.00	00.00				00.0		0.00							0.00	
				Spike	Factor	(totvac)	4.59E-06	4.59E-06	4.59E-06				4.59E-06		4.59E-06							4.59E-06	
Stabilized Stabilized Stabilized		0.16	350.72	Steady	CERISSION	ton	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
Stabilized				Steady	h	(ton/ac/hr)	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	
Stable		0.84	1841.28	Spike	1	ton 🥂	0.39	0.39	0.39				0.39		0.39							0.39	
Stable				Spike	Factor	(ton/ac)	2.12E-04	2.12E-04	2.12E-04				2.12E-04		2.12E-04							2.12E-04	
Stable		0.84	1841.28	Steady	Emission	toh	2.54	2.54	2.54	2.54	2.54	2.54	2.54	2.54	2.54	2.54	2.54	2.54	2.54	2.54	2.54	2.54	
Stable	_			Steady	Eactor	(ton/ac/hr)	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	
		raction	Area (acres)		A STATE OF A	Mind (mph)	20.299999	21.4	20.299999	21.6	21.4	20.20001	21.200001	20.799999	21.6	20.4	21.1	20.9	22.700001	22.299999	21	20.4	
	acres	ł			States of the second	Cum hour	1335	1768	1885	1886	1887	1888	2151	2153	2281	2282	2283	2284	2285	2286	2287	4982	
	2192 4	0.84	0.16		の記述の変化になった。	Hour	15	16	13	14	15	16	15	17	-	2	e	4	20	9	7	14	
1999	vacant land area	stable fraction	unstable fraction			Ved	25	15		20		20			9	9	9	9	9	9	9	27	
DM PM-10	olygon 8	Excel 5.0			all and a subscription of the	Month	2	3	e	e	3	e	3	e	4	4	4	4	4	4	4	2	Tabol

Table A.5 - Polygon 8 - CCHD Station dm

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					Total	tons	10.65	9.22	9.25	9.25	9.25	10.65	9.25	9.25	9.25	10.65	9.25	9.25	9.25	10.65	9.25	10.65	10.65	17.05	9.25	9.25	9.25	9.25	9.25	9.25	17.05	17.05	9.25	9.25	9.25	10.65	10.65	9.25	9.25	10.65	10.65	9.25	9.25
Stabilized		0.16	1253.2	Spike	Emission	ton	0.01					0.01				0.01				0.01		0.01	0.01						_							0.01	0.01			0.01	0.01		
Stabilized Stabilized				Spike	Factor	(ton/ac)	4.59E-06					4.59E-06				4.59E-06		-		4.59E-06		4.59E-06	4.59E-06													4.59E-06	4.59E-06			4.59E-06	4.59E-06		
Stabilized		0.16	1253.2	Steady	Emission	ton	0.17	0.14	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.14	0.17	0.17	0.17	0.17	0.17	0.17	0.14	0.14	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17
Stabilized				Steady	Factor	(ton/ac/hr)	1.38E-04	1.09E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.09E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.09E-04	1.09E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1 385 04
otable		0.84	6579.3	Spike	Emission	ton	1.39					1.39				1.39				1.39		1.39	1.39													1.39	1.39			1.39	1.39		
Stable				Spike	Factor	(ton/ac)	2.12E-04					2.12E-04				2.12E-04				2.12E-04		2.12E-04	2.12E-04													2.12E-04	2.12E-04			2.12E-04	2.12E-04		
Stable		0.84	6579.3	Steady	Emission	ton	90.6	9 <u>.</u> 08	9.08	9.08	9.08	90.6	9.08	9.08	9.08	90.6	9.08	9.08	9.08	9.08	9.08	9.08	9.08	16.91	9.08	9.08	9.08	9.08	9.08	9.08	16.91	16.91	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	9.08	80.0
Stable				Steady	Factor	(ton/ac/hr)	1.38E-03	1		1 38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03		1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	2.57E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03			1	2.57E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1 3RE 03
		fraction	Area (acres)			wind (mph)	24.4	25.5	22 799999	22 799999	23.5	8	22.1	22.1	22.299999	20.5	23.4	22.9	20.6	20.20001	22	21.6	24.700001	25.5	24.1	23.6	22.6	20	20.5	20.9	38	27.299999	23.299999	23.299999	24.799999	20.1	21.799999	20	21	20.200001	21.1	20.5	2000007 00
	acres	-	/			Cum hour	477	480	481	492	18 <del>1</del>	1235	1236	1237	1238	1329	1330	1332	1333	1488	1489	1888	2123	2124	2125	2126	2127	2138	2142	2144	2149	2150	2151	2152	2153	2225	2349	2350	2351	2798	2808	2822	5CBC
		0.84	0.16			Hour	21	24		12	13	11	12	13	14	6	0	12	13	24	1	16	11	12	13	14	15	7	9	8	13	14	15	16	17	17	21	8	23	14	24	14	15
1999	vacant land area	stable fraction	unstable fraction			Dav		8	21	21	31	21	21	21	21	8	8	25	22	e	4	8	90	30	30	90	90	31	31	31	31	31	31	31	31	e	8	Ø	80	27	27	28	lac
FL PM-10	Polygon 9					Month	1	F		•	-	2	2	2	2	2	2	2	2	9	3	e	e	3	3	3	3	e	3	e	e	3	3	e	e	4	4	4	4	4	4	4	V

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Stabilized soil, spike-corrected emission factors 

:  Table A.6 - Polygon 9 - CCHD Station fl

i

10.65	9.25	9.25	9.25	18.44	9.25	9.25	9.25	9.25	9.25	9.25	9.25	9.25	10.65	9.25	9.25	9.25	10.65	9.25	9.25	9.25	10.65	598.02
8 8				0.00									0.01				0.01				0.01	
													4.59E-06				4.59E-06				4.59E-06	
0.17	0.17	0.17	0.17	0,14	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	
1.38E-04	1.38E-04	1.36E-04	1.38E-04	1.09E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	
1.39				1.39									1.39				1.39				1.39	
2.12E-04				2.12E-04									2.12E-04				2.12E-04				2.12E-04	
9.08	9.08	9.08	9.08	16.91	9.08	9.08	9.08	9.08	9.08	9,08	9.08	9.08	9.08	9.08	9.08	9.08	9,08	9.08	9.08	9.08	9.08	
1.38E-03	1.38E-03	1.38E-03	1.38E-03	2.57E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	
20.4	24.4	21.1	23.6	25.9	23.6	21.799999	20.4	20.6	22	23.700001	21.4	23.5	22	23.799999	22.6	22.299999	21.700001	21.5	21.700001	20.5	21.799999	
2921	2922	2925	2927	3168	3169	3170	3186	3187	3188	3189	3210	3214	3671	3672	3673	3676	8063	8072	8073	8074	8180	
17	18	21	23	24	1	7	18	19	50	21	18	ន	8	24	-	4	83	8	6	10	20	
5	2	2	2	12	13	13	13	13	13	13	14	14	2	2	9	е	7	e	6	e	7	
5	5	5	5	5	5	5	5	5	5	5	5	5	9	9	9	9	12	12	12	12	12	1-4-1-

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Table A.6 - Polygon 9 - CCHD Station fl

GV PM-10	1999				Stable	Stable	Stable	Stable	Stabilized	Stabilized	Stabilized	Stabilized	
Polygon 14	vacant land area		acres										
Excel 5.0	stable fraction	0.84		fraction		0.84		0.84		0.16		0.16	
	unstable fraction	0.16		Area (acres)		21857.22		21857.22		4163.28		4163.28	
						Steady	Spike	Spike	Steady	Steady	Spike	Spike	
10.00 March		のないないないないである			Factor	Emission	Factor:	Emission	Factor	Emission	Factor	Emission	Total
Month	Dav	Hour	Cum hour	wind (mph)	(toniachr)	tón	(toh/ac)	ton	(tontacthr)	, tot	(ton/ac)	- tot	tons
1					1.38E-03	30.16		4.63	1.38E-04	0.57	4.59E-06	0.02	35.39
	20		Y		1.38E-03	30.16			1.38E-04	0.57			30.74
	21				1.38E-03	30.16			1.38E-04	0.57			30.74
	25			20.29	1.38E-03	30.16	2.12E-04	4.63		0.57	4.59E-06	0.02	35.39
	80				1.38E-03	30.16	1	4.63		0.57	4.59E-06	0.02	35.39
	0	2	2364		1.38E-03	30.16				0.57			30.74
				20.299999	1.38E-03	30.16	2.12E-04	4.63		0.57	4.59E-06	0.02	35.39
						30.16	I I		1.38E-04	0.57			30.74
	5			22.700001	1.38E-03	30.16			1.38E-04	0.57			30.74
47						30.16			1.38E-04	0.57			30.74
47				20	1.38E-03	30.16			1.38E-04				30.74
				20.20001	1.38E-03	30.16			1.38E-04	0.57			30.74
(1)					1.38E-03	30.16			1.38E-04	0.57			30.74
L.				21.6	1.38E-03	30.16	2.12E-04	4.63	1.38E-04	0.57	4.59E-06	0.02	35.39
				22.70	1.38E-03	30.16			1.38E-04				30.74
37									1.38E-04				30.74
<b>ر ت</b>										0.45			56.63
				21.799999	1.38E-03	30.16	2.12E-04	4.63		0.57	4.59E-06	0.02	35.39
						30.16			1.38E-04				30.74
						30.16	2.12E-04	4.63			4.59E-06	0.02	35.39
						30.16			1.38E-04				30.74
							- 1						30.74
				20.29	1.38E-03	30.16	2.12E-04	4.63	1.38E-04		4.59E-06	0.02	35.39
									1.38E-04				30.74
						30.16			1.38E-04				30.74
		-			1	56.17			1.09E-04	0.45			56.63
-	7 27	15		27.4	2.57E-03				1.09E-04				56.63
	7 28			21.299999	1.38E-03	30.16	2.12E-04	4.63		0.57	4.59E-06	0.02	35.39
	8			ଷ	1.38E-03			4.63	1.38E-04	0.57	4.59E-06	0.02	35.39
		10		21.200001	1.38E-03	30.16			1.38E-04	0.57			30.74
				21	1.38E-03	30.16			1.38E-04				30.74
	8	14	5222	20.5					1.38E-04				30.74
1.		12	7692		1.38E-03	30.16	2.12E-04	4.63	1.38E-04	0.57	4.59E-06	0.02	35.39
													14 42 40
Total													27

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## Stabilized soil, spike-corrected emission factors

Table A.7 - Polygon 14 - CCHD Station gv

					Total	tons	4.24	4.24	4.24	3.68	6.78	3.68	6.78	3.68	4.24	4.24	4.24	4.24	54.26
Stabilized		0.16	498.48	Spike	Emission	ton	00:0	0.00	00.0						0.00	0.00	0.00	0.00	
Stabilized Stabilized				Spike	Factor	(ton/ac)	4.59E-06	4.59E-06	4.59E-06						4.59E-06	4.59E-06	4.59E-06	4.59E-06	
Stabilized		0.16	498.48	Steady	Emission	ton	0.07	0.07	0.07	0.07	0.05	0.07	0.05	0.07	0.07	0.07	0.07	0.07	
Stabilized				Steady	Factor	(tion(ac/ht)	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.09E-04	1.38E-04	1.09E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	
Stable		0.84	2617.02	Spike	Enission	ton	0.55	0.55	0.55						95:0	0.55	0.55	0.55	
Stable				Spike	Factor		2.12E-04	2.12E-04	2.12E-04						2.12E-04	2.12E-04	2.12E-04	2.12E-04	
Stable		0.84	2617.02	Steady	Emission	ton	3.61	3.61	3.61	3.61	6.73	3.61	6.73	3.61	3.61	3.61	3.61	3.61	
Stable				Steady	Factor	1997	1.38E-03	1.38E-03	1.38E-03	1.38E-03	2.57E-03	1.38E-03	2.57E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	
		fraction	Area (acres)			(hdm) briw	22.9	24.6	21.200001	21.4	26.1	24.200001	26.5	23.1	21.6	20.299999	20.4	21.799999	
	acres					Cum hour	611	1335	2125	2149	2150	2151	2152	2153	2433	4982	4983	8180	
	3115.5 acres	0.84	0.16			Hour	11	15	13	13	14	15	16	17	6	4	15	20	
1999	vacant land area	stable fraction	unstable fraction		「「「「「「」」」」	Neo	8	55	99	31	31	31	31	31	12	27	27	7	
JD PM-10	Polygon 11 N	Excel 5.0				Month	1	2	e	e	e	e	3	e	4	7	7	12	Total

Stabilized soil, spike-corrected emission factors

Table A.8 - Polygon 11 - CCHD Station jd

Table A.9 - Polygon 17 - CCHD Station to

Stabilized soil, spike-corrected emission factors

3 9	9		21.700001	1.38E-03	30.26	2.12E-04	4.65	1.38E-04	0.58	4.59E-06	0.02	
	10		25.799999	2.57E-03	56.35			1.09E-04	0.46			56.80
	11		24.6	1.38E-03	30.26			1.38E-04	0.58			30.83
	12		24.5	1.38E-03	30.26			1.38E-04	0.58			30.83
	13		81	1.38E-03	30.26			1.38E-04	0.58			30.
	14		2	1.38E-03	30.26			1.38E-04	0.58			30.83
	15		20.9	1.38E-03	30.26			1.38E-04	0.58			30.83
	16		ន	1.38E-03	30.26	2.12E-04	4.65	1.38E-04	0.58	4.59E-06	0.02	35.50
	14		20.299999	1.38E-03	30.26	2.12E-04	4.65	1.38E-04	0.58	4.59E-06	0.02	35.50
	15		22.299999	1.38E-03	30.26			1.38E-04	0.58			30.83
	16		20.4	1.38E-03	30.26			1.38E-04	0.58			30.83
	10		21.200001	1.38E-03	30.26	2.12E-04	4.65	1.38E-04	0.58	4.59E-06	0.02	35.50
	11		21.799999		30.26			1.38E-04	0.58			30.83
	1		22.299999		30.26			1.38E-04	0.58			30.83
	2		24.200001		30.26			1.38E-04	0.58			30.83
	e		28.1	2.57E-03	56.35			1.09E-04	0.46			56.80
	4		27.20001	2.57E-03	56.35			1.09E-04	0.46			56.80
	5		25.1	2.57E-03	56.35			1.09E-04	0.46			56.80
	9		20.6	1.38E-03	30.26			1.38E-04	0.58			30.83
	6		20.799999	1.38E-03	30.26			1.38E-04	0.58			30.83
	10		22.1	1.38E-03	30.26			1.38E-04	0.58			30.83
	11		22.6	1.38E-03	30.26			1.38E-04	0.58			30.83
3 31	12	2148	23.1	1.38E-03	30.26			1.38E-04	0.58			30.83
	13		21.4	1.38E-03	30.26			1.38E-04	0.58			30.83
	14		21.4	1.38E-03	30.26			1.38E-04	0.58			30.83
	16		29.200001	2.57E-03	56.35			1.09E-04	0.46			56.80
	17		22.6	1.38E-03	30.26			1.38E-04	0.58			30.83
	2		21.5	1.38E-03	30.26	2.12E-04	4.65	1.38E-04	0.58	4.59E-06	0.02	
	12		20.200001	1.38E-03	30.26	2.12E-04	4.65	1.38E-04	0.58	4.59E-06	0.02	
	16		20.1	1.38E-03	30.26	2.12E-04	4.65	1.38E-04	0.58	4.59E-06	0.02	
	20		23.6	1.38E-03	30.26	2.12E-04	4.65	1.38E-04	0.58	4.59E-06	0.02	
	21		22.5	1.38E-03	30.26			1.38E-04	0.58			30.83
	8		21.200001	1.38E-03	30.26			1.38E-04	0.58			
	21		23	1.38E-03	30.26	2.12E-04	4.65	1.38E-04	0.58	4.59E-06	0.02	
	15		21	1.38E-03	30.26	2.12E-04	4.65	1.38E-04	0.58	4.59E-06	0.02	
	4		24.299999	1.38E-03	30.26	2.12E-04	4.65	1.38E-04	0.58	4.59E-06	0.0	
	e		20.200001	1.38E-03	30.26			1.38E-04	0.58			30.83
	4		22.200001	1.38E-03	30.26			1.38E-04	0.58			30.83
	9		20.9	1.38E-03	30.26			1.38E-04	0.58			30.83
	10		23.5	1.38E-03	30.26			1.38E-04	0.58			30.83
	11		20.4	1.38E-03	30.26			1.38E-04	0.58			30.83
10 16	12		20.9		30.26			1.38E-04	0.58			30.83
	V		000001 00									
			00.2999990	1.69E-02	370.54	3.32E-U3	72.79	6.30E-03	26.31		0.00	469.64

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<u>_</u>	
Station	
CCHD	
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Polygon	
A.9 -	
Table	

Stabilized soil, spike-corrected emission factors

-06 0.02 35.50 -06 0.02 35.50	0.02		56.80	30.83	30.83	-06 0.02 35.50	56.80	56.80	30.83	30.83	30.83	-06 0.02 35.50	30.83	4257.80
0.30 4.335-00	0.58 4.59E-06	0.58 4.59E-06	0.46	0.58	0.58	0.58 4.59E-06	0.46	0.46	0.58	0.58	0.58	0.58 4.59E-06	0.58	
0 1.38E-04	5 1.38E-04	5 1.38E-04	1.09E-04	1.38E-04	1.38E-04	5 1.38E-04	1.09E-04	1.09E-04	1.38E-04	1.38E-04	1.38E-04	5 1.38E-04	1.38E-04	
4.65	4.65	4.65				4.65						4.65		
2.12E-04	2.12E-04	2.12E-04				2.12E-04						2.12E-04		
30.26	30.26	30.26	56.35	30.26	30.26	30.26	56.35	56.35	30.26	30.26	30.26	30.26	30.26	
1.38E-03	1.38E-03	1.38E-03	2.57E-03	1.38E-03	1.38E-03	1.38E-03	2.57E-03	2.57E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	
21.6	20.5	23	29.5	22.700001	23.6	24.299999	25.1	25	20.6	22.299999	21.700001	21.299999	21.1	
7689	8030	8062	8063	8064	8073	8180	8181	8182	8184	8185	8186	8508	8509	
6	14	22	23	24	6	20	21	ឌ	24	1	2	12	13	
17	1	2	2	2	3	7	7	7	12	8	8	21	21	
11	12	12	12	12	12	12	12	12	12	12	12	12	12	 Total

MC PM-10	1999				Stable	Stable	Stable	Stable	Stabilized	Stabilized	Stabilized	Stabilized	
Polygon 6	vacant land area	421.5	421.5 acres										
Excel 5.0	stable fraction	0.84		fraction		0.84		0.84		0.16		0.16	
	unstable fraction	0.16		Area (acres)		354.06		354.06		67.44		67.44	
					Steady	Steady	Spike	Spike	Steady	Steady	Spike	Spike	
		and the second second second second			Factor	Emission	Factor	Emission	Eactor	Emission	Factor	Emission	Total
Month	Day	Hour	Cun hour	(udu) (ubu)	(ton/ac/hr)	in ton	(ton/ac)	ton	(ton/ac/hr)	lon	(ton/ac)	ton	tons
	2	10	970	20.5	1.38E-03	0.49	2.12E-04	0.08	1.38E-04	0.01	4.59E-06	0.00	0.57
• •	10	1	971	20.200001	1.38E-03	0.49			1.38E-04	0.01			0.50
• •		14	974	20	1.38E-03	0.49			1.38E-04	0.01			0.50
		14	-	25.20001	2.57E-03	0.91	4.90E-04	0.17	1.09E-04	0.01	4.59E-06	0.0	1.09
• •	2	15	1335	24.1	1.38E-03	0.49			1.38E-04	0.01			0.50
		13	3	22	1.38E-03	0.49	2.12E-04	0.08	1.38E-04	0.01	4.59E-06	0.00	0.57
•••		14	2126	20.1	1.38E-03	0.49			1.38E-04	0.01			0.50
**	3	14	2150	21.9	1.38E-03	0.49	2.12E-04	0.08	1.38E-04	0.01	4.59E-06	0.00	0.57
	3 31	15	2151	22.5	1.38E-03	0.49			1.38E-04	0.01			0.50
••	3	16	2152	24.1	1.38E-03	0.49			1.38E-04	0.01			0.50
••	3 31	18	2154	23.6	1.38E-03	0.49			1.38E-04	0.01			0.50
•	4	23	2351	21.5	1.38E-03	0.49	2.12E-04	0.08	1.38E-04	0.01	4.59E-06	0.00	0.57
5	9	2	6242	20.299999	1.38E-03	0.49	2.12E-04	0.08	1.38E-04	0.01	4.59E-06	0.00	0.57
12	2	20	8180	20.4	1.38E-03	0.49	2.12E-04	0.08	1.38E-04	0.01	4.59E-06	0.0	0.57
Total													8.02
					-								

Table A.10 - Polygon 6 CCHD Station mc

Stabilized soil, spike-corrected emission factors

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MS PM-10	1999				Stable	Stable	Stable	Stable	Stabilized	Stabilized Stabilized Stabilized	Stabilized	Stabilized	
Polygon 7	vacant land area	169.5	acres										
Excel 5.0	stable fraction	0.84		fraction		0.84		0.84		0.16		0.16	
	unstable fraction	0.16		Area (acres)		142.38		142.38		27.12		27.12	
					Steady	Steady	Spike	Spike	Steady	Steady	Spike	Spike	
					Ficulty	Emission	Factor	Emission	Factor	Emission	Factor	Emission	Total
Month	Ved Ver	Figure 2.	- oun hou	(indin)_brink*	(inhochno)	ton	(toniac)	tón	(ion/ac/hr)	ton	(ton)ac)	ton	tons
-		11	·		1.38E-03	0.20	2.12E-04	0.03		0.0	4.59E-06	0.00	0.23
	2	13	1333	20.6	1.38E-03	0.20	2.12E-04	0.03	1.38E-04	0.0	4.59E-06	0.0	0.23
		14		25.5	2.57E-03	0.37			1.09E-04	0.0			0.37
2		15		24.9	1.38E-03	0.20			1.38E-04	0.0			0.20
0	2 <del>2</del>	16	1336	21.799999	1.38E-03	0.20			1.38E-04	0.0			0.20
e		13		20.6	1.38E-03	0.20	2.12E-04	0.03	1.38E-04	0.0	4.59E-06	0.0	0.23
3		15		20	1.38E-03	0.20			1.38E-04	0.0			0.20
e		11		22.4	1.38E-03	0.20	2.12E-04	0.03	1.38E-04	0.0	4.59E-06	0.0	0.23
e		12		24		0.20			1.38E-04	0.00			0.20
(T)	8	13		25.4	2.57E-03	0.37			1.09E-04	0.00			0.37
e		14		24.200001	1.38E-03	0.20			1.38E-04	0.0			0.20
3		15		21.6	1.38E-03	0.20			1.38E-04	0.0			0.20
e		6		21.799999	1.38E-03	0.20			1.38E-04	0.00			0.20
e		7		20.20001	1.38E-03	0.20			1.38E-04	0.00			0.20
e)	31	8		20.1	1.38E-03	0.20			1.38E-04	0.00			0.20
e		6		20.5	1.38E-03	0.20			1.38E-04	0.00			0.20
e e		10		21	1.38E-03	0.20			1.38E-04	0.00			0.20
e		13		20.1	1.38E-03	0.20			1.38E-04	0.0			0.20
e		14	2150		1.38E-03	0.20			1.38E-04	0.00			0.20
4	27	14	2798	20.20001	1.38E-03	0.20	2.12E-04	0.03	1.38E-04	0.00	4.59E-06	0.0	0.23
4		15		20.5	1.38E-03	0.20			1.38E-04	0.00			0.20
5	13	19		21.6	1.38E-03	0.20	2.12E-04	0.03	1.38E-04	0.0	4.59E-06	0.00	0.23
5	14	20		20.200001	1.38E-03	0.20	2.12E-04	0.03	1.38E-04	00.00	4.59E-06	0.00	0.23
Total													5.15

.

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# Stabilized soil, spike-corrected emission factors

Table A.11 - Polygon 7 - CCHD Station ms

					Total	tons :	11.27	11.27	9.79	9.79	9.79	9.79	9.79	9.79	11.27	9.79	9.79	9.79	9.79	9.79	9.79	9.79	9.79	9.79	9.79	9.79	9.79	9.79	9.79	9.79	11.27	9.79	9.79	11.27	9.79	9.79	11.27	11.27	11.27	9.79	9.79	11.27	9.79
Stabilized		0.16	1326.08	Spike	Emission	ton	0.01	0.01							0.01																0.0			0.01			0.01	0.01	0.01			0.01	
Stabilized				Spike		1.00	4.59E-06	4.59E-06							4.59E-06																4.59E-06			4.59E-06			4.59E-06	4.59E-06	4.59E-06			4.59E-06	
Stabilized		0.16	1326.08	Steady	Emission	ton	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18
Stabilized Stabilized				Steady	Facility	(ton/ac/hic)	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1 3RF_AA
Stable		0.84	6961.92	Spike		ion -	1.48	1.48							1.48																1.48			1.48			1.48	1.48	1.48			1.48	
Stable				Spike	Factor	(ton/ac)	2.12E-04	2.12E-04							2.12E-04																2.12E-04			2.12E-04			2.12E-04	2.12E-04	2.12E-04			2.12E-04	
Stable	:	0.84	6961.92	Steady	Emission	in ton	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	9.61	0 E4
Stable				Steady	Factor	(ion/achi)	1.38E-03	1.38E-03			1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03		1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03								1.38E-03	1.38E-03	1.38E-03	1.38E-03				1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1 205 02
		fraction	Area (acres)			wind (mph)	21.299999	20	23.4	21.9	22.1	21.5	20.6	21.6	20.1	21	22.9	21.700001	23.6	21.4	21.6	20.9	22.9	22.799999	22.5	24	22.4	23.6	24.1	20.299999	20.299999	21.299999	20.1	21.9	22.4	20.700001	20	22.1	20.6	22	22.299999	20.200001	27 200000
~	acres	Į				Cum hour	477	546	547	548	549	550	551	591	943	<del>4</del> 8	945	946	096	961	962	968	969	970	971	972	973	974	975	976	1243	1244	1245	1332	1333	1334	1483	1622	1885	1886	1887	2123	2125
		0.84	0.16		A STATE OF STATES	Hour	21	18	19	8	21	ន	23	15	7	8	6	10	24	Ŧ	2	8	6	10	11	12	13	4	15	16	19	20	21	12	13	14	19	14	13	14	15	11	61
1999	vacant land area	stable fraction	unstable fraction			Day Car	ୟ	8	83	8	8	33	23	25	8	6	6	6	6	10	10	10	10	10	10	9	10	10	10	10	21	21	21	25	25	25	3	6	20	20	20	90	Ş
	5					Month	1	1	F	-	-	1	1	1	2	2	2	2	2	2	2	2	2	2	7	7	2	7	2	2	8	2	2	2	3	2	3	3	3	3	3	e	2

Table A.12 - Polygon 5 - CCHD Station pl

Stabilized soil, spike-corrected emission factors

. . . . . . . . .

|           | 9.79  | 9.79   | 9.79   | 11.27  | 9.79  | 9.79  | 9.79   | 9.79   | 9.79  | 9.79  | 11.27   
   | 9.79  
   
   
  | 9.79  | 9.79  | 9.79  | 11.27  
  | 11.27  | 11.27  | 9.79   | 9.79  
   
  | 21.45  | 18.04   | 9.79  | 11.27   
   | 9.79   | 9.79   | 11.27   
   | 11.27  | 9.79  | 9.79   
  | 9.79   | 9.79  | 9.79   | 11.27   | 11.27  | 11.27  | 9.79   | 9.79  | 11.27   | 9.79  | 874 <u>4</u> 8  |
|-----------|---|--|--|--|---|---|--|--|---|---
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--|--|---|---|---|--|--
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---|--|---|---
--|---|--|---|--|--|--|---|---|---|---|
|           |   |  |  | 0.01   |   |   |  |  |   |   | 0.01  
   |   
   
   
  |   |   |   | 0.01   
  | 0.01   | 0.01   |  |   
   
  | 0.01   |   |   | 0.01  
   |  |  | 0.01  
   | 0.01   |   |  
  |  |   |  | 0.01  | 0.01   | 0.01   |  |   | 0.01  |   |   |
|           |   |  |  | 4.59E-06   |   |   |  |  |   |   | 4.59E-06  
   |   
   
   
  |   |   |   | 4.59E-06   
  | 4.59E-06   | 4.59E-06   |  |   
   
  | 4.59E-06   |   |   | 4.59E-06  
   |  |  | 4.59E-06  
   | 4.59E-06   |   |  
  |  |   |  | 4.59E-06  | 4.59E-06   | 4.59E-06   |  |   | 4.59E-06  |   |   |
| 0.18      | 0.18  | 0.18   | 0.18   | 0.18   | 0.18  | 0.18  | 0.18   | 0.18   | 0.18  | 0.18  | 0.18  
   | 0.18  
   
   
  | 0.18  | 0.18  | 0.18  | 0.18   
  | 0.18   | 0.18   | 0.18   | 0.18  
   
  | 0.14   | 0.14  | 0.18  | 0.18  
   | 0.18   | 0.18   |   
   | 0.18   | 0.18  | 0.18   
  | 0.18   | 0.18  | 0.18   | 0.18  | 0.18   | 0.18   | 0.18   | 0.18  | 0.18  | 0.18  | -+  |
| 1.38E-04  | 1.38E-04                                      | 1.38E-04   | 1.38E-04   | 1.38E-04   | 1.38E-04  | 1.38E-04  | 1.38E-04   | 1.38E-04   | 1.38E-04  | 1.38E-04  | 1.38E-04  
   | 1.38E-04  
   
   
  | 1.38E-04  | 1.38E-04  | 1.38E-04  | 1.38E-04   
  | 1.38E-04   | 1.38E-04   | 1.38E-04   | 1.38E-04  
   
  | 1.09E-04   | 1.09E-04  | 1.38E-04  | 1.38E-04  
   | 1.38E-04   | 1.38E-04   | 1.38E-04  
   | 1.38E-04   | 1.38E-04  | 1.38E-04   
  | 1.38E-04   | 1.38E-04  | 1.38E-04   | 1.38E-04  | 1.38E-04   | 1.38E-04   | 1.38E-04   | 1.38E-04  | 1.38E-04  | 1.38E-04  |   |
|           |   |  |  | 1.48   |   |   |  |  |   |   | 1.48  
   |   
   
   
  |   |   |   | 1.48   
  | 1.48   | 1.48   |  |   
   
  | 3.41   |   |   | 1.48  
   |  |  | 1.48  
   | 1.48   |   |  
  |  |   |  | 1.48  | 1.48   | 1.48   |  |   | 1.48  |   |   |
|           |   |  |  | 2.12E-04   |   |   |  |  |   |   | 2.12E-04  
   |   
   
   
  |   |   |   | 2.12E-04   
  | 2.12E-04   | 2.12E-04   |  |   
   
  | 4.90E-04   |   |   | 2.12E-04  
   |  |  | 2.12E-04  
   | 2.12E-04   |   |  
  |  |   |  | 2.12E-04  | 2.12E-04   | 2.12E-04   |  |   | 2.12E-04  |   |   |
| 9.61      | 9.61  | 9.61   | 9.61   | 9.61   | 9.61  | 9.61  | 9.61   | 9.61   | 9.61  | 9.61  | 9.61  
   | 9.61  
   
   
  | 9.61  | 9.61  | 9.61  | 9.61   
  | 9.61   | 9.61   | 9.61   | 9.61  
   
  | 17.89  | 17.89   | 9.61  | 9.61  
   | 9.61   | 9.61   | 9.61  
   | 9.61   | 9.61  | 9.61   
  | 9.61   | 9.61  | 9.61   | 9.61  | 9.61   | 9.61   | 9.61   | 9.61  | 9.61  | 9.61  |   |
| 1.38E-03  | 1.38E-03                                      | 1.38E-03   | 1.38E-03   | 1.38E-03   | 1.38E-03  | 1.38E-03  | 1.38E-03   | 1.38E-03   | 1.38E-03  | 1.38E-03  | 1.38E-03  
   | 1.38E-03  
   
   
  | 1.38E-03  | 1.38E-03  | 1.38E-03  | 1.38E-03   
  | 1.38E-03   | 1.38E-03   | 1.38E-03   | 1.38E-03  
   
  | 2.57E-03   | 2.57E-03  | 1.38E-03  | 1.38E-03  
   | 1.38E-03   | 1.38E-03   | 1.38E-03  
   | 1.38E-03   | 1.38E-03  | 1.38E-03   
  | 1.38E-03   | 1.38E-03  | 1.38E-03   | 1.38E-03  | 1.38E-03   | 1.38E-03   | 1.38E-03   | 1.38E-03  | 1.38E-03  | 1.38E-03  |   |
| 21.200001 | 21.700001                                     | 20.1   | 22.4   | 21.299999  | 23.6  | 23.4  | 22.700001  | 21.5   | 20.299999   | 20  | 20.299999   
   | 20.299999   
   
   
  | 21.299999   | 21.799999   | 21  | 20.799999  
  | 20.700001  | 21.299999  | 20.299999  | 20.5  
   
  | 28.6   | 28.200001   | 20.6  | 20  
   | 20.4   | 20.4   | 20.5  
   | 20.700001  | 21.5  | 21.299999  
  | 20.200001  | 20.1  | 21.200001  | 22  | 21.4   | 20.200001  | 22.4   | 20.9  | 21.700001   | 21  |   |
| 2148      | 2149  | 2151   | 2153   | 2269   | 2270  | 2271  | 2272   | 2273   | 2274  | 2295  | 2352  
   | 2353  
   
   
  | 2360  | 2361  | 2362  | 2929   
  | 3211   | 4484   | 4489   | 4493  
   
  | 4982   | 4983  | 4984  | 5009  
   | 5010   | 5011   | 6692  
   | 6922   | 6923  | 6925   
  | 6926   | 6930  | 6931   | 7794  | 8030   | 8071   | 8076   | 8077  | 8180  | 8183  |   |
| 12        | 13  | 15   | 17   | 13   | 14  | 15  | 16   | 17   | 18  | 15  | 24  
   | 1   
   
   
  | 8   | 6   | 10  | 1  
  | 19   | 20   | 1  | 5   
   
  | 14   | 15  | 16  | 17  
   | 18   | 19   | 20  
   | 10   | 1   | 13   
  | 14   | 18  | 19   | 18  | 14   | 7  | 12   | 13  | 20  | 23  |   |
| 31        | 31  | 31   | 31   | 5  | 5   | 5   | 5  | 5  | 5   | 9   | 8   
   | 6   
   
   
  | 6   | 9   | 6   | Э  
  | 14   | 9  | 7  | 7   
   
  | 27   | 27  | 27  | 28  
   | 28   | 28   | 9   
   | 16   | 16  | 16   
  | 16   | 16  | 16   | 21  | 1  | 3  | 3  | 3   | 7   | 7   |   |
| 3         | 3   | 3  | Э  | 4  | 4   | 4   | 4  | 4  | 4   | 4   | 4   
   | 4   
   
   
  | 4   | 4   | 4   | ۍ<br>۲   
  | 5  | 7  | 7  | 7   
   
  | 7  | 7   | 7   | 7   
   | 7  | 7  | 10  
   | 10   | 10  | 10   
  | 10   | 10  | 10   | 11  | 12   | 12   | 12   | 12  | 12  | 12  | Total   |
|           | 31 12 2148 21.200001 1.38E-03 9.61 1 1.38E-04 | 31 12 21.48 21.200001 1.38E.03 9.61 1.38E-04 1.3 | 31         12         21.48         21.200001         1.38E-03         9.61         1.38E-04           31         13         21.49         21.700001         1.38E-03         9.61         1.38E-04           31         15         2151         20.1         1.38E-03         9.61         1.38E-04 | 31         12         21.48         21.200001         1.38E-03         9.61         1.38E-04           31         13         21.49         21.700001         1.38E-03         9.61         1.38E-04           31         15         2151         20.1         1.38E-03         9.61         1.38E-04           31         15         2151         20.1         1.38E-03         9.61         1.38E-04           31         17         2153         22.4         1.38E-03         9.61         1.38E-04 | 31         12         2148         21.200001         1.38E-03         9.61         1.38E-04         0.18           31         13         2149         21.700001         1.38E-03         9.61         1.38E-04         0.18           31         15         2151         20.1         1.38E-03         9.61         1.38E-04         0.18           31         15         2151         20.1         1.38E-03         9.61         1.38E-04         0.18           31         17         2153         20.1         1.38E-03         9.61         1.38E-04         0.18           5         13         2259         21.38E-03         9.61         1.48         1.38E-04         0.18 | 31         12         2148         21.200001         1.38E-03         9.61         1.38E-04         0.18           31         13         2149         21.700001         1.38E-03         9.61         1.38E-04         0.18           31         15         2151         20.1         1.38E-03         9.61         1.38E-04         0.18           31         15         2151         20.1         1.38E-03         9.61         1.38E-04         0.18           31         17         2153         20.1         1.38E-03         9.61         1.38E-04         0.18           5         13         2153         22.4         1.38E-03         9.61         1.38E-04         0.18           5         13         2269         21.299399         1.38E-03         9.61         1.48         1.38E-04         0.18           5         14         2270         23.6         1.38E-03         9.61         1.48         1.38E-04         0.18 | 31         12         2148         21.200001         1.38E-03         9.61         1.38E-04         0.18           31         13         2149         21.700001         1.38E-03         9.61         1.38E-04         0.18           31         15         2151         20.1         1.38E-03         9.61         1.38E-04         0.18           31         15         2151         20.1         1.38E-03         9.61         1.38E-04         0.18           31         17         2153         22.14         1.38E-03         9.61         1.38E-04         0.18           5         13         2153         22.4         1.38E-03         9.61         1.48         1.38E-04         0.18           5         14         2270         23.16         1.38E-03         9.61         1.48         1.38E-04         0.18         4.59E-06           5         14         2270         23.6         1.38E-03         9.61         1.38E-04         0.18         4.59E-06           5         15         2270         23.4         1.38E-03         9.61         1.38E-04         0.18         4.59E-06           5         15         2270         23.4         1.38E-03 | 31         12         2148         21.200001         1.38E-03         9.61         1.38E-04         0.18           31         13         2149         21.700001         1.38E-03         9.61         1.38E-04         0.18           31         15         2151         20.1         1.38E-03         9.61         1.38E-04         0.18           31         17         2153         20.1         1.38E-03         9.61         1.38E-04         0.18           31         17         2153         20.1         1.38E-03         9.61         1.38E-04         0.18           5         13         2153         22.4         1.38E-03         9.61         1.48         1.38E-04         0.18           5         14         2270         23.1299999         1.38E-03         9.61         1.48         1.38E-04         0.18         4.59E-06           5         16         2271         23.4         1.38E-03         9.61         1.48         1.38E-04         0.18         4.59E-06           5         15         2270         23.4         1.38E-03         9.61         1.48         0.18         4.59E-06           5         16         2271         2274         < | 31         12         2148         21.200001         1.38E-03         9.61         1.38E-04         0.18           31         13         2149         21.700001         1.38E-03         9.61         1.38E-04         0.18           31         15         2151         20.1         1.38E-03         9.61         1.38E-04         0.18           31         17         2153         20.1         1.38E-03         9.61         1.38E-04         0.18           5         13         2153         22.4         1.38E-03         9.61         1.38E-04         0.18           5         13         2269         21.38E-03         9.61         2.12E-04         0.18         4.59E-06           5         14         2270         23.6         1.38E-03         9.61         1.48         1.38E-04         0.18         4.59E-06           5         16         2271         23.4         1.38E-03         9.61         1.48         1.38E-04         0.18         4.59E-06           6         16         2.12E-04         1.48         1.38E-04         0.18         4.59E-06           7         23.6         1.38E-03         9.61         1.38E-04         0.18         4.59E-0 | 31         12         2148         21.200001         1.38E-03         9.61         1.38E-04         0.18           31         13         2149         21.700001         1.38E-03         9.61         1.38E-04         0.18           31         15         2151         20.1         1.38E-03         9.61         1.38E-04         0.18           31         17         2153         20.1         1.38E-03         9.61         1.38E-04         0.18           5         13         2153         22.4         1.38E-03         9.61         1.38E-04         0.18         4.59E-06           5         14         2270         23.5         1.38E-03         9.61         1.48         1.38E-04         0.18         4.59E-06           5         16         22770         23.4         1.38E-03         9.61         1.48         1.38E-04         0.18         4.59E-06           5         16         22771         23.4         1.38E-03         9.61         1.38E-04         0.18         4.59E-06           5         16         22772         22.7700001         1.38E-03         9.61         1.38E-04         0.18         4.59E-06           5         16         22772 | 31         12         2148         21.200001         1.38E-03         9.61         1.38E-04         0.18           31         13         2149         21.700001         1.38E-03         9.61         1.38E-04         0.18           31         15         2151         20.1         1.38E-03         9.61         1.38E-04         0.18           31         17         2153         22.14         1.38E-03         9.61         1.38E-04         0.18           5         13         2153         22.4         1.38E-03         9.61         1.38E-04         0.18         4.59E-06           5         14         2270         23.6         1.38E-03         9.61         1.48         1.38E-04         0.18         4.59E-06           5         16         2277         23.4         1.38E-03         9.61         1.48         1.38E-04         0.18         4.59E-06           5         16         2277         23.4         1.38E-03         9.61         1.38E-04         0.18         4.59E-06           5         16         2277         2277         2277         227.700001         1.38E-03         9.61         0.18         0.18         1.38E-04         0.18         1.3 | 31 $12$ $2148$ $21.200001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $0.18$ $31$ $15$ $2149$ $21.700001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $0.18$ $31$ $17$ $2151$ $20.1$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $0.18$ $5$ $13$ $2273$ $22.4$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $4.59E.06$ $5$ $14$ $22770$ $22.3.6$ $1.38E.03$ $9.61$ $1.48$ $1.38E.04$ $0.18$ $4.59E.06$ $5$ $16$ $2277$ $22.7$ $1.38E.03$ $9.61$ $1.48$ $1.38E.04$ $0.18$ $4.59E.06$ $5$ $16$ $2277$ $22.77$ $22.7$ $1.38E.03$ $9.61$ $1.48$ $1.38E.04$ $0.18$ $4.59E.06$ $5$ $16$ $2277$ $2277$ $22.77$ $22.77$ $22.77$ $22.77$ $22.77$ $22.77$
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<math>1.38E.03</math> <math>9.61</math> <math>1.38E.04</math> <math>0.18</math> <math>4.59E.06</math> <math>6</math> <math>15</math> <math>2.274</math> <math>2.0289999</math> <math>1.38E.03</math> <math>9.61</math> <math>1.38E.04</math> <math>0.1</math></td><td>31 <math>12</math> <math>2148</math> <math>21,20001</math> <math>1.38E.04</math> <math>0.18</math> <math>0.18</math> <math>31</math> <math>15</math> <math>2161</math> <math>21,30001</math> <math>1.38E.04</math> <math>0.18</math> <math>0.18</math> <math>31</math> <math>15</math> <math>2161</math> <math>21,3001</math> <math>38E.04</math> <math>0.18</math> <math>0.18</math> <math>31</math> <math>17</math> <math>2153</math> <math>2201</math> <math>38E.04</math> <math>0.18</math> <math>0.18</math> <math>5</math> <math>13</math> <math>2269</math> <math>21,29996</math> <math>38E.04</math> <math>0.18</math> <math>0.18</math> <math>5</math> <math>16</math> <math>2271</math> <math>2234</math> <math>38E.04</math> <math>0.18</math> <math>0.18</math> <math>5</math> <math>17</math> <math>2277</math> <math>2270001</math> <math>38E.03</math> <math>961</math> <math>1.48</math> <math>1.38E.04</math> <math>0.18</math> <math>5</math> <math>17</math> <math>22772</math> <math>2270001</math> <math>38E.03</math> <math>961</math> <math>1.38E.04</math> <math>0.18</math> <math>5</math> <math>17</math> <math>22772</math> <math>2270001</math> <math>38E.03</math> <math>961</math> <math>1.38E.04</math> <math>0.18</math> <math>6</math> <math>18</math> <math>22772</math> <math>2029990</math> <math>138E.03</math> <math>961</math> <math>1.38E.04</math> <math>0.18</math> <math>8</math></td><td>31         12         2148         21.20001         1.38E-03         961         1.38E-04         0.18           31         15         2149         21.700001         1.38E-03         961         1.38E-04         0.18           31         17         2153         22.4         1.38E-03         961         1.38E-04         0.18           5         14         2770         23.54         1.38E-03         961         1.38E-04         0.18           5         14         2270         23.44         1.38E-03         961         1.38E-04         0.18           5         16         2277         22.34         1.38E-03         961         1.38E-04         0.18           5         16         2277         23.4         1.38E-03         961         1.38E-04         0.18           5         16         2277         23.4         1.38E-03         961         1.38E-04         0.18           6         15         2273         22.34         1.38E-03         961         1.38E-04         0.18           6         16         2277         23.7         1.38E-03         961         1.38E-04         0.18           7         248</td><td>31         12         2148         21,20001         1,36E-03         961         1,38E-04         0.16           31         15         2151         21.50001         1,38E-03         961         1,38E-04         0.16           31         17         215         2266         21.56001         366         1,38E-04         0.16         456E-06           5         16         2151         2224         1,38E-03         9.61         1,38E-04         0.16         456E-06           5         16         2271         223.61         1,38E-03         9.61         0.16         456E-06           5         16         2271         223.61         1,38E-03         9.61         0.16         456E-06           6         15         2271         2236         1,38E-03         9.61         0.16         456E-06           6         15         2273         20.296999         1,38E-03         9.61         0.16         456E-06           6         15         2274         20.296999         1,38E-03         0.16         456E-06           7         236         1,38E-03         9.61         1,38E-04         0.18         456E-06           6         &lt;</td><td>31         112         <math>2148</math> <math>21,20001</math> <math>138c.04</math> <math>0.16</math> <math>0.16</math>           31         15         <math>2169</math> <math>21,70001</math> <math>138c.03</math> <math>961</math> <math>1.38c.94</math> <math>0.16</math>           31         17         <math>2153</math> <math>2244</math> <math>38c.03</math> <math>961</math> <math>1.38c.94</math> <math>0.18</math>           5         14         <math>2770</math> <math>23693</math> <math>138c.03</math> <math>961</math> <math>1.38c.94</math> <math>0.18</math>           5         16         <math>2777</math> <math>2274</math> <math>328-36</math> <math>961</math> <math>1.38c.94</math> <math>0.18</math>           5         16         <math>2777</math> <math>22.7300001</math> <math>138c.03</math> <math>961</math> <math>1.38c.94</math> <math>0.18</math>           6         15         <math>2773</math> <math>22.732020591</math> <math>38c.03</math> <math>961</math> <math>1.38c.94</math> <math>0.18</math>           6         15         <math>2773</math> <math>20.2399991</math> <math>38c.03</math> <math>961</math> <math>1.38c.94</math> <math>0.18</math>           6         15         <math>22773</math> <math>20.2399991</math> <math>38c.03</math> <math>961</math> <math>1.38c.94</math> <math>0.18</math>           7         2295         <math>20.2399991</math> <math>138c.03</math> <math>961</math> <math>1.38c.94</math></td><td>31         12         <math>2140</math> <math>21,20001</math> <math>1362.03</math> <math>961</math> <math>1.382.44</math> <math>0.18</math>           31         15         <math>2149</math> <math>21,70001</math> <math>1382.03</math> <math>961</math> <math>1.382.44</math> <math>0.18</math>           31         17         <math>2153</math> <math>22.44</math> <math>1382.03</math> <math>961</math> <math>1.382.44</math> <math>0.18</math>           5         14         <math>2270</math> <math>2234</math> <math>1382.03</math> <math>961</math> <math>1.382.64</math> <math>0.18</math>           5         14         <math>2277</math> <math>2234</math> <math>1382.03</math> <math>961</math>
<math>1.382.64</math> <math>0.18</math>           5         16         <math>2277</math> <math>2273</math> <math>1.382.03</math> <math>961</math> <math>1.382.64</math> <math>0.16</math>           5         16         <math>2277</math> <math>2273</math> <math>1.382.03</math> <math>961</math> <math>1.382.64</math> <math>0.16</math>           6         17         <math>2277</math> <math>2270</math> <math>1.382.03</math> <math>961</math> <math>1.382.64</math> <math>0.16</math>           6         17         <math>2277</math> <math>2270301</math> <math>1.382.03</math> <math>961</math> <math>1.382.64</math> <math>0.16</math>           6         18         <math>2774</math> <math>2229309301         <math>1.382.03</math> <math>961</math> </math></td><td>31         11         2         2148         <math>21,20001</math>         1,38E,03         961         1,38E,04         0.18           31         11         2         2161         21,0001         1,38E,03         961         1,38E,04         0.18           31         17         2153         2161         2161         21,001         1,38E,03         961         1,38E,04         0.18           5         14         2270         2266         1,38E,03         961         1,38E,04         0.18           5         15         2271         2216         1,38E,03         961         1,38E,04         0.18           5         16         2277         2216         1,38E,03         961         1,38E,04         0.18           6         15         2271         2216         1,38E,03         961         1,38E,04         0.18           6         15         2273         2236999         1,38E,03         961         1,38E,04         0.16         4,56E,06           6         16         2773         2274         2028999         1,38E,03         961         1,38E,04         0.16           7         2773         2271         202899         1,38E,03<td>31         11         2148         21.200001         1.38E-03         9.61         1.38E-04         0.18           31         13         2.148         2.1700001         1.38E-03         9.61         1.38E-04         0.18           31         17         2.153         2.10001         1.38E-03         9.61         1.38E-04         0.18           5         14         2.770         2.316         1.38E-03         9.61         1.38E-04         0.18           5         14         2.770         2.334         1.38E-03         9.61         1.38E-04         0.18           5         16         2.277         2.273         2.306         1.38E-03         9.61         1.38E-04         0.18           5         16         2.277         2.273         2.30699         1.38E-03         9.61         1.38E-04         0.18           6         15         2.274         2.274         2.273         2.30699         1.38E-03         9.61         1.38E-04         0.18           6         15         2.274         2.274         2.274         2.274         2.276         0.18           7         2.36999         1.38E-03         9.61         1.38E-04         0</td><td>31         11         2148         21,20001         138-03         9.61         138-04         0.18           31         16         215         21,30001         138-03         9.61         138-04         0.18           31         17         2163         2101         38-03         9.61         138-04         0.18           5         14         2270         23.61         3.86-03         9.61         1.36-04         0.18           5         14         2270         23.61         3.86-03         9.61         1.36-04         0.18           5         16         2272         22.00001         1.36-03         9.61         1.36-04         0.18           5         17         2272         22.00001         1.36-03         9.61         1.36-04         0.18           6         217         227         22.00001         1.36-03         9.61         1.36-04         0.18           6         16         2274         20.20809         1.36-03         9.61         1.36-04         0.18           7         18         2274         20.20809         1.36-03         9.61         1.36-04         0.18           8         2274</td><td>31         12         2148         21.00001         1.38E-03         9.61         1.38E-04         0.18           31         15         2169         21.00001         1.38E-03         9.61         1.38E-04         0.18           5         13         2.553         2.563         2.661         3.61         1.38E-03         0.16         4.56E-06           5         14         2.770         2.361         1.38E-03         9.61         1.38E-04         0.18         4.56E-06           5         16         2.771         2.7003         9.61         1.38E-04         0.18         4.56E-06           5         16         2.771         2.7003         9.61         1.38E-04         0.18         4.56E-06           6         15         2.77         2.7003         9.61         1.38E-04         0.18         4.56E-06           6         15         2.77         2.7003         9.61         1.38E-04         0.18         4.56E-06           6         15         2.77         2.722         1.38E-03         0.18         4.56E-06           7         272         2.723         1.38E-03         9.61         1.38E-04         0.18         4.56E-06      &lt;</td><td>31         12         2148         21,20001         1,38E,03         961         1,38E,04         0,19           31         13         2161         2100001         138E,03         961         1,38E,04         0,19           5         13         2215         2201         138E,03         961         1,38E,04         0,19           5         14         2270         2234         1,38E,03         961         1,38E,04         0,19           5         14         2270         2234         1,38E,03         961         1,38E,04         0,19           6         15         2277         2270001         1,38E,03         961         1,38E,04         0,19           6         17         2273         2203         961         1,38E,04         0,18           6         17         2273         2203         961         1,38E,04         0,18           7         19         277         2003         138E,03         961         1,38E,04         0,18           6         15         2273         2029999         138E,03         961         1,38E,04         0,18           7         14         2382         27286991         138E,03</td><td>31         11         22         27.44         27.00001         1.38E-03         9.61         1.38E-04         0.18           31         13         21         20001         1.38E-03         9.61         1.38E-04         0.18           31         13         2161         2.0001         1.38E-03         9.61         1.38E-04         0.18           5         13         2278         2.21         32003         9.61         1.38E-04         0.18           5         14         2270         223         1.38E-03         9.61         1.38E-04         0.18           5         17         2273         2270034         1.38E-03         9.61         1.38E-04         0.18           6         16         2772         2270304         1.38E-03         9.61         1.38E-04         0.18           6         13         2273         2003069         1.38E-03         9.61         1.38E-04         0.18           7         24         2382         2036969         1.38E-03         9.61         1.38E-04         0.18           7         24         2382         2036969         1.38E-03         9.61         1.38E-04         0.18           7&lt;</td><td>31         12         <math>2148</math> <math>27.30001</math> <math>386.04</math> <math>018</math> <math>010</math> <math>1386.04</math> <math>018</math>           31         13         23.48         <math>27.700001</math> <math>386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           5         14         <math>2277</math> <math>2036</math> <math>386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           5         14         <math>2277</math> <math>2336</math> <math>386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           5         14         <math>2277</math> <math>2336</math> <math>386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           6         17         <math>22773</math> <math>2386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           6         17         <math>22773</math> <math>2386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           7         18         <math>2277</math> <math>2273</math> <math>3286.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           9         1         <math>2277</math> <math>2273</math> <math>3286.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           9         1         <math>2267</math> <math>27398696</math> <math>1386.04</math> <math>018</math> <math>1386.04</math> <math>018</math></td><td>31         12         <math>2148</math> <math>27,00001</math> <math>138E,00</math>         961         <math>138E,04</math>         018           31         13         2148         <math>27,00001</math> <math>138E,03</math>         961         <math>138E,04</math>         018           31         14         <math>2170</math> <math>2361</math> <math>38E,03</math>         961         <math>138E,04</math>         018           5         14         <math>2270</math> <math>2361</math> <math>38E,03</math>         961         <math>138E,04</math>         018           5         14         <math>2272</math> <math>2270001</math> <math>38E,03</math>         961         <math>138E,04</math>         018           6         15         <math>2272</math> <math>2270001</math> <math>38E,03</math>         961         <math>138E,04</math>         018           6         15         <math>2272</math> <math>2203996</math> <math>138E,03</math>         961         <math>138E,04</math>         018           6         14    
    <math>2272</math> <math>22730966</math> <math>138E,03</math>         961         <math>138E,04</math>         018           7         14         <math>2276</math> <math>21726,04</math> <math>1,48</math> <math>138E,04</math>         018           9         2         <math>2272</math> <math>22729996</math> <math>138E,04</math>         018         <math>438E,06</math>           9         14&lt;</td><td>31         12         2140         21,00001         1,38E,04         0118         138E,04         0118           31         13         2140         21,00001         1,38E,03         9.61         1,38E,04         0.18           31         13         2140         27,001         1,38E,03         9.61         1,38E,04         0.18           5         14         2270         2276         31.8E,03         9.61         1,38E,04         0.18           5         16         2277         227001         1,38E,03         9.61         1,38E,04         0.18           5         16         2277         227001         1,38E,03         9.61         1,38E,04         0.18           6         15         2277         2270001         1,38E,03         9.61         1,38E,04         0.18           6         15         2277         2270001         1,38E,03         9.61         1,12E,04         1.61         1,38E,04         0.18           6         15         2274         20.308691         1,38E,03         9.61         1,38E,04         0.18         1,456E,06           7         2274         20.3286901         1,38E,03         9.61         1,28E,04</td><td>31         12         2148         21,00001         138:00         138:04         0.18           31         13         2148         21,00001         138:03         9.61         138:04         0.18           31         13         2148         21,00001         138:03         9.61         138:04         0.18           5         13         2163         138:03         9.61         2.17:04         138:04         0.18           5         16         2277         2270         138:03         9.61         138:04         0.18           5         18         2773         22.66         9.61         138:04         0.18         138:04         0.19           6         17         2273         22.6669         138:03         9.61         138:04         0.19         14.66           6         13         2773         22.6669         138:03         9.61         138:04         0.19         14.66           7         2235         2236699         138:03         9.61         138:04         0.19         14.66         0.16           9         2         138:04         0.18         138:04         0.19         138:04         0.19         1</td><td>31         12         2148         21,00001         38E-03         961         1,38E-04         0.18           31         15         216         2,100001         38E-03         961         1,38E-04         0.18           31         16         2276         2,266         1,38E-04         0.18         1,38E-04         0.18           5         16         2273         22,10001         38E-03         961         1,38E-04         0.18           5         16         2273         22,10001         38E-03         961         1,38E-04         0.18           6         16         2273         22,100001         38E-03         961         1,38E-04         0.18           6         16         2273         22,100001         38E-03         961         1,38E-04         0.18           6         16         2273         22,100001         38E-03         961         1,38E-04         0.18         456E-06           7         2245         20,298696         1,38E-03         961         1,38E-04         0.18         456E-06           7         2247         2272         200001         38E-03         0.18         456E-06         0.18         456E-06</td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td>31         12         2.48         71,20001         1.38E,40         0.16         1.38E,40         0.16           31         15         2.48         71,20001         1.38E,40         0.16         1.38E,40         0.16           5         13         2.51         2.24         1.38E,40         0.16         1.38E,40         0.16           6         16         2.27         2.24         1.38E,40         9.61         1.38E,40         0.16           5         17         2.260         2.34         3.8E,40         9.61         1.38E,40         0.16           6         16         2.27         2.271         2.24         3.8E,40         9.61         1.38E,40         0.16           7         16         2.27         2.274         3.8E,40         9.61         1.38E,40         0.16           6         16         2.77         2.216         3.8E,40         9.61         1.38E,40         0.16           7         2.86         2.155         3.7266696         1.38E,40         0.16         4.58E,40           9         1         2.72         2.7201         3.8E,40         9.61         1.48E,40         0.16           1         2.72&lt;</td><td>1.38E.03         9.61         <math>1.38E.04</math>         0.18           <math>1.38E.03</math>         9.61         <math>1.38E.04</math>         0.18           <td< td=""></td<></td></td></t<></td> | 31 $12$ $2148$ $21,200001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $31$ $15$ $2151$ $20.1$ $38E.03$ $9.61$ $1.38E.04$ $0.18$ $31$ $17$ $2153$ $22.4$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $5$ $13$ $2153$ $22.4$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $5$ $13$ $2269$ $21.299999$ $1.38E.03$ $9.61$ $1.48$ $1.38E.04$ $0.18$ $5$ $14$ $2270$ $23.6$ $1.38E.03$ $9.61$ $1.48$ $1.38E.04$ $0.18$ $5$ $16$ $2271$ $2273$ $21.5$ $9.61$ $1.48$ $1.38E.04$ $0.18$ $5$ $16$ $2277$ $2271$ $2274$ $20299999$ $9.61$ $1.38E.04$ $0.18$ $6$ $17$ $2277$ $2277$ $227700001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $6$ $16$ $2272$ $2277$ $2277$ $2272$ $227700001$ $3.8E.03$ $9.61$ $1.38E.04$ $0.18$ $6$ $15$ $2272$ $2277$ $2272$ $22700001$ $3.8E.03$ $9.61$ $1.38E.04$ $0.18$ $6$ $15$ $2272$ $2272$ $22700001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $6$ $15$ $2272$ $2272$ $2272$ $22700001$ $3.8E.04$ $0.18$ $0.18$ $6$ $16$ $2272$ $2274$ $202999999$ $1.38E.03$ $9.61$ $1$ | 31 $12$ $2148$ $21,200001$ $1.38E,03$ $9.61$ $1.38E,04$ $0.18$ $31$ $15$ $2161$ $20.1$ $38E,03$ $9.61$ $1.38E,04$ $0.18$ $31$ $17$ $2153$ $22.1$ $20.1$ $1.38E,03$ $9.61$ $1.38E,04$ $0.18$ $5$ $13$ $2153$ $22.4$ $1.38E,03$ $9.61$ $1.38E,04$ $0.18$ $4.59E,06$ $5$ $13$ $2269$ $21.298999$ $1.38E,03$ $9.61$ $1.48$ $1.38E,04$ $0.18$ $4.59E,06$ $5$ $14$ $22770$ $22.34$ $1.38E,03$ $9.61$ $1.48$ $1.38E,04$ $0.18$ $4.59E,06$ $5$ $16$ $22772$ $22.72$ $22.73$ $22.15$ $1.38E,03$ $9.61$ $1.38E,04$ $0.18$ $5$ $16$ $22772$ $22772$ $22.73$ $21.5$ $1.38E,03$ $9.61$ $1.38E,04$ $0.18$ $6$ $17$ $22772$ $22772$ $22.75$ $22.75$ $22.75$ $22.75$ $0.61$ $1.38E,04$ $0.18$ $6$ $17$ $22772$ $2274$ $20.299999$ $1.38E,03$ $9.61$ $1.38E,04$ $0.18$ $6$ $15$ $2274$ $20.299999$ $1.38E,03$ $9.61$ $1.38E,04$ $0.18$ $6$ $15$ $2274$ $20.299999$ $1.38E,03$ $9.61$ $1.38E,04$ $0.18$ $6$ $15$ $2274$ $20.299999$ $1.38E,03$ $9.61$ $1.38E,04$ $0.18$ $6$ $12$ $2274$ $20.2999$ | 31 $12$ $2148$ $21.200001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $31$ $15$ $2151$ $20.11$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $31$ $17$ $2153$ $20.11$ $38E.03$ $9.61$ $1.38E.04$ $0.18$ $5$ $13$ $2269$ $21.28999$ $3.861$ $3.61$ $1.38E.04$ $0.18$ $5$ $14$ $2270$ $23.6$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $5$ $16$ $2277$ $22.700001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $5$ $17$ $22772$ $22.700001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $5$ $117$ $22772$ $2272$ $22.700001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $6$ $15$ $2272$ $22.72$ $22.700001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $6$ | 31 $12$ $2148$ $21.20001$ $1.38E.03$ $961$ $1.38E.04$ $0.18$ $31$ $15$ $2151$ $201$ $1.38E.03$ $961$ $1.38E.04$ $0.18$ $31$ $17$ $2153$ $2149$ $21.70001$ $1.38E.03$ $961$ $1.38E.04$ $0.18$ $5$ $13$ $2153$ $2234$ $1.38E.03$ $961$ $1.38E.04$ $0.18$ $5$ $14$ $2270$ $2336$ $1.38E.03$ $961$ $1.38E.04$ $0.18$ $5$ $16$ $2277$ $2234$ $1.38E.03$ $961$ $1.38E.04$ $0.18$ $5$ $16$ $2277$ $2271$ $2272$ $2270031$ $1.38E.03$ $961$ $1.38E.04$ $0.18$ $6$ $15$ $2277$ $20239391$ $1.38E.03$ $961$ $1.38E.04$ $0.18$ $6$ $15$ $2273$ $20239391$ $1.38E.03$ $961$ $1.38E.04$ $0.18$ $6$ | 31 $12$ $2148$ $21,20001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $31$ $15$ $2151$ $21,30001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $31$ $17$ $2153$ $22.1$ $21,30001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $5$ $13$ $2209$ $21,38E.03$ $9.61$ $1.38E.04$ $0.18$ $4.59E.06$ $5$ $14$ $2270$ $223.6$ $1.38E.03$ $9.61$ $1.48$ $1.38E.04$ $0.18$ $5$ $16$ $2277$ $22.70001$ $1.38E.03$ $9.61$ $1.48$ $1.38E.04$ $0.18$ $5$ $17$ $2277$ $22.70001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $5$ $17$ $2277$ $22.700001$ $1.38E.03$ $9.61$ $0.18$ $1.38E.04$ $0.18$ $5$ $16$ $2272$ $22.700001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.1$ | 31 $12$ $2148$ $21,20001$ $1.38E-04$ $0.18$ $0.18$ $31$ $15$ $2149$ $21,70001$ $1.38E-03$ $9.61$ $1.38E-04$ $0.18$ $31$ $17$ $2153$ $22.41$ $1.38E-03$ $9.61$ $1.38E-04$ $0.18$ $5$ $13$ $2269$ $21.38E-03$ $9.61$ $1.38E-04$ $0.18$ $459E-06$ $5$ $14$ $2270$ $23.61$ $1.38E-03$ $9.61$ $1.48$ $1.38E-04$ $0.18$ $5$ $16$ $2277$ $22.70001$ $1.38E-03$ $9.61$ $1.48$ $1.38E-04$ $0.18$ $5$ $11$ $2277$ $22.70001$ $1.38E-03$ $9.61$ $1.48$ $1.38E-04$ $0.18$ $5$ $11$ $2277$ $2271$ $22.39299$ $1.38E-03$ $9.61$ $1.48$ $1.38E-04$ $0.18$ $6$ $15$ $2277$ $22279$ $22.3299999$ $1.38E-03$ $9.61$ $1.38E-04$ | 31         12 $2148$ $21.200001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $31$ $15$ $2153$ $22.4$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $31$ $17$ $2153$ $22.4$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $5$ $13$ $2269$ $21.299999$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $5$ $14$ $2270$ $22.36$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $5$ $16$ $2277$ $22.73$ $2.36999$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $5$ $16$ $2277$ $22773$ $2.2739993$ $9.61$ $1.38E.04$
$0.18$ $6$ $15$ $22773$ $2.29299399$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $6$ $15$ $22773$ $2.29299399$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $6$ $15$ < | 31         12 $2148$ $21.20001$ $1.38E.04$ $0.16$ $0.16$ $31$ $15$ $2149$ $21.70001$ $1.38E.03$ $961$ $1.38E.04$ $0.16$ $31$ $17$ $2153$ $22.4$ $1.38E.03$ $961$ $1.38E.04$ $0.16$ $5$ $14$ $2270$ $23.6$ $1.38E.03$ $961$ $1.38E.04$ $0.18$ $5$ $14$ $2277$ $22.70$ $3.61$ $1.48$ $1.38E.04$ $0.18$ $5$ $17$ $2277$ $22.70$ $23.6$ $1.38E.03$ $961$ $1.38E.04$ $0.18$ $5$ $17$ $2277$ $22.7000$ $3.8E.03$ $961$ $1.38E.04$ $0.18$ $6$ $15$ $2772$ $22.7000$ $3.8E.03$ $961$ $1.38E.04$ $0.18$ $6$ $15$ $2772$ $22.7000$ $3.8E.03$ $961$ $1.38E.04$ $0.18$ $6$ $15$ $2772$ $22.020009$ <t< td=""><td>31 <math>12</math> <math>2148</math> <math>21,200001</math> <math>1.38E.03</math> <math>9.61</math> <math>1.38E.04</math> <math>0.16</math> <math>31</math> <math>15</math> <math>2153</math> <math>22.44</math> <math>21,138E.03</math> <math>9.61</math> <math>1.38E.04</math> <math>0.16</math> <math>5</math> <math>13</math> <math>2.743</math> <math>2.153</math> <math>22.24</math> <math>1.38E.03</math> <math>9.61</math> <math>1.38E.04</math> <math>0.16</math> <math>5</math> <math>14</math> <math>2.273</math> <math>2.24</math> <math>1.38E.03</math> <math>9.61</math> <math>1.38E.04</math> <math>0.16</math> <math>5</math> <math>14</math> <math>2.277</math> <math>2.234</math> <math>1.38E.03</math> <math>9.61</math> <math>1.38E.04</math> <math>0.16</math> <math>5</math> <math>16</math> <math>2.277</math> <math>2.271</math> <math>2.271</math> <math>2.271</math> <math>2.274</math> <math>0.18</math> <math>4.59E.06</math> <math>6</math> <math>15</math> <math>2.273</math> <math>2.215</math> <math>1.38E.03</math> <math>9.61</math> <math>1.38E.04</math> <math>0.18</math> <math>4.59E.06</math> <math>6</math> <math>15</math> <math>2.274</math> <math>2.0289999</math> <math>1.38E.03</math> <math>9.61</math> <math>1.38E.04</math> <math>0.18</math> <math>4.59E.06</math> <math>6</math> <math>15</math> <math>2.274</math> <math>2.0289999</math> <math>1.38E.03</math> <math>9.61</math> <math>1.38E.04</math> <math>0.1</math></td><td>31 <math>12</math> <math>2148</math> <math>21,20001</math> <math>1.38E.04</math> <math>0.18</math> <math>0.18</math> <math>31</math> <math>15</math> <math>2161</math> <math>21,30001</math> <math>1.38E.04</math> <math>0.18</math> <math>0.18</math> <math>31</math> <math>15</math> <math>2161</math> <math>21,3001</math> <math>38E.04</math> <math>0.18</math> <math>0.18</math> <math>31</math> <math>17</math> <math>2153</math> <math>2201</math> <math>38E.04</math> <math>0.18</math> <math>0.18</math> <math>5</math> <math>13</math> <math>2269</math> <math>21,29996</math> <math>38E.04</math> <math>0.18</math> <math>0.18</math> <math>5</math> <math>16</math> <math>2271</math> <math>2234</math> <math>38E.04</math> <math>0.18</math> <math>0.18</math> <math>5</math> <math>17</math> <math>2277</math> <math>2270001</math> <math>38E.03</math> <math>961</math> <math>1.48</math> <math>1.38E.04</math> <math>0.18</math> <math>5</math> <math>17</math> <math>22772</math> <math>2270001</math> <math>38E.03</math> <math>961</math> <math>1.38E.04</math> <math>0.18</math> <math>5</math> <math>17</math> <math>22772</math> <math>2270001</math> <math>38E.03</math> <math>961</math> <math>1.38E.04</math> <math>0.18</math> <math>6</math> <math>18</math> <math>22772</math> <math>2029990</math> <math>138E.03</math> <math>961</math> <math>1.38E.04</math> <math>0.18</math> <math>8</math></td><td>31         12         2148         21.20001         1.38E-03         961         1.38E-04         0.18           31         15         2149         21.700001         1.38E-03         961         1.38E-04         0.18           31         17         2153         22.4         1.38E-03         961         1.38E-04         0.18           5         14         2770         23.54         1.38E-03         961         1.38E-04         0.18           5         14         2270         23.44         1.38E-03         961         1.38E-04         0.18           5         16         2277         22.34         1.38E-03         961         1.38E-04         0.18           5         16         2277         23.4         1.38E-03         961         1.38E-04         0.18           5         16         2277         23.4         1.38E-03         961         1.38E-04         0.18           6         15         2273         22.34         1.38E-03         961         1.38E-04         0.18           6         16         2277         23.7         1.38E-03         961         1.38E-04         0.18           7         248</td><td>31         12         2148         21,20001         1,36E-03         961         1,38E-04         0.16           31         15         2151         21.50001         1,38E-03         961         1,38E-04         0.16           31         17         215         2266         21.56001         366         1,38E-04         0.16         456E-06           5         16         2151         2224         1,38E-03         9.61         1,38E-04         0.16         456E-06           5         16         2271         223.61         1,38E-03         9.61         0.16         456E-06           5         16         2271         223.61         1,38E-03         9.61         0.16         456E-06           6         15         2271         2236         1,38E-03         9.61         0.16         456E-06           6         15         2273         20.296999         1,38E-03         9.61         0.16         456E-06           6         15         2274         20.296999         1,38E-03         0.16         456E-06           7         236         1,38E-03         9.61         1,38E-04         0.18         456E-06           6         &lt;</td><td>31         112         <math>2148</math> <math>21,20001</math> <math>138c.04</math> <math>0.16</math> <math>0.16</math>           31         15         <math>2169</math> <math>21,70001</math> <math>138c.03</math> <math>961</math> <math>1.38c.94</math> <math>0.16</math>           31         17         <math>2153</math> <math>2244</math> <math>38c.03</math> <math>961</math> <math>1.38c.94</math> <math>0.18</math>           5         14         <math>2770</math> <math>23693</math> <math>138c.03</math> <math>961</math> <math>1.38c.94</math> <math>0.18</math>           5         16         <math>2777</math> <math>2274</math> <math>328-36</math> <math>961</math> <math>1.38c.94</math> <math>0.18</math>           5         16         <math>2777</math> <math>22.7300001</math> <math>138c.03</math> <math>961</math> <math>1.38c.94</math> <math>0.18</math>           6         15         <math>2773</math> <math>22.732020591</math> <math>38c.03</math> <math>961</math> <math>1.38c.94</math> <math>0.18</math>           6         15         <math>2773</math> <math>20.2399991</math> <math>38c.03</math> <math>961</math> <math>1.38c.94</math> <math>0.18</math>           6         15         <math>22773</math> <math>20.2399991</math> <math>38c.03</math> <math>961</math> <math>1.38c.94</math> <math>0.18</math>           7         2295         <math>20.2399991</math> <math>138c.03</math> <math>961</math> <math>1.38c.94</math></td><td>31         12         <math>2140</math> <math>21,20001</math> <math>1362.03</math> <math>961</math> <math>1.382.44</math> <math>0.18</math>           31         15         <math>2149</math> <math>21,70001</math> <math>1382.03</math> <math>961</math> <math>1.382.44</math> <math>0.18</math>           31         17         <math>2153</math> <math>22.44</math> <math>1382.03</math> <math>961</math> <math>1.382.44</math> <math>0.18</math>           5         14         <math>2270</math> <math>2234</math> <math>1382.03</math> <math>961</math> <math>1.382.64</math> <math>0.18</math>           5         14         <math>2277</math> <math>2234</math> <math>1382.03</math> <math>961</math> <math>1.382.64</math> <math>0.18</math>           5         16         <math>2277</math> <math>2273</math> <math>1.382.03</math> <math>961</math> <math>1.382.64</math> <math>0.16</math>           5         16         <math>2277</math> <math>2273</math> <math>1.382.03</math> <math>961</math> <math>1.382.64</math> <math>0.16</math>           6         17         <math>2277</math> <math>2270</math> <math>1.382.03</math> <math>961</math> <math>1.382.64</math> <math>0.16</math>           6         17         <math>2277</math> <math>2270301</math> <math>1.382.03</math> <math>961</math> <math>1.382.64</math> <math>0.16</math>           6         18         <math>2774</math> <math>2229309301         <math>1.382.03</math> <math>961</math> </math></td><td>31         11         2         2148         <math>21,20001</math>         1,38E,03         961         1,38E,04         0.18           31         11         2         2161         21,0001         1,38E,03         961         1,38E,04         0.18           31         17         2153         2161         2161         21,001         1,38E,03         961         1,38E,04         0.18           5         14         2270         2266         1,38E,03         961         1,38E,04         0.18           5         15         2271         2216         1,38E,03         961         1,38E,04         0.18           5         16         2277         2216         1,38E,03         961         1,38E,04         0.18           6         15         2271         2216         1,38E,03         961         1,38E,04         0.18           6         15         2273         2236999         1,38E,03         961         1,38E,04         0.16         4,56E,06           6         16         2773         2274         2028999         1,38E,03         961         1,38E,04         0.16           7         2773         2271         202899         1,38E,03<td>31         11         2148         21.200001         1.38E-03         9.61         1.38E-04         0.18           31         13         2.148         2.1700001         1.38E-03    
    9.61         1.38E-04         0.18           31         17         2.153         2.10001         1.38E-03         9.61         1.38E-04         0.18           5         14         2.770         2.316         1.38E-03         9.61         1.38E-04         0.18           5         14         2.770         2.334         1.38E-03         9.61         1.38E-04         0.18           5         16         2.277         2.273         2.306         1.38E-03         9.61         1.38E-04         0.18           5         16         2.277         2.273         2.30699         1.38E-03         9.61         1.38E-04         0.18           6         15         2.274         2.274         2.273         2.30699         1.38E-03         9.61         1.38E-04         0.18           6         15         2.274         2.274         2.274         2.274         2.276         0.18           7         2.36999         1.38E-03         9.61         1.38E-04         0</td><td>31         11         2148         21,20001         138-03         9.61         138-04         0.18           31         16         215         21,30001         138-03         9.61         138-04         0.18           31         17         2163         2101         38-03         9.61         138-04         0.18           5         14         2270         23.61         3.86-03         9.61         1.36-04         0.18           5         14         2270         23.61         3.86-03         9.61         1.36-04         0.18           5         16         2272         22.00001         1.36-03         9.61         1.36-04         0.18           5         17         2272         22.00001         1.36-03         9.61         1.36-04         0.18           6         217         227         22.00001         1.36-03         9.61         1.36-04         0.18           6         16         2274         20.20809         1.36-03         9.61         1.36-04         0.18           7         18         2274         20.20809         1.36-03         9.61         1.36-04         0.18           8         2274</td><td>31         12         2148         21.00001         1.38E-03         9.61         1.38E-04         0.18           31         15         2169         21.00001         1.38E-03         9.61         1.38E-04         0.18           5         13         2.553         2.563         2.661         3.61         1.38E-03         0.16         4.56E-06           5         14         2.770         2.361         1.38E-03         9.61         1.38E-04         0.18         4.56E-06           5         16         2.771         2.7003         9.61         1.38E-04         0.18         4.56E-06           5         16         2.771         2.7003         9.61         1.38E-04         0.18         4.56E-06           6         15         2.77         2.7003         9.61         1.38E-04         0.18         4.56E-06           6         15         2.77         2.7003         9.61         1.38E-04         0.18         4.56E-06           6         15         2.77         2.722         1.38E-03         0.18         4.56E-06           7         272         2.723         1.38E-03         9.61         1.38E-04         0.18         4.56E-06      &lt;</td><td>31         12         2148         21,20001         1,38E,03         961         1,38E,04         0,19           31         13         2161         2100001         138E,03         961         1,38E,04         0,19           5         13         2215         2201         138E,03         961         1,38E,04         0,19           5         14         2270         2234         1,38E,03         961         1,38E,04         0,19           5         14         2270         2234         1,38E,03         961         1,38E,04         0,19           6         15         2277         2270001         1,38E,03         961         1,38E,04         0,19           6         17         2273         2203         961         1,38E,04         0,18           6         17         2273         2203         961         1,38E,04         0,18           7         19         277         2003         138E,03         961         1,38E,04         0,18           6         15         2273         2029999         138E,03         961         1,38E,04         0,18           7         14         2382         27286991         138E,03</td><td>31         11         22         27.44         27.00001         1.38E-03         9.61         1.38E-04         0.18           31         13         21         20001         1.38E-03         9.61         1.38E-04         0.18           31         13         2161         2.0001         1.38E-03         9.61         1.38E-04         0.18           5         13         2278         2.21         32003         9.61         1.38E-04         0.18           5         14         2270         223         1.38E-03         9.61         1.38E-04         0.18           5         17         2273         2270034         1.38E-03         9.61         1.38E-04         0.18           6         16         2772         2270304         1.38E-03         9.61         1.38E-04         0.18           6         13         2273         2003069         1.38E-03         9.61         1.38E-04         0.18           7         24         2382         2036969         1.38E-03         9.61         1.38E-04         0.18           7         24         2382         2036969         1.38E-03         9.61         1.38E-04         0.18           7&lt;</td><td>31         12         <math>2148</math> <math>27.30001</math> <math>386.04</math> <math>018</math> <math>010</math> <math>1386.04</math> <math>018</math>           31         13         23.48         <math>27.700001</math> <math>386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           5         14         <math>2277</math> <math>2036</math> <math>386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           5         14         <math>2277</math> <math>2336</math> <math>386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           5         14         <math>2277</math> <math>2336</math> <math>386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           6         17         <math>22773</math> <math>2386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           6         17         <math>22773</math> <math>2386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           7         18         <math>2277</math> <math>2273</math> <math>3286.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           9         1         <math>2277</math> <math>2273</math> <math>3286.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           9         1         <math>2267</math> <math>27398696</math> <math>1386.04</math> <math>018</math> <math>1386.04</math> <math>018</math></td><td>31         12         <math>2148</math> <math>27,00001</math> <math>138E,00</math>         961         <math>138E,04</math>         018           31         13         2148         <math>27,00001</math> <math>138E,03</math>         961         <math>138E,04</math>         018           31         14         <math>2170</math> <math>2361</math> <math>38E,03</math>         961         <math>138E,04</math>         018           5         14         <math>2270</math> <math>2361</math> <math>38E,03</math>         961         <math>138E,04</math>         018           5         14         <math>2272</math> <math>2270001</math> <math>38E,03</math>         961         <math>138E,04</math>         018           6         15         <math>2272</math> <math>2270001</math> <math>38E,03</math>         961         <math>138E,04</math>         018           6         15         <math>2272</math> <math>2203996</math> <math>138E,03</math>         961         <math>138E,04</math>         018           6         14         <math>2272</math> <math>22730966</math> <math>138E,03</math>         961         <math>138E,04</math>         018           7         14         <math>2276</math> <math>21726,04</math> <math>1,48</math> <math>138E,04</math>         018           9         2         <math>2272</math> <math>22729996</math> <math>138E,04</math>         018         <math>438E,06</math>           9         14&lt;</td><td>31         12         2140         21,00001         1,38E,04         0118         138E,04         0118           31         13         2140         21,00001         1,38E,03         9.61         1,38E,04         0.18           31         13         2140         27,001         1,38E,03         9.61         1,38E,04         0.18           5         14         2270         2276         31.8E,03         9.61         1,38E,04         0.18           5         16         2277         227001         1,38E,03         9.61         1,38E,04         0.18           5         16         2277         227001         1,38E,03         9.61         1,38E,04         0.18           6         15         2277         2270001         1,38E,03         9.61         1,38E,04         0.18           6         15         2277         2270001         1,38E,03         9.61         1,12E,04         1.61         1,38E,04         0.18           6         15         2274         20.308691         1,38E,03         9.61         1,38E,04         0.18         1,456E,06           7         2274         20.3286901         1,38E,03         9.61         1,28E,04</td><td>31         12         2148         21,00001         138:00         138:04         0.18           31         13         2148         21,00001         138:03         9.61         138:04         0.18           31         13         2148         21,00001         138:03         9.61         138:04         0.18           5         13         2163         138:03         9.61         2.17:04         138:04         0.18           5         16         2277         2270         138:03         9.61         138:04         0.18        
  5         18         2773         22.66         9.61         138:04         0.18         138:04         0.19           6         17         2273         22.6669         138:03         9.61         138:04         0.19         14.66           6         13         2773         22.6669         138:03         9.61         138:04         0.19         14.66           7         2235         2236699         138:03         9.61         138:04         0.19         14.66         0.16           9         2         138:04         0.18         138:04         0.19         138:04         0.19         1</td><td>31         12         2148         21,00001         38E-03         961         1,38E-04         0.18           31         15         216         2,100001         38E-03         961         1,38E-04         0.18           31         16         2276         2,266         1,38E-04         0.18         1,38E-04         0.18           5         16         2273         22,10001         38E-03         961         1,38E-04         0.18           5         16         2273         22,10001         38E-03         961         1,38E-04         0.18           6         16         2273         22,100001         38E-03         961         1,38E-04         0.18           6         16         2273         22,100001         38E-03         961         1,38E-04         0.18           6         16         2273         22,100001         38E-03         961         1,38E-04         0.18         456E-06           7         2245         20,298696         1,38E-03         961         1,38E-04         0.18         456E-06           7         2247         2272         200001         38E-03         0.18         456E-06         0.18         456E-06</td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td>31         12         2.48         71,20001         1.38E,40         0.16         1.38E,40         0.16           31         15         2.48         71,20001         1.38E,40         0.16         1.38E,40         0.16           5         13         2.51         2.24         1.38E,40         0.16         1.38E,40         0.16           6         16         2.27         2.24         1.38E,40         9.61         1.38E,40         0.16           5         17         2.260         2.34         3.8E,40         9.61         1.38E,40         0.16           6         16         2.27         2.271         2.24         3.8E,40         9.61         1.38E,40         0.16           7         16         2.27         2.274         3.8E,40         9.61         1.38E,40         0.16           6         16         2.77         2.216         3.8E,40         9.61         1.38E,40         0.16           7         2.86         2.155         3.7266696         1.38E,40         0.16         4.58E,40           9         1         2.72         2.7201         3.8E,40         9.61         1.48E,40         0.16           1         2.72&lt;</td><td>1.38E.03         9.61         <math>1.38E.04</math>         0.18           <math>1.38E.03</math>         9.61         <math>1.38E.04</math>         0.18           <td< td=""></td<></td></td></t<> | 31 $12$ $2148$ $21,200001$ $1.38E.03$ $9.61$ $1.38E.04$ $0.16$ $31$ $15$ $2153$ $22.44$ $21,138E.03$ $9.61$ $1.38E.04$ $0.16$ $5$ $13$ $2.743$ $2.153$ $22.24$ $1.38E.03$ $9.61$ $1.38E.04$ $0.16$ $5$ $14$ $2.273$ $2.24$ $1.38E.03$ $9.61$ $1.38E.04$ $0.16$ $5$ $14$ $2.277$ $2.234$ $1.38E.03$ $9.61$ $1.38E.04$ $0.16$ $5$ $16$ $2.277$ $2.271$ $2.271$ $2.271$ $2.274$ $0.18$ $4.59E.06$ $6$ $15$ $2.273$ $2.215$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $4.59E.06$ $6$ $15$ $2.274$ $2.0289999$ $1.38E.03$ $9.61$ $1.38E.04$ $0.18$ $4.59E.06$ $6$ $15$ $2.274$ $2.0289999$ $1.38E.03$ $9.61$ $1.38E.04$ $0.1$ | 31 $12$ $2148$ $21,20001$ $1.38E.04$ $0.18$ $0.18$ $31$ $15$ $2161$ $21,30001$ $1.38E.04$ $0.18$ $0.18$ $31$ $15$ $2161$ $21,3001$ $38E.04$ $0.18$ $0.18$ $31$ $17$ $2153$ $2201$ $38E.04$ $0.18$ $0.18$ $5$ $13$ $2269$ $21,29996$ $38E.04$ $0.18$ $0.18$ $5$ $16$ $2271$ $2234$ $38E.04$ $0.18$ $0.18$ $5$ $17$ $2277$ $2270001$ $38E.03$ $961$ $1.48$ $1.38E.04$ $0.18$ $5$ $17$ $22772$ $2270001$ $38E.03$ $961$ $1.38E.04$ $0.18$ $5$ $17$ $22772$ $2270001$ $38E.03$ $961$ $1.38E.04$ $0.18$ $6$ $18$ $22772$ $2029990$ $138E.03$ $961$ $1.38E.04$ $0.18$ $8$ | 31         12         2148         21.20001         1.38E-03         961         1.38E-04         0.18           31         15         2149         21.700001         1.38E-03         961         1.38E-04         0.18           31         17         2153         22.4         1.38E-03         961         1.38E-04         0.18           5         14         2770         23.54         1.38E-03         961         1.38E-04         0.18           5         14         2270         23.44         1.38E-03         961         1.38E-04         0.18           5         16         2277         22.34         1.38E-03         961         1.38E-04         0.18           5         16         2277         23.4         1.38E-03         961         1.38E-04         0.18           5         16         2277         23.4         1.38E-03         961         1.38E-04         0.18           6         15         2273         22.34         1.38E-03         961         1.38E-04         0.18           6         16         2277         23.7         1.38E-03         961         1.38E-04         0.18           7         248 | 31         12         2148         21,20001         1,36E-03         961         1,38E-04         0.16           31         15         2151         21.50001         1,38E-03         961         1,38E-04         0.16           31         17         215         2266         21.56001         366         1,38E-04         0.16         456E-06           5         16         2151         2224         1,38E-03         9.61         1,38E-04         0.16         456E-06           5         16         2271         223.61         1,38E-03         9.61         0.16         456E-06           5         16         2271         223.61         1,38E-03         9.61         0.16         456E-06           6         15         2271         2236         1,38E-03         9.61         0.16         456E-06           6         15         2273         20.296999         1,38E-03         9.61         0.16         456E-06           6         15         2274         20.296999         1,38E-03         0.16         456E-06           7         236         1,38E-03         9.61         1,38E-04         0.18         456E-06           6         < | 31         112 $2148$ $21,20001$ $138c.04$ $0.16$ $0.16$ 31         15 $2169$ $21,70001$ $138c.03$ $961$ $1.38c.94$ $0.16$ 31         17 $2153$ $2244$ $38c.03$ $961$ $1.38c.94$ $0.18$ 5         14 $2770$ $23693$ $138c.03$ $961$ $1.38c.94$ $0.18$ 5         16 $2777$ $2274$ $328-36$ $961$ $1.38c.94$ $0.18$ 5         16 $2777$ $22.7300001$ $138c.03$ $961$ $1.38c.94$ $0.18$ 6         15 $2773$ $22.732020591$ $38c.03$ $961$ $1.38c.94$ $0.18$ 6         15 $2773$ $20.2399991$ $38c.03$ $961$ $1.38c.94$ $0.18$ 6         15 $22773$ $20.2399991$ $38c.03$ $961$ $1.38c.94$ $0.18$ 7         2295 $20.2399991$ $138c.03$ $961$ $1.38c.94$ | 31         12 $2140$ $21,20001$ $1362.03$ $961$ $1.382.44$ $0.18$ 31         15 $2149$ $21,70001$ $1382.03$ $961$ $1.382.44$ $0.18$ 31         17 $2153$ $22.44$ $1382.03$ $961$ $1.382.44$ $0.18$ 5         14 $2270$ $2234$ $1382.03$ $961$ $1.382.64$ $0.18$ 5         14 $2277$ $2234$ $1382.03$ $961$ $1.382.64$ $0.18$ 5         16 $2277$ $2273$ $1.382.03$ $961$ $1.382.64$ $0.16$ 5         16 $2277$ $2273$ $1.382.03$ $961$ $1.382.64$ $0.16$ 6         17 $2277$ $2270$ $1.382.03$ $961$ $1.382.64$ $0.16$ 6         17 $2277$ $2270301$ $1.382.03$ $961$ $1.382.64$ $0.16$ 6         18 $2774$ $2229309301         1.382.03 961 $ | 31         11         2         2148 $21,20001$ 1,38E,03         961         1,38E,04         0.18           31         11         2         2161         21,0001         1,38E,03         961         1,38E,04         0.18           31         17         2153         2161         2161         21,001         1,38E,03         961         1,38E,04         0.18           5         14         2270         2266         1,38E,03         961         1,38E,04         0.18           5         15         2271         2216         1,38E,03         961         1,38E,04         0.18           5         16         2277         2216         1,38E,03         961         1,38E,04         0.18           6         15         2271         2216         1,38E,03         961         1,38E,04         0.18           6         15         2273         2236999         1,38E,03         961         1,38E,04         0.16         4,56E,06           6         16         2773         2274         2028999         1,38E,03         961         1,38E,04         0.16           7         2773         2271         202899         1,38E,03 <td>31         11         2148         21.200001         1.38E-03         9.61         1.38E-04         0.18           31         13         2.148         2.1700001         1.38E-03         9.61         1.38E-04         0.18           31         17         2.153         2.10001         1.38E-03         9.61         1.38E-04         0.18           5         14         2.770         2.316         1.38E-03         9.61         1.38E-04         0.18           5         14         2.770         2.334         1.38E-03         9.61         1.38E-04         0.18           5         16         2.277         2.273         2.306         1.38E-03         9.61         1.38E-04         0.18           5         16         2.277         2.273         2.30699         1.38E-03         9.61         1.38E-04         0.18           6         15         2.274         2.274         2.273         2.30699         1.38E-03         9.61         1.38E-04         0.18           6         15     
   2.274         2.274         2.274         2.274         2.276         0.18           7         2.36999         1.38E-03         9.61         1.38E-04         0</td> <td>31         11         2148         21,20001         138-03         9.61         138-04         0.18           31         16         215         21,30001         138-03         9.61         138-04         0.18           31         17         2163         2101         38-03         9.61         138-04         0.18           5         14         2270         23.61         3.86-03         9.61         1.36-04         0.18           5         14         2270         23.61         3.86-03         9.61         1.36-04         0.18           5         16         2272         22.00001         1.36-03         9.61         1.36-04         0.18           5         17         2272         22.00001         1.36-03         9.61         1.36-04         0.18           6         217         227         22.00001         1.36-03         9.61         1.36-04         0.18           6         16         2274         20.20809         1.36-03         9.61         1.36-04         0.18           7         18         2274         20.20809         1.36-03         9.61         1.36-04         0.18           8         2274</td> <td>31         12         2148         21.00001         1.38E-03         9.61         1.38E-04         0.18           31         15         2169         21.00001         1.38E-03         9.61         1.38E-04         0.18           5         13         2.553         2.563         2.661         3.61         1.38E-03         0.16         4.56E-06           5         14         2.770         2.361         1.38E-03         9.61         1.38E-04         0.18         4.56E-06           5         16         2.771         2.7003         9.61         1.38E-04         0.18         4.56E-06           5         16         2.771         2.7003         9.61         1.38E-04         0.18         4.56E-06           6         15         2.77         2.7003         9.61         1.38E-04         0.18         4.56E-06           6         15         2.77         2.7003         9.61         1.38E-04         0.18         4.56E-06           6         15         2.77         2.722         1.38E-03         0.18         4.56E-06           7         272         2.723         1.38E-03         9.61         1.38E-04         0.18         4.56E-06      &lt;</td> <td>31         12         2148         21,20001         1,38E,03         961         1,38E,04         0,19           31         13         2161         2100001         138E,03         961         1,38E,04         0,19           5         13         2215         2201         138E,03         961         1,38E,04         0,19           5         14         2270         2234         1,38E,03         961         1,38E,04         0,19           5         14         2270         2234         1,38E,03         961         1,38E,04         0,19           6         15         2277         2270001         1,38E,03         961         1,38E,04         0,19           6         17         2273         2203         961         1,38E,04         0,18           6         17         2273         2203         961         1,38E,04         0,18           7         19         277         2003         138E,03         961         1,38E,04         0,18           6         15         2273         2029999         138E,03         961         1,38E,04         0,18           7         14         2382         27286991         138E,03</td> <td>31         11         22         27.44         27.00001         1.38E-03         9.61         1.38E-04         0.18           31         13         21         20001         1.38E-03         9.61         1.38E-04         0.18           31         13         2161         2.0001         1.38E-03         9.61         1.38E-04         0.18           5         13         2278         2.21         32003         9.61         1.38E-04         0.18           5         14         2270         223         1.38E-03         9.61         1.38E-04         0.18           5         17         2273         2270034         1.38E-03         9.61         1.38E-04         0.18           6         16         2772         2270304         1.38E-03         9.61         1.38E-04         0.18           6         13         2273         2003069         1.38E-03         9.61         1.38E-04         0.18           7         24         2382         2036969         1.38E-03         9.61         1.38E-04         0.18           7         24         2382         2036969         1.38E-03         9.61         1.38E-04         0.18           7&lt;</td> <td>31         12         <math>2148</math> <math>27.30001</math> <math>386.04</math> <math>018</math> <math>010</math> <math>1386.04</math> <math>018</math>           31         13         23.48         <math>27.700001</math> <math>386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           5         14         <math>2277</math> <math>2036</math> <math>386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           5         14         <math>2277</math> <math>2336</math> <math>386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           5         14         <math>2277</math> <math>2336</math> <math>386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           6         17         <math>22773</math> <math>2386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           6         17         <math>22773</math> <math>2386.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           7         18         <math>2277</math> <math>2273</math> <math>3286.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           9         1         <math>2277</math> <math>2273</math> <math>3286.03</math> <math>961</math> <math>1386.04</math> <math>018</math>           9         1         <math>2267</math> <math>27398696</math> <math>1386.04</math> <math>018</math> <math>1386.04</math> <math>018</math></td> <td>31         12         <math>2148</math> <math>27,00001</math> <math>138E,00</math>         961         <math>138E,04</math>         018           31         13         2148         <math>27,00001</math> <math>138E,03</math>         961         <math>138E,04</math>         018           31         14         <math>2170</math> <math>2361</math> <math>38E,03</math>         961         <math>138E,04</math>         018           5         14         <math>2270</math> <math>2361</math> <math>38E,03</math>         961         <math>138E,04</math>         018           5         14         <math>2272</math> <math>2270001</math> <math>38E,03</math>         961         <math>138E,04</math>         018           6         15         <math>2272</math> <math>2270001</math> <math>38E,03</math>         961         <math>138E,04</math>         018           6         15         <math>2272</math> <math>2203996</math> <math>138E,03</math>         961         <math>138E,04</math>         018           6         14         <math>2272</math> <math>22730966</math> <math>138E,03</math>         961         <math>138E,04</math>         018           7         14         <math>2276</math> <math>21726,04</math> <math>1,48</math> <math>138E,04</math>         018           9         2         <math>2272</math> <math>22729996</math> <math>138E,04</math>         018         <math>438E,06</math>           9         14&lt;</td> <td>31         12         2140         21,00001         1,38E,04         0118         138E,04         0118           31         13         2140         21,00001         1,38E,03         9.61         1,38E,04         0.18           31         13         2140         27,001         1,38E,03         9.61         1,38E,04         0.18           5         14         2270         2276         31.8E,03         9.61         1,38E,04         0.18           5         16         2277         227001         1,38E,03         9.61         1,38E,04         0.18           5         16         2277         227001         1,38E,03         9.61         1,38E,04         0.18           6         15         2277         2270001         1,38E,03         9.61         1,38E,04         0.18           6         15         2277         2270001         1,38E,03         9.61         1,12E,04         1.61         1,38E,04         0.18           6         15         2274         20.308691         1,38E,03         9.61         1,38E,04         0.18         1,456E,06           7         2274         20.3286901         1,38E,03         9.61         1,28E,04</td> <td>31         12         2148         21,00001         138:00         138:04         0.18           31         13         2148         21,00001         138:03         9.61         138:04         0.18           31         13         2148         21,00001         138:03         9.61         138:04         0.18           5         13         2163         138:03         9.61         2.17:04         138:04         0.18           5         16         2277         2270         138:03         9.61         138:04         0.18           5         18         2773         22.66         9.61         138:04         0.18         138:04         0.19           6         17         2273         22.6669         138:03         9.61         138:04         0.19         14.66           6         13         2773         22.6669         138:03         9.61         138:04         0.19         14.66           7         2235         2236699         138:03         9.61         138:04         0.19         14.66         0.16           9         2         138:04         0.18         138:04         0.19         138:04         0.19         1</td> <td>31         12         2148         21,00001         38E-03         961         1,38E-04         0.18           31         15         216         2,100001         38E-03         961   
     1,38E-04         0.18           31         16         2276         2,266         1,38E-04         0.18         1,38E-04         0.18           5         16         2273         22,10001         38E-03         961         1,38E-04         0.18           5         16         2273         22,10001         38E-03         961         1,38E-04         0.18           6         16         2273         22,100001         38E-03         961         1,38E-04         0.18           6         16         2273         22,100001         38E-03         961         1,38E-04         0.18           6         16         2273         22,100001         38E-03         961         1,38E-04         0.18         456E-06           7         2245         20,298696         1,38E-03         961         1,38E-04         0.18         456E-06           7         2247         2272         200001         38E-03         0.18         456E-06         0.18         456E-06</td> <td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td> <td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td> <td>31         12         2.48         71,20001         1.38E,40         0.16         1.38E,40         0.16           31         15         2.48         71,20001         1.38E,40         0.16         1.38E,40         0.16           5         13         2.51         2.24         1.38E,40         0.16         1.38E,40         0.16           6         16         2.27         2.24         1.38E,40         9.61         1.38E,40         0.16           5         17         2.260         2.34         3.8E,40         9.61         1.38E,40         0.16           6         16         2.27         2.271         2.24         3.8E,40         9.61         1.38E,40         0.16           7         16         2.27         2.274         3.8E,40         9.61         1.38E,40         0.16           6         16         2.77         2.216         3.8E,40         9.61         1.38E,40         0.16           7         2.86         2.155         3.7266696         1.38E,40         0.16         4.58E,40           9         1         2.72         2.7201         3.8E,40         9.61         1.48E,40         0.16           1         2.72&lt;</td> <td>1.38E.03         9.61         <math>1.38E.04</math>         0.18           <math>1.38E.03</math>         9.61         <math>1.38E.04</math>         0.18           <td< td=""></td<></td> | 31         11         2148         21.200001         1.38E-03         9.61         1.38E-04         0.18           31         13         2.148         2.1700001         1.38E-03         9.61         1.38E-04         0.18           31         17         2.153         2.10001         1.38E-03         9.61         1.38E-04         0.18           5         14         2.770         2.316         1.38E-03         9.61         1.38E-04         0.18           5         14         2.770         2.334         1.38E-03         9.61         1.38E-04         0.18           5         16         2.277         2.273         2.306         1.38E-03         9.61         1.38E-04         0.18           5         16         2.277         2.273         2.30699         1.38E-03         9.61         1.38E-04         0.18           6         15         2.274         2.274         2.273         2.30699         1.38E-03         9.61         1.38E-04         0.18           6         15         2.274         2.274         2.274         2.274         2.276         0.18           7         2.36999         1.38E-03         9.61         1.38E-04         0 | 31         11         2148         21,20001         138-03         9.61         138-04         0.18           31         16         215         21,30001         138-03         9.61         138-04         0.18           31         17         2163         2101         38-03         9.61         138-04         0.18           5         14         2270         23.61         3.86-03         9.61         1.36-04         0.18           5         14         2270         23.61         3.86-03         9.61         1.36-04         0.18           5         16         2272         22.00001         1.36-03         9.61         1.36-04         0.18           5         17         2272         22.00001         1.36-03         9.61         1.36-04         0.18           6         217         227         22.00001         1.36-03         9.61         1.36-04         0.18           6         16         2274         20.20809         1.36-03         9.61         1.36-04         0.18           7         18         2274         20.20809         1.36-03         9.61         1.36-04         0.18           8         2274 | 31         12         2148         21.00001         1.38E-03         9.61         1.38E-04         0.18           31         15         2169         21.00001         1.38E-03         9.61         1.38E-04         0.18           5         13         2.553         2.563         2.661         3.61         1.38E-03         0.16         4.56E-06           5         14         2.770         2.361         1.38E-03         9.61         1.38E-04         0.18         4.56E-06           5         16         2.771         2.7003         9.61         1.38E-04         0.18         4.56E-06           5         16         2.771         2.7003         9.61         1.38E-04         0.18         4.56E-06           6         15         2.77         2.7003         9.61         1.38E-04         0.18         4.56E-06           6         15         2.77         2.7003         9.61         1.38E-04         0.18         4.56E-06           6         15         2.77         2.722         1.38E-03         0.18         4.56E-06           7         272         2.723         1.38E-03         9.61         1.38E-04         0.18         4.56E-06      < | 31         12         2148         21,20001         1,38E,03         961         1,38E,04         0,19           31         13         2161         2100001         138E,03         961         1,38E,04         0,19           5         13         2215         2201         138E,03         961         1,38E,04         0,19           5         14         2270         2234         1,38E,03         961         1,38E,04         0,19           5         14         2270         2234         1,38E,03         961         1,38E,04         0,19           6         15         2277         2270001         1,38E,03         961         1,38E,04         0,19           6         17         2273         2203         961         1,38E,04         0,18           6         17         2273         2203         961         1,38E,04         0,18           7         19         277         2003         138E,03         961         1,38E,04         0,18           6         15         2273         2029999         138E,03         961         1,38E,04         0,18           7         14         2382         27286991         138E,03 | 31         11         22         27.44         27.00001         1.38E-03         9.61         1.38E-04         0.18           31         13         21         20001         1.38E-03         9.61         1.38E-04         0.18           31         13         2161         2.0001         1.38E-03         9.61         1.38E-04         0.18           5         13         2278         2.21         32003         9.61         1.38E-04         0.18           5         14         2270         223         1.38E-03         9.61         1.38E-04         0.18           5         17         2273         2270034         1.38E-03         9.61         1.38E-04         0.18           6         16         2772         2270304         1.38E-03         9.61         1.38E-04         0.18           6         13         2273         2003069         1.38E-03         9.61         1.38E-04         0.18           7         24         2382         2036969         1.38E-03         9.61         1.38E-04         0.18           7         24         2382         2036969         1.38E-03         9.61         1.38E-04         0.18           7< | 31         12 $2148$ $27.30001$ $386.04$ $018$ $010$ $1386.04$ $018$ 31         13         23.48 $27.700001$ $386.03$ $961$ $1386.04$ $018$ 5         14 $2277$ $2036$ $386.03$ $961$ $1386.04$ $018$ 5         14 $2277$ $2336$ $386.03$ $961$ $1386.04$ $018$ 5         14 $2277$ $2336$ $386.03$ $961$ $1386.04$ $018$ 6         17 $22773$ $2386.03$ $961$ $1386.04$ $018$ 6         17 $22773$ $2386.03$ $961$ $1386.04$ $018$ 7         18 $2277$ $2273$ $3286.03$ $961$ $1386.04$ $018$ 9         1 $2277$ $2273$ $3286.03$ $961$ $1386.04$ $018$ 9         1 $2267$ $27398696$ $1386.04$ $018$ $1386.04$ $018$ | 31         12 $2148$ $27,00001$ $138E,00$ 961 $138E,04$ 018           31         13         2148 $27,00001$ $138E,03$ 961 $138E,04$ 018           31         14 $2170$ $2361$ $38E,03$ 961 $138E,04$ 018           5         14 $2270$ $2361$ $38E,03$ 961 $138E,04$ 018           5         14 $2272$ $2270001$ $38E,03$ 961 $138E,04$ 018           6         15 $2272$ $2270001$ $38E,03$ 961 $138E,04$ 018           6         15 $2272$ $2203996$ $138E,03$ 961 $138E,04$ 018           6         14 $2272$ $22730966$ $138E,03$ 961 $138E,04$ 018           7         14 $2276$ $21726,04$ $1,48$ $138E,04$ 018           9         2 $2272$ $22729996$ $138E,04$ 018 $438E,06$ 9         14< | 31         12         2140         21,00001         1,38E,04         0118         138E,04         0118           31         13         2140         21,00001         1,38E,03         9.61         1,38E,04         0.18           31         13         2140         27,001         1,38E,03         9.61         1,38E,04         0.18           5         14         2270         2276         31.8E,03         9.61         1,38E,04         0.18           5         16         2277         227001         1,38E,03         9.61         1,38E,04         0.18           5         16         2277         227001         1,38E,03
        9.61         1,38E,04         0.18           6         15         2277         2270001         1,38E,03         9.61         1,38E,04         0.18           6         15         2277         2270001         1,38E,03         9.61         1,12E,04         1.61         1,38E,04         0.18           6         15         2274         20.308691         1,38E,03         9.61         1,38E,04         0.18         1,456E,06           7         2274         20.3286901         1,38E,03         9.61         1,28E,04 | 31         12         2148         21,00001         138:00         138:04         0.18           31         13         2148         21,00001         138:03         9.61         138:04         0.18           31         13         2148         21,00001         138:03         9.61         138:04         0.18           5         13         2163         138:03         9.61         2.17:04         138:04         0.18           5         16         2277         2270         138:03         9.61         138:04         0.18           5         18         2773         22.66         9.61         138:04         0.18         138:04         0.19           6         17         2273         22.6669         138:03         9.61         138:04         0.19         14.66           6         13         2773         22.6669         138:03         9.61         138:04         0.19         14.66           7         2235         2236699         138:03         9.61         138:04         0.19         14.66         0.16           9         2         138:04         0.18         138:04         0.19         138:04         0.19         1 | 31         12         2148         21,00001         38E-03         961         1,38E-04         0.18           31         15         216         2,100001         38E-03         961         1,38E-04         0.18           31         16         2276         2,266         1,38E-04         0.18         1,38E-04         0.18           5         16         2273         22,10001         38E-03         961         1,38E-04         0.18           5         16         2273         22,10001         38E-03         961         1,38E-04         0.18           6         16         2273         22,100001         38E-03         961         1,38E-04         0.18           6         16         2273         22,100001         38E-03         961         1,38E-04         0.18           6         16         2273         22,100001         38E-03         961         1,38E-04         0.18         456E-06           7         2245         20,298696         1,38E-03         961         1,38E-04         0.18         456E-06           7         2247         2272         200001         38E-03         0.18         456E-06         0.18         456E-06 | $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | 31         12         2.48         71,20001         1.38E,40         0.16         1.38E,40         0.16           31         15         2.48         71,20001         1.38E,40         0.16         1.38E,40         0.16           5         13         2.51         2.24         1.38E,40         0.16         1.38E,40         0.16           6         16         2.27         2.24         1.38E,40         9.61         1.38E,40         0.16           5         17         2.260         2.34         3.8E,40         9.61         1.38E,40         0.16           6         16         2.27         2.271         2.24         3.8E,40         9.61         1.38E,40         0.16           7         16         2.27         2.274         3.8E,40         9.61         1.38E,40         0.16           6         16         2.77         2.216         3.8E,40         9.61         1.38E,40         0.16           7         2.86         2.155         3.7266696         1.38E,40         0.16         4.58E,40           9         1         2.72         2.7201         3.8E,40         9.61         1.48E,40         0.16           1         2.72< | 1.38E.03         9.61 $1.38E.04$ 0.18 $1.38E.03$ 9.61 $1.38E.04$ 0.18 <td< td=""></td<> |

Stabilized soil, spike-corrected emission factors

Table A.12 - Polygon 5 - CCHD Station pl

					Jotal 🖉	tons	41.70	41.70	36.22	36.22	36.22	36.22	41.70	41.70	66.73	66.73	36.22	41.70	41.70	41.70	36.22	36.22	41.70	36.22	36.22	36.22	41.70	41.70	41.70	41.70	41.70	41.70	1010 10	
Stabilized		0.16	4905.92	Spike	Emission	ton	0.02	0.02					0.02	0.02				0.02	0.02	0.02			0.02				0.02	0.02	0.02	0.02	0.02	0.02		_
Stabilized			-	Spike		(ton/ac)	4.59E-06	4.59E-06					4.59E-06	4.59E-06				4.59E-06	4.59E-06	4.59E-06			4.59E-06					4.59E-06	4.59E-06		4.59E-06	4.59E-06		-
Stabilized		0.16	4905.92	Steady	Emission	ton	0.68	0.68	0.68	0.68	0.68	0.68	0.68	0.68	0.53	0.53	0.68	0.68	0.68	0.68	0.68	0.68	0.68	0.68	0.68	0.68	0.68	0.68	0.68	0.68	0.68	0.68		
Stabilized				Steady	Factor	(ton/achr)	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.09E-04	1.09E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04		
Stable		0.84	25756.08	Spike	Emission	ton	5.46	5.46					5.46	5.46				5.46	5.46	5.46			5.46				5.46	5.46	5.46	5.46	5.46	5.46		
Stable				Spike	Factor	(ton/ac)	2.12E-04	2.12E-04					2.12E-04	2.12E-04				2.12E-04	2.12E-04	2.12E-04			2.12E-04				2.12E-04	2.12E-04	2.12E-04	2.12E-04	2.12E-04	2.12E-04		
Stable		0.84	25756.08	Steady	Emission	ton	35.54	35.54	35.54	35.54	35.54	35.54	35.54	35.54	66.19	66.19	35.54	35.54	35.54	35.54	35.54	35.54	35.54	35.54	35.54	35.54	35.54	35.54	35.54	35.54	35.54	35.54		
Stable				Steady	Factor	(ton/achr)	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	2.57E-03	2.57E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03				1.38E-03								
		fraction	Area (acres)			wind (man)	20.299999	23.1	24.200001	22.299999	22.299999	8	20.299999	22.9	58	29.4	22.1	23.5	21.299999	20.1	22.4	21.1	20.6	8	20.9	23.6	21.1	20.9	20.20001		21.5	22.20001		
	acres					Cim hur	174	491	492	493	494	495	958	1330	1331	1332	1333	1486	1622	1886	1887	1888	2124	2146	2149	2150	2351	2820	2942	3211	3500	8180		
	30662 a	0.84	0.16			Hour	9	11	12	13	14	15	8	9	11	12	13	8	14	14	15	16	12	ę	13	14	8	12	4	19	8	20		
1999	vacant land area	stable fraction	unstable fraction			Dav 1		21	31	21	21	21	0	8	25	12	8	ñ	6	8	8	8	900	31	31	31	60	38		4	8	2		
PM PM-10	2					Month	1		•			-	2	2	2			6	(C)	C			e	e	e	r	4	•	2	2		12		Total

Stabilized soil, spike-corrected emission factors

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Table A.13 - Polygon 12 - CCHD Station pm

					Total	tons	9.20	7.99	9.20	7.99	7.99	9.20	9.20	7.99	7.99	9.20	2.99	7.99	7.99	2.99	2.99	7.99	14.72	66.7	7.99	7.99	9.20	7.99	9.20	9.20	9.20	7.99	225.34
Stabilized		0.16	1082.16	Spike	Emission	ton	0.0		0.00			0.00	0.00			0.0											0.00		0.00	00.00	0.0		
Stabilized Stabilized Stabilized Stabilized				Spike	Factor	(ton/ac)	4.59E-06		4.59E-06			4.59E-06	4.59E-06			4.59E-06											4.59E-06		4.59E-06	4.59E-06	4.59E-06		
Stabilized		0.16	1082.16	Steady	Emission	bu	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.12	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
Stabilized				Steady	Factor	(ton/ac/hr)	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.09E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	
Stable		0.84	5681.34	Spike	Emission	ton	1.20		1.20			1.20	1.20			1.20											1.20		1.20	1.20	1.20		
Stable				Spike	Eactor	(ton/ac)	2.12E-04		2.12E-04			2.12E-04	2.12E-04			2.12E-04											2.12E-04		2.12E-04	2.12E-04	2.12E-04		
Stable		0.84	5681.34	Steady	Emission	ton	7.84	7.84	7.84	7.84	7.84	7.84	7.84	7.84	7.84	7.84	7.84	7.84	7.84	7.84	7.84	7.84	14.60	7.84	7.84	7.84	7.84	7.84	7.84	7.84	7.84	7.84	
Stable				Steady	Eactor	(ton/ac/hr)	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	2.57E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	
		fraction	Area (acres)		のである。	wind (mph)	21.1	20.700001	23	23.299999	23.299999	20.20001	20	24.200001	22.6	8	22.799999	23.799999	21.1	20.799999	20.799999	22.799999	25.200001	23.4	24.200001	20.1	20	20.700001	21.799999	20.9	23.6	23	
	acres					Cum hour	096	962	1332	1333	1334	1483	1621	1622	1623	2123	2124	2125	2127	2145	2147	2148	2149	2150	2151	2152	2363	2354	3189	3211	4982	4983	
	6763.5	0.84	0.16			Hour	24	5	12	13	14	19	13	4	15	11	12	13	15	6	11	12	13	14	15	16	-	2	21	19	14	15	
1999	vacant land area	stable fraction	unstable fraction			Ved	6	10	25	25	22	3	6	σ	6	90	90	30	90	31	31	31	31	31	31	31	6	6	13	14	27	27	
PT PM-10	0	Excel 5.0	-			Month	2	2	2	2	2	3	3	3	3	3	3	3	3	3	3	3	Э	3	3	Э	4	4	5	5	2	1	Total

# Stabilized soil, spike-corrected emission factors

Table A.14 - Polygon 10 - CCHD Station pt

01 16.49	16.49	14.32	14.32	16.49	01 16.49	01 16.49	11 16.49	16.49	16.49	10 16.49	14.32	14.32	14.32	14.32	16.49	26.39	26.39	26.39	33.12	33.12	26.39	14.32	14.32		14.32	26.39	26.39	14.32	14.32	14.32	14.32	0 31.38	14.32	14.32	32.40	14.32	
0.01	0.01			0.01	0.01	0.01	0.01	0.01	0.01	0.01					0.01									0.01								00.0					
4.59E-06	4.59E-06			4.59E-06	4.59E-06	4.59E-06	4.59E-06	4.59E-06	4.59E-06	4.59E-06					4.59E-06									4.59E-06													
0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.21	0.21	0.21	0.94	0.94	0.21	0.27	0.27	0.27	0.27	0.21	0.21	0.27	0.27	0.27	0.27	0.21	0.27	0.27	0.21	0.27	
1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.09E-04	1.09E-04	1.09E-04	4.83E-04	4.83E-04	1.09E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.09E-04	1.09E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.09E-04	1.38E-04	1.38E-04	1.09E-04	1.38E-04							
2.16	2.16			2.16	2.16	2.16	2.16	2.16	2.16	2.16					2.16									2.16								4.99					
2.12E-04	2.12E-04			2.12E-04	2.12E-04	2.12E-04	2.12E-04	2.12E-04	2.12E-04	2.12E-04					2.12E-04									2.12E-04								4.90E-04					
14.06	14.06	14.06	14,06	14.06	14.06	14.06	14.06	14.06	14.06	14.06	14.06	14.06	14.06	14.06	14.06	26.18	26.18	26.18	32.18	32.18	26.18	14.06	14.06	14.06	14.06	26.18	26.18	14.06	14.06	14.06	14.06	26.18	14.06	14.06	32.18	14.06	
1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	2.57E-03	2.57E-03	2.57E-03	3.16E-03	3.16E-03	2.57E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	2.57E-03	2.57E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	2.57E-03	1.38E-03	1.38E-03	3.16E-03	1.38E-03							
21.1	20.1	21.1	21.9	20	24	20.799999	20	20.200001	21.299999	20.4	23.4	21.799999	21.299999	22.299999	22.4	28.5	25.1	29.4	30.1	31.799999	29.5	23.200001	22	21.799999	21.1	25.9	25.200001	22.200001	22	22.200001	20.6	27.4	26.200001	21.9	31.299999	22.200001	
4117	4215	4216	4220	4406	4701	4983	5798	6923	7228	7472	7473	7474	7476	7478	7685	7686	7687	7688	7689	7690	7691	7692	7693	8022	8063	8064	8065	8073	8077	8078	8079	8180	8181	8182	8185	8186	
13	15	16	20	14	21	15	14	11	4	80	σ	10	12	14	5	9	7	8	6	10	11	12	13	9	23	24	1	6	13	14	15	20	21	22	1	2	
21	25	35	25	З	15	27	30	16	8	80	80	80	80	8	17	17	17	17	17	17	17	17	17	1	2	2	Э	Э	3	Э	3	7	7	7	8	8	
6	6	9	9	7	7	7	8	10	10	11	11	11	11	11	11	11	11	11	11	11	11	11	11	12	12	12	12	12	12	12	12	12	12	12	12	12	

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# Stabilized soil, spike-corrected emission factors

Table A.15 - Polygon 18 - CCHD Station pv

# Stabilized soil, spike-corrected emission factors

Table A.15 - Polygon 18 - CCHD Station pv

| - 1      |  | 14.32  | 14.32   | 14.32   | 14.32  | 14.32  | 26.39   | 26.39   
   
   
   | 14.32   | 14.32   
   
   
   | 14.32  | 16.49   | 14.32  | 14.32  | 14.32   | 14.32  
   
   | 14.32  | 14.32  
  | 14.32   | 14.32   | 16.49   | 16.49   | 14.32   | 14.32   | 14.32   | 14.32   | 14.32   | 14.32   | 14.32   | 14.32   | 16.49   | 14.32   | 14.32   | 16.49   | 14.32  
   | 26.39   | 26.39   | 14.32  | 26.39   | 26.39  | 31.10  |   |
|----------|--|--|---|---|--|--|---
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--|--|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---
--|---|---|--|---|--|--|---|
|          | 0.01                                   |  |   |   |  |  |   |   
   
   
   |   |   
   
   
   |  | 0.01  |  |  |   |  
   
   |  |  
  |   |   | 0.01  | 0.01  |   |   |   |   |   |   |   |   | 0.0   |   |   | 0.01  |  
   |   |   |  |   |  |  |   |
|          | 4.59E-06                               |  |   |   |  |  |   |   
   
   
   |   |   
   
   
   |  | 4.59E-06  |  |  |   |  
   
   |  |  
  |   |   | 4.59E-06  | 4.59E-06  |   |   |   |   |   |   |   | -   | 4.59E-06  |   |   | 4.59E-06  |  
   |   |   |  |   |  |  |   |
| 0.21     | 0.27                                   | 0.27   | 0.27  | 0.27  | 0.27   | 0.27   | 0.21  | 0.21  
   
   
   | 0.27  | 0.27  
   
   
   | 0.27   | 0.27  | 0.27   | 0.27   | 0.27  | 0.27   
   
   | 0.27   | 0.27   
  | 0.27  | 0.27  | 0.27  | 0.27  | 0.27  | 0.27  | 0.27  | 0.27  | 0.27  | 0.27  | 0.27  | 0.27  | 0.27  | 0.27  | 0.27  | 0.27  | 0.27   
   | 0.21  | 0.21  | 0.27   | 0.21  | 0.21   | 0.64   |   |
| 1.09E-04 | 1.38E-04                               | 1.38E-04   | 1.38E-04  | 1.38E-04  | 1.38E-04   | 1.38E-04   | 1.09E-04  | 1.09E-04  
   
   
   | 1.38E-04  | 1.38E-04  
   
   
   | 1.38E-04   | 1.38E-04  | 1.38E-04   | 1.38E-04   | 1.38E-04  | 1.38E-04   
   
   | 1.38E-04   | 1.38E-04   
  | 1.38E-04  | 1.38E-04  | 1.38E-04  | 1.38E-04  | 1.38E-04  | 1.38E-04  | 1.38E-04  | 1.38E-04  | 1.38E-04  | 1.38E-04  | 1.38E-04  | 1.38E-04  | 1.38E-04  | 1.38E-04  | 1.38E-04  | 1.38E-04  | 1.38E-04   
   | 1.09E-04  | 1.09E-04  | 1.38E-04   | 1.09E-04  | 1.09E-04   | 3.32E-04   |   |
|          | 2.16                                   |  |   |   |  |  |   |   
   
   
   |   |   
   
   
   |  | 2.16  |  |  |   |  
   
   |  |  
  |   |   | 2.16  | 2.16  |   |   |   |   |   |   |   |   | 2.16  |   |   | 2.16  |  
   |   |   |  |   |  |  |   |
|          | 2.12E-04                               |  |   |   |  |  |   |   
   
   
   |   |   
   
   
   |  | 2.12E-04  |  |  |   |  
   
   |  |  
  |   |   | 2.12E-04  | 2.12E-04  |   |   |   |   |   |   |   |   | 2.12E-04  |   |   | 2.12E-04  |  
   |   |   |  |   |  |  |   |
| 26.18    | 14.06                                  | 14.06  | 14.06   | 14.06   | 14.06  | 14.06  | 26.18   | 26.18   
   
   
   | 14.06   | 14.06   
   
   
   | 14.06  | 14.06   | 14.06  | 14.06  | 14.06   | 14.06  
   
   | 14.06  | 14.06  
  | 14.06   | 14.06   | 14.06   | 14.06   | 14.06   | 14.06   | 14.06   | 14.06   | 14.06   | 14.06   | 14.06   | 14.06   | 14.06   | 14.06   | 14.06   | 14.06   | 14.06  
   | 26.18   | 26.18   | 14.06  | 26.18   | 26.18  | 30.45  |   |
| 2.57E-03 | 1.38E-03                               | 1.38E-03   | 1.38E-03  | 1.38E-03  | 1.38E-03   | 1.38E-03   | 2.57E-03  | 2.57E-03  
   
   
   | 1.38E-03  | 1.38E-03  
   
   
   | 1.38E-03   | 1.38E-03  | 1.38E-03   | 1.38E-03   | 1.38E-03  | 1.38E-03   
   
   | 1.38E-03   | 1.38E-03   
  | 1.38E-03  | 1.38E-03  | 1.38E-03  | 1.38E-03  | 1.38E-03  | 1.38E-03  | 1.38E-03  | 1.38E-03  | 1.38E-03  | 1.38E-03  | 1.38E-03  | 1.38E-03  | 1.38E-03  | 1.38E-03  | 1.38E-03  | 1.38E-03  | 1.38E-03   
   | 2.57E-03  | 2.57E-03  | 1.38E-03   | 2.57E-03  | 2.57E-03   | 2.99E-03   |   |
| 27       | 21.4                                   | 22   | 23  | 21.5  | 23.5   | 23.299999  | 25.299999   | 26.200001   
   
   
   | 21.6  | 22.700001   
   
   
   | 22.299999  | 20.299999   | 20.700001  | 22.200001  | 24  | 22.700001  
   
   | 21.9   | 21.4   
  | 23.299999   | 20.299999   | 20.1  | 21.200001   | 23.700001   | 23.299999   | 20  | 20.9  | 21.299999   | ឌ   | 22.5  | 20.9  | 20.9  | 22.799999   | 20.700001   | 22.299999   | 24.9   
   | 27.200001   | 26.700001   | 21.700001  | 25.799999   | 29.4   | 35.799999  |   |
| 1332     | 1476                                   | 1477   | 1478  | 1479  | 1480   | 1481   | 1482  | 1483  
   
   
   | 1484  | 1487  
   
   
   | 1488   | 1607  | 1608   | 1609   | 1610  | 1611   
   
   | 1612   | 1622   
  | 1623  | 1624  | 1768  | 1885  | 1886  | 1887  | 1888  | 1889  | 1890  | 1891  | 1892  | 1912  | 1949  | 1950  | 1952  | 2121  | 2122   
   | 2123  | 2124  | 2125   | 2148  | 2149   | 2150   |   |
| 12       | 12                                     | 13   | 14  | 15  | 16   | 17   | 18  | 19  
   
   
   | 20  | 23  
   
   
   | 24   | 23  | 24   | -  | 2   | e  
   
   | 4  | 14   
  | 15  | 16  | 16  | 13  | 14  | 15  | 16  | 17  | 18  | 19  | 8   | 16  | 2   | 9   | 8   | 6   | 10   
   | 11  | 12  | 13   | 12  | 13   | 14   |   |
| 52       | 3                                      | Э  | З   | e   | 9  | e  | e   | 8   
   
   
   | e   | e   
   
   
   | е  | 80  | 80   | 0  | 6   | 6  
   
   | 6  | 6  
  | 6   | 6   | 15  | 20  | 20  | 20  | 20  | 20  | 20  | 20  | 2   | 21  | 33  | 23  | 33  | 90  | 30   
   | 30  | 30  | 90   | 31  | 31   | 31   |   |
| 2        | 3                                      | 3  | e   | e   | e  | e  | e   | 3   
   
   
   | e   | e   
   
   
   | e  | e   | e  | З  | 3   | з  
   
   | 3  | 3  
  | 9   | 3   | 3   | Э   | З   | Э   | Э   | e   | e   | e   | e   | e   | e   | e   | e   | 3   | 3  
   | 3   | 3   | e  | e   | e  | 3  |   |
|          | 261 12 1332 271 25/E-03 26.18 1.09E-04 | 23         12         1332         2/         25/E-03         26.18         1.09E-04         0.21           3         12         14/6         21.4         1.38E-03         14.06         2.12E-04         2.16         1.38E-04         0.27         4.59E-06 | Z3         12         1332         2/         2.5/E-03         2.6.18         1.08E-04         0.21           3         12         1476         21.4         1.38E-03         14.06         2.12E-04         2.16         1.38E-04         0.27         4.59E-06           3         13         1477         22         1.38E-03         14.06         1.38E-04         0.27         4.59E-06 | Z3         12         1332         2/         2.5/E-U3         2.6.18         1.09E-04         0.21           3         12         1476         21.4         1.38E-03         14.06         2.12E-04         2.16         1.38E-04         0.27         4.59E-06           3         13         1477         22         1.38E-03         14.06         1.38E-04         0.27         4.59E-06           3         14         14.06         14.06         1.38E-04         0.27         4.59E-06           3         14         1477         22         1.38E-03         14.06         1.38E-04         0.277           3         14         14.06         1.38E-04         0.277         4.59E-06 | Z3         12         1332         2/         2.5/E-U3         2.6.18         1.09E-04         0.21           3         12         1476         21.4         1.38E-03         14.06         2.16         1.38E-04         0.27         4.59E-06           3         13         1477         22         1.38E-03         14.06         2.16         1.38E-04         0.27         4.59E-06           3         14         14.06         2.16         1.38E-04         0.27         4.59E-06           3         14         14.06         14.06         1.38E-04         0.27         4.59E-06           3         14         14.06         14.06         1.38E-04         0.27         4.59E-06           3         15         1479         21.5         1.38E-03         14.06         1.38E-04         0.27 | Z3         12         1332         2/         2.5/E-U3         2.6/18         1.09E-04         0.2/         4.59E-06           3         12         14/7         22         1.38E-03         14.06         2.16         1.38E-04         0.27         4.59E-06           3         13         1477         22         1.38E-03         14.06         1.38E-04         0.27         4.59E-06           3         14         14.06         1.38E-04         0.27         4.59E-06           3         14         14.06         1.38E-04         0.27         4.59E-06           3         15         1478         23         138E-03         14.06         1.38E-04         0.27           3         16         1479         21.5         1.38E-03         14.06         1.38E-04         0.27           3         16         1480         23.5         1.38E-03         14.06         1.38E-04         0.27 | Z <sup>3</sup> 12         1332         Z/1         Z/5.16         21.6         1.09E-04         0.21           3         112         1476         21.4         1.38E-04         2.21         1.38E-04         0.27         4.59E-06           3         113         1477         22         1.38E-03         14.06         2.16         1.38E-04         0.27         4.59E-06           3         14         14.06         14.06         1.38E-04         0.27         4.59E-06           3         15         1478         23         1.38E-03         14.06         1.38E-04         0.27         5           3         16         1479         21.5         1.38E-03         14.06         1.38E-04         0.27         5           3         16         1480         23.5         1.38E-03         14.06         1.38E-04         0.27         5           3         17         1481         23.599999         1.38E-03         14.06         1.38E-04         0.27         5 | Zo         12         1332         Z/1         Z/2.5/E-U3         Z/6.18         0.21         0.21           3         112         1476         21.4         1.38E-04         0.27         4.59E-06           3         13         147         22         1.38E-03         14.06         1.38E-04         0.27         4.59E-06           3         14         14.06         1.38E-04         0.27         4.59E-06           3         15         1478         23         1.38E-03         14.06         1.38E-04         0.27         4.59E-06           3         15         1479         23         1.38E-03         14.06         1.38E-04         0.27         5.59E-06           3         16         1479         23.5         1.38E-03         14.06         1.38E-04         0.27         5.7           3         16         1480         23.5         1.38E-03         14.06         1.38E-04         0.27         7           3         18         1481         23.299999         1.38E-03         14.06         1.38E-04         0.27         7           3         18         1482         25.7E-03         26.18         0.27         1         7 </td <td>Zol         12         1332         Z/1         Z/2         <thz 2<="" th=""> <thz 2<="" th=""> <thz 2<="" th=""></thz></thz></thz></td> <td>23 <math>12</math> <math>1332</math> <math>27</math> <math>2.57E-03</math> <math>2.6.18</math> <math>1.00E-04</math> <math>0.21</math>           3         112         <math>1476</math> <math>21.4</math> <math>1.38E-04</math> <math>0.27</math> <math>459E-06</math>           3         113         <math>1477</math> <math>22</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>459E-06</math>           3         15         <math>1478</math> <math>223</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>259E-06</math>           3         16         <math>14.06</math> <math>21.4.06</math> <math>1.38E-04</math> <math>0.27</math> <math>27</math> <math>38</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>259E-06</math>           3         16         <math>1480</math> <math>23.5</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>27</math> <math>28</math>           3         17         <math>1481</math> <math>23.299999</math> <math>138E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>27</math>           3         18         <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>28</math> <math>26.18</math> <math>1.06E-04</math> <math>0.27</math> <math>28</math> <math>28</math> <math>28</math> <math>28</math><td>23 <math>12</math> <math>1332</math> <math>2.7</math> <math>2.57E-03</math> <math>2.6.18</math> <math>1.00E-04</math> <math>0.21</math>           3         112         <math>1476</math> <math>21.4</math> <math>1.38E-04</math> <math>0.27</math> <math>459E-06</math>           3         113         <math>1477</math> <math>22</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>459E-06</math>           3         15         <math>1478</math> <math>223</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>259E-06</math>           3         16         <math>1479</math> <math>223</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>276E-06</math>           3         17         <math>1480</math> <math>23.5</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>276E-03</math>           3         18         <math>1481</math> <math>23.299999</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>276E-03</math>           3         19         <math>1481</math> <math>23.57E-03</math> <math>26.18</math> <math>0.27</math> <math>0.21</math> <math>0.27</math> <math>0.27</math> <math>0.27</math> <math>0.21</math>           3         20         <math>1488</math> <math>257E-03</math></td><td>23 <math>12</math> <math>1332</math> <math>2.7</math> <math>2.57E-03</math> <math>2.6.18</math> <math>1.00E-04</math> <math>0.21</math>           3         112         <math>1476</math> <math>21.4</math> <math>1.38E-04</math> <math>0.27</math> <math>459E-06</math>           3         113         <math>1477</math> <math>22</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>459E-06</math>           3         115         <math>1478</math> <math>223</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>259E-06</math>           3         16         <math>1480</math> <math>23.5</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>276E-03</math>           3         16         <math>1480</math> <math>23.5299999</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>276E-03</math>           3         19         <math>1481</math> <math>23.299999</math> <math>1.38E-03</math> <math>14.06</math> <math>1.06E-04</math> <math>0.27</math> <math>276E-03</math>           3         20         <math>1481</math> <math>23.2299999</math> <math>257E-03</math> <math>26.18</math> <math>0.27</math> <math>0.27</math> <math>0.27</math>           3         20         <math>1488</math> <math>22.16003</math> <math>14.06</math> <math>1.06E</math></td><td>23 <math>12</math> <math>1332</math> <math>2.7</math> <math>2.57-0.3</math> <math>2.6.18</math> <math>1.00E-04</math> <math>0.21</math>           3         112         <math>1476</math> <math>21.4</math> <math>1.38E-04</math> <math>0.27</math> <math>4.59E-06</math>           3         113         <math>1477</math> <math>22</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>4.59E-06</math>           3         115         <math>1479</math> <math>223</math> <math>1.38E-03</math> <math>14.06</math>
<math>1.38E-04</math> <math>0.27</math> <math>2.666</math>           3         116         <math>1480</math> <math>23.5</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>2.666</math>           3         117         <math>1480</math> <math>23.5299999</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>2.666</math>           3         119         <math>1482</math> <math>25.2599999</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>2.666</math>           3         20         <math>14.88</math> <math>25.72-03</math> <math>26.18</math> <math>0.27</math> <math>0.27</math> <math>2.7</math>           3         20         <math>14.86</math> <math>25.7299999</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math></td><td><math>z^3</math>         1/2         1332         <math>z^1</math> <math>z^{50.16}</math> <math>z^{10.6}</math> <math>1.09E-04</math> <math>0.271</math> <math>459E-06</math>           3         12         1477         22         1.38E-03         14.06         2.16         1.38E-04         0.27         459E-06           3         15         1478         22         1.38E-03         14.06         1.38E-04         0.27         459E-06           3         16         1480         23.5         1.38E-03         14.06         1.38E-04         0.27         7           3         16         1480         23.5         1.38E-03         14.06         1.38E-04         0.27         7           3         18         1481         23.299899         1.38E-03         14.06         1.38E-04         0.27         7           3         19         1482         25.299899         1.38E-03         14.06         1.38E-04         0.27         7           3         20         1481         23.299899         1.38E-03         14.06         1.38E-04         0.27         7           3         20         1482         25.2998999         1.38E-03         14.06         1.09E-04         0.21         7</td><td><math>z_{2}</math> <math>1/2</math> <math>1322</math> <math>z576-03</math> <math>z6.18</math> <math>1.096-04</math> <math>0.271</math> <math>4596-06</math>           3         14         <math>1477</math> <math>21.4</math> <math>1.386-03</math> <math>14.06</math> <math>1.386-04</math> <math>0.271</math> <math>4596-06</math>           3         15         <math>1477</math> <math>22</math> <math>1.386-03</math> <math>14.06</math> <math>1.386-04</math> <math>0.277</math> <math>4596-06</math>           3         16         <math>1479</math> <math>21.5</math> <math>1.386-03</math> <math>14.06</math> <math>1.386-04</math> <math>0.277</math>           3         16         <math>14470</math> <math>23.5</math> <math>1.386-03</math> <math>14.06</math> <math>1.386-04</math> <math>0.277</math>           3         16         <math>1480</math> <math>23.5</math> <math>1.386-03</math> <math>1.406</math> <math>1.386-04</math> <math>0.277</math>           3         19         <math>1481</math> <math>2.32299999</math> <math>1.386-03</math> <math>1.406</math> <math>1.386-04</math> <math>0.27</math>           3         20         <math>1481</math> <math>2.22299999</math> <math>1.386-03</math> <math>1.406</math> <math>1.386-04</math> <math>0.27</math>           3         24         <math>1481</math> <math>2.2700001</math> <math>1.386-03</math> <math>1.406</math> <math>1.386-04</math> <math>0.27</math>           3         24         &lt;</td><td><math>z^3</math>         1/2         1332         <math>z^2</math> <math>z^{25}</math>/re<sup>-103</sup> <math>z^{26}</math>/re<sup>10</sup> <math>1.09e-04</math> <math>0.27</math> <math>4.59e-06</math>           3         13         147         23         1.38e-03         14.06         1.38e-04         <math>0.27</math> <math>4.59e-06</math>           3         15         1477         23         1.38e-03         14.06         1.38e-04         <math>0.27</math> <math>4.59e-06</math>           3         16         1480         23.55         1.38e-03         14.06         1.38e-04         <math>0.27</math> <math>4.59e-06</math>           3         17         1481         23.299999         1.38e-03         14.06         1.38e-04         <math>0.27</math> <math>4.59e-06</math>           3         18         1481         23.299999         1.38e-03         14.06         1.38e-04         <math>0.27</math>           3         19         1481         23.299999         1.38e-03         14.06         1.38e-04         <math>0.27</math>           3         20         1481         23.299999         1.38e-03         14.06         1.38e-04         <math>0.27</math>           3         20         1481         22.299999         1.38e-03         14.06         1.38e-04         <math>0.27</math>           3         24<td><math>z_3</math>         12         1332         <math>z_1</math> <math>z_5</math> 16         <math>z_6</math> 16         <math>z_7</math> 158         <math>z_6</math> 16         <math>z_7</math> 158         <math>z_6</math> 16         <math>z_7</math> 16         <math>z_7</math> 145         <math>z_7</math> 145         <math>z_7</math> 140         <math>z_7</math> 140</td><td><math>2^{20}</math>         132         27         2.57E-03         2.6.18         1.09E-04         0.27         4.56E-06           3         13         147         221         38E-03         14.06         2.16         138E-04         0.27         4.56E-06           3         14         1478         221         1.38E-03         14.06         1.38E-04         0.27         4.56E-06           3         16         1479         231         1.38E-03         14.06         1.38E-04         0.27         1.56E-04         0.21         1.56E-04         0.21         1.56E-04         0.27         1.56E-04         0.21         1.56E-04         0.27         1.56E-04         0.21         1.56E-04         0.21         1.56E-04         0.21         1.56E-04</td><td>23 <math>12</math> <math>1332</math> <math>2.5</math> <math>2.5</math> <math>2.5</math> <math>1.00E-04</math> <math>0.271</math> <math>1.00E-04</math> <math>0.271</math> <math>1.56E-06</math> <math>0.271</math> <math>0</math></td><td><math>z_0</math>         12         1332         27.14         2.51-6         2.61-10         1.08E-04         0.271         4.56E-06         &lt;</td><td><math>z_{2}</math> <math>12</math> <math>1332</math> <math>2.57</math> <math>2.576-03</math> <math>2.613</math> <math>1.096-04</math> <math>0.271</math> <math>1.096-04</math> <math>0.271</math>           3         13         1477         22         1.366-03         14.06         1         1.386-04         <math>0.271</math>           3         14         1.386-03         14.06         1         1.386-04         <math>0.271</math> <math>0.271</math>           3         16         1.477         22.3         1.386-03         14.06         1         <math>0.271</math> <math>0.271</math>           3         16         1.480         23.5         1.386-03         14.06         1         <math>0.271</math> <math>0.271</math>           3         16         1.481         25.208099         1.386-03         <math>14.06</math>         1         <math>0.271</math> <math>0.271</math>           3         19         1.482         25.208099         <math>1.386-03</math> <math>14.06</math>         1         <math>0.271</math> <math>0.271</math>           3         20         1.482         25.208099         <math>1.386-03</math> <math>14.06</math> <math>0.271</math> <math>0.271</math>           3         20         1.483         26.200001         <math>2.576-03</math> <math>2.614</math> <math>0.271</math> <math>0.271</math>           3</td><td><math>z_{col}</math>         12         1332         <math>z_{col}</math> <math>z_{col}</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td>2 <math>12</math> <math>1332</math> <math>22</math> <math>250E-03</math> <math>2618</math> <math>1.08E-04</math> <math>0.27</math> <math>456E-06</math> <math>0.27</math></td><td>-2         12         132         2.1         2.51-6.0         2.61 8         1.08E-04         0.27         4.58E-06           3         13         12         1476         2.14         1.35E-04         0.27         4.58E-06         0.27           3         14         1477         22         1.38E-03         14.06         1         1.38E-04         0.27         4.59E-06           3         16         1440         2.31         1.38E-03         14.06         1         1.38E-04         0.27         4.59E-06           3         17         1.481         2.32.936990         1.38E-03         14.06         1         1.38E-04         0.27           3         2.0         1.443         2.5299990         1.38E-03         14.06         1         1.38E-04         0.27           3         2.0         1.443         2.2700001         1.38E-03         14.06         0.27         0.27           3         2.24         1.463         2.2700001         1.38E-03         14.06         0.27         4.56E-06           8         2.3         160         2.7250001         1.38E-03         14.06         1.38E-04         0.27           9         1</td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math>z_{2}</math> <math>12</math> <math>1322</math> <math>22</math> <math>1382</math>-10         <math>161</math> <math>1382</math>-40         <math>0.27</math> <math>4562</math>-40         <math>0.27</math></td><td>3 <math>12</math> <math>1477</math> <math>22</math> <math>1.286-04</math> <math>0.27</math> <math>1.386-04</math> <math>0.27</math> <math>1.386-04</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c
c c c c c c c c</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td>22 <math>12</math> <math>1132</math> <math>22.5</math> <math>23.6</math> <math>31.6</math> <math>31.6</math><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{c c c c c c c c c c c c c c c c c c c </math></td><td><math display="block"> \begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td><td><math display="block"> \begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td><td>22 <math>21/2</math> <math>25/12</math> <math>25/12</math></td></td></td></td> | Zol         12         1332         Z/1         Z/2         Z/2 <thz 2<="" th=""> <thz 2<="" th=""> <thz 2<="" th=""></thz></thz></thz> | 23 $12$ $1332$ $27$ $2.57E-03$ $2.6.18$ $1.00E-04$ $0.21$ 3         112 $1476$ $21.4$ $1.38E-04$ $0.27$ $459E-06$ 3         113 $1477$ $22$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $459E-06$ 3         15 $1478$ $223$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $259E-06$ 3         16 $14.06$ $21.4.06$ $1.38E-04$ $0.27$ $27$ $38$ $14.06$ $1.38E-04$ $0.27$ $259E-06$ 3         16 $1480$ $23.5$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $27$ $28$ 3         17 $1481$ $23.299999$ $138E-03$ $14.06$ $1.38E-04$ $0.27$ $27$ 3         18 $14.06$ $1.38E-04$ $0.27$ $28$ $26.18$ $1.06E-04$ $0.27$ $28$ $28$ $28$ $28$ <td>23 <math>12</math> <math>1332</math> <math>2.7</math> <math>2.57E-03</math> <math>2.6.18</math> <math>1.00E-04</math> <math>0.21</math>           3         112         <math>1476</math> <math>21.4</math> <math>1.38E-04</math> <math>0.27</math> <math>459E-06</math>           3         113         <math>1477</math> <math>22</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>459E-06</math>           3         15         <math>1478</math> <math>223</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>259E-06</math>           3         16         <math>1479</math> <math>223</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>276E-06</math>           3         17         <math>1480</math> <math>23.5</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>276E-03</math>           3         18         <math>1481</math> <math>23.299999</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>276E-03</math>           3         19         <math>1481</math> <math>23.57E-03</math> <math>26.18</math> <math>0.27</math> <math>0.21</math> <math>0.27</math> <math>0.27</math> <math>0.27</math> <math>0.21</math>           3         20         <math>1488</math> <math>257E-03</math></td> <td>23 <math>12</math> <math>1332</math> <math>2.7</math> <math>2.57E-03</math> <math>2.6.18</math> <math>1.00E-04</math> <math>0.21</math>           3         112         <math>1476</math> <math>21.4</math> <math>1.38E-04</math> <math>0.27</math> <math>459E-06</math>           3         113         <math>1477</math> <math>22</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>459E-06</math>           3         115         <math>1478</math> <math>223</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>259E-06</math>           3         16         <math>1480</math> <math>23.5</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>276E-03</math>           3         16         <math>1480</math> <math>23.5299999</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>276E-03</math>           3         19         <math>1481</math> <math>23.299999</math> <math>1.38E-03</math> <math>14.06</math> <math>1.06E-04</math> <math>0.27</math> <math>276E-03</math>           3         20         <math>1481</math> <math>23.2299999</math> <math>257E-03</math> <math>26.18</math> <math>0.27</math> <math>0.27</math> <math>0.27</math>           3         20         <math>1488</math> <math>22.16003</math> <math>14.06</math> <math>1.06E</math></td> <td>23 <math>12</math> <math>1332</math> <math>2.7</math> <math>2.57-0.3</math> <math>2.6.18</math> <math>1.00E-04</math> <math>0.21</math>           3         112         <math>1476</math> <math>21.4</math> <math>1.38E-04</math> <math>0.27</math> <math>4.59E-06</math>           3         113         <math>1477</math> <math>22</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>4.59E-06</math>           3         115         <math>1479</math> <math>223</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>2.666</math>           3         116         <math>1480</math> <math>23.5</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>2.666</math>           3         117         <math>1480</math> <math>23.5299999</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>2.666</math>           3         119         <math>1482</math> <math>25.2599999</math> <math>1.38E-03</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math> <math>2.666</math>           3         20         <math>14.88</math> <math>25.72-03</math> <math>26.18</math> <math>0.27</math> <math>0.27</math> <math>2.7</math>           3         20         <math>14.86</math> <math>25.7299999</math> <math>14.06</math> <math>1.38E-04</math> <math>0.27</math></td> <td><math>z^3</math>         1/2         1332         <math>z^1</math> <math>z^{50.16}</math> <math>z^{10.6}</math> <math>1.09E-04</math> <math>0.271</math> <math>459E-06</math>           3         12         1477         22         1.38E-03         14.06         2.16         1.38E-04         0.27         459E-06           3         15         1478         22         1.38E-03         14.06         1.38E-04         0.27         459E-06           3         16         1480         23.5         1.38E-03         14.06         1.38E-04         0.27         7           3         16         1480         23.5         1.38E-03         14.06         1.38E-04         0.27         7           3         18         1481         23.299899         1.38E-03         14.06         1.38E-04         0.27         7           3         19         1482         25.299899         1.38E-03         14.06         1.38E-04         0.27         7           3         20         1481         23.299899         1.38E-03         14.06         1.38E-04         0.27         7           3         20         1482         25.2998999         1.38E-03         14.06         1.09E-04         0.21         7</td> <td><math>z_{2}</math> <math>1/2</math> <math>1322</math> <math>z576-03</math> <math>z6.18</math> <math>1.096-04</math> <math>0.271</math> <math>4596-06</math>           3         14         <math>1477</math> <math>21.4</math> <math>1.386-03</math> <math>14.06</math> <math>1.386-04</math> <math>0.271</math> <math>4596-06</math>           3         15         <math>1477</math> <math>22</math> <math>1.386-03</math> <math>14.06</math> <math>1.386-04</math> <math>0.277</math> <math>4596-06</math>           3         16         <math>1479</math> <math>21.5</math> <math>1.386-03</math> <math>14.06</math> <math>1.386-04</math> <math>0.277</math>           3         16         <math>14470</math> <math>23.5</math> <math>1.386-03</math> <math>14.06</math> <math>1.386-04</math> <math>0.277</math>           3         16         <math>1480</math> <math>23.5</math> <math>1.386-03</math> <math>1.406</math> <math>1.386-04</math> <math>0.277</math>           3         19         <math>1481</math> <math>2.32299999</math> <math>1.386-03</math> <math>1.406</math> <math>1.386-04</math> <math>0.27</math>           3         20         <math>1481</math> <math>2.22299999</math> <math>1.386-03</math> <math>1.406</math> <math>1.386-04</math> <math>0.27</math>           3         24         <math>1481</math> <math>2.2700001</math> <math>1.386-03</math> <math>1.406</math> <math>1.386-04</math> <math>0.27</math>           3         24         &lt;</td> <td><math>z^3</math>         1/2         1332         <math>z^2</math> <math>z^{25}</math>/re<sup>-103</sup> <math>z^{26}</math>/re<sup>10</sup> <math>1.09e-04</math> <math>0.27</math> <math>4.59e-06</math>           3         13         147         23         1.38e-03         14.06         1.38e-04         <math>0.27</math> <math>4.59e-06</math>           3         15         1477         23         1.38e-03         14.06         1.38e-04         <math>0.27</math> <math>4.59e-06</math>           3         16         1480         23.55         1.38e-03         14.06         1.38e-04         <math>0.27</math> <math>4.59e-06</math>           3         17         1481         23.299999         1.38e-03         14.06         1.38e-04         <math>0.27</math> <math>4.59e-06</math>           3         18         1481         23.299999         1.38e-03         14.06         1.38e-04         <math>0.27</math>           3         19         1481         23.299999         1.38e-03         14.06         1.38e-04         <math>0.27</math>           3         20         1481         23.299999         1.38e-03         14.06         1.38e-04         <math>0.27</math>           3         20         1481         22.299999         1.38e-03         14.06         1.38e-04         <math>0.27</math>           3         24<td><math>z_3</math>         12         1332         <math>z_1</math> <math>z_5</math> 16         <math>z_6</math> 16         <math>z_7</math> 158        
<math>z_6</math> 16         <math>z_7</math> 158         <math>z_6</math> 16         <math>z_7</math> 16         <math>z_7</math> 145         <math>z_7</math> 145         <math>z_7</math> 140         <math>z_7</math> 140</td><td><math>2^{20}</math>         132         27         2.57E-03         2.6.18         1.09E-04         0.27         4.56E-06           3         13         147         221         38E-03         14.06         2.16         138E-04         0.27         4.56E-06           3         14         1478         221         1.38E-03         14.06         1.38E-04         0.27         4.56E-06           3         16         1479         231         1.38E-03         14.06         1.38E-04         0.27         1.56E-04         0.21         1.56E-04         0.21         1.56E-04         0.27         1.56E-04         0.21         1.56E-04         0.27         1.56E-04         0.21         1.56E-04         0.21         1.56E-04         0.21         1.56E-04</td><td>23 <math>12</math> <math>1332</math> <math>2.5</math> <math>2.5</math> <math>2.5</math> <math>1.00E-04</math> <math>0.271</math> <math>1.00E-04</math> <math>0.271</math> <math>1.56E-06</math> <math>0.271</math> <math>0</math></td><td><math>z_0</math>         12         1332         27.14         2.51-6         2.61-10         1.08E-04         0.271         4.56E-06         &lt;</td><td><math>z_{2}</math> <math>12</math> <math>1332</math> <math>2.57</math> <math>2.576-03</math> <math>2.613</math> <math>1.096-04</math> <math>0.271</math> <math>1.096-04</math> <math>0.271</math>           3         13         1477         22         1.366-03         14.06         1         1.386-04         <math>0.271</math>           3         14         1.386-03         14.06         1         1.386-04         <math>0.271</math> <math>0.271</math>           3         16         1.477         22.3         1.386-03         14.06         1         <math>0.271</math> <math>0.271</math>           3         16         1.480         23.5         1.386-03         14.06         1         <math>0.271</math> <math>0.271</math>           3         16         1.481         25.208099         1.386-03         <math>14.06</math>         1         <math>0.271</math> <math>0.271</math>           3         19         1.482         25.208099         <math>1.386-03</math> <math>14.06</math>         1         <math>0.271</math> <math>0.271</math>           3         20         1.482         25.208099         <math>1.386-03</math> <math>14.06</math> <math>0.271</math> <math>0.271</math>           3         20         1.483         26.200001         <math>2.576-03</math> <math>2.614</math> <math>0.271</math> <math>0.271</math>           3</td><td><math>z_{col}</math>         12         1332         <math>z_{col}</math> <math>z_{col}</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td>2 <math>12</math> <math>1332</math> <math>22</math> <math>250E-03</math> <math>2618</math> <math>1.08E-04</math> <math>0.27</math> <math>456E-06</math> <math>0.27</math></td><td>-2         12         132         2.1         2.51-6.0         2.61 8         1.08E-04         0.27         4.58E-06           3         13         12         1476         2.14         1.35E-04         0.27         4.58E-06         0.27           3         14         1477         22         1.38E-03         14.06         1         1.38E-04         0.27         4.59E-06           3         16         1440         2.31         1.38E-03         14.06         1         1.38E-04         0.27         4.59E-06           3         17         1.481         2.32.936990         1.38E-03         14.06         1         1.38E-04         0.27           3         2.0         1.443         2.5299990         1.38E-03         14.06         1         1.38E-04         0.27           3         2.0         1.443         2.2700001         1.38E-03         14.06         0.27         0.27           3         2.24         1.463         2.2700001         1.38E-03         14.06         0.27         4.56E-06           8         2.3         160         2.7250001         1.38E-03         14.06         1.38E-04         0.27           9         1</td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math>z_{2}</math> <math>12</math> <math>1322</math> <math>22</math> <math>1382</math>-10         <math>161</math> <math>1382</math>-40         <math>0.27</math> <math>4562</math>-40         <math>0.27</math></td><td>3 <math>12</math> <math>1477</math> <math>22</math> <math>1.286-04</math> <math>0.27</math> <math>1.386-04</math> <math>0.27</math> <math>1.386-04</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td>22 <math>12</math> <math>1132</math> <math>22.5</math> <math>23.6</math> <math>31.6</math> <math>31.6</math><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{c c c c c c c c c c c c c c c c c c c </math></td><td><math display="block"> \begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td><td><math display="block"> \begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td><td>22 <math>21/2</math> <math>25/12</math> <math>25/12</math></td></td></td> | 23 $12$ $1332$ $2.7$ $2.57E-03$ $2.6.18$ $1.00E-04$ $0.21$ 3         112 $1476$ $21.4$ $1.38E-04$ $0.27$ $459E-06$ 3         113 $1477$ $22$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $459E-06$ 3         15 $1478$ $223$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $259E-06$ 3         16 $1479$ $223$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $276E-06$ 3         17 $1480$ $23.5$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $276E-03$ 3         18 $1481$ $23.299999$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $276E-03$ 3         19 $1481$ $23.57E-03$ $26.18$ $0.27$ $0.21$ $0.27$ $0.27$ $0.27$ $0.21$ 3         20 $1488$ $257E-03$ | 23 $12$ $1332$ $2.7$ $2.57E-03$ $2.6.18$ $1.00E-04$ $0.21$ 3         112 $1476$ $21.4$ $1.38E-04$ $0.27$ $459E-06$ 3         113 $1477$ $22$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $459E-06$ 3         115 $1478$ $223$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $259E-06$ 3         16 $1480$ $23.5$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $276E-03$ 3         16 $1480$ $23.5299999$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $276E-03$ 3         19 $1481$ $23.299999$ $1.38E-03$ $14.06$ $1.06E-04$ $0.27$ $276E-03$ 3         20 $1481$ $23.2299999$ $257E-03$ $26.18$ $0.27$ $0.27$ $0.27$ 3         20 $1488$ $22.16003$ $14.06$ $1.06E$ | 23 $12$ $1332$ $2.7$ $2.57-0.3$ $2.6.18$ $1.00E-04$ $0.21$ 3         112 $1476$ $21.4$ $1.38E-04$ $0.27$ $4.59E-06$ 3         113 $1477$ $22$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $4.59E-06$ 3         115 $1479$ $223$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $2.666$ 3         116 $1480$ $23.5$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $2.666$ 3         117 $1480$ $23.5299999$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $2.666$ 3         119 $1482$ $25.2599999$ $1.38E-03$ $14.06$ $1.38E-04$ $0.27$ $2.666$ 3         20 $14.88$ $25.72-03$ $26.18$ $0.27$ $0.27$ $2.7$ 3         20 $14.86$ $25.7299999$ $14.06$ $1.38E-04$ $0.27$ | $z^3$ 1/2         1332 $z^1$ $z^{50.16}$ $z^{10.6}$ $1.09E-04$ $0.271$ $459E-06$ 3         12         1477         22         1.38E-03         14.06         2.16         1.38E-04         0.27         459E-06           3         15         1478         22         1.38E-03         14.06         1.38E-04         0.27         459E-06           3         16         1480         23.5         1.38E-03         14.06         1.38E-04         0.27         7           3         16         1480         23.5         1.38E-03         14.06         1.38E-04         0.27         7           3         18         1481         23.299899         1.38E-03         14.06         1.38E-04         0.27         7           3         19         1482         25.299899         1.38E-03         14.06         1.38E-04         0.27         7           3         20         1481         23.299899         1.38E-03         14.06         1.38E-04         0.27         7           3         20         1482         25.2998999         1.38E-03         14.06         1.09E-04         0.21         7 | $z_{2}$ $1/2$ $1322$ $z576-03$ $z6.18$ $1.096-04$ $0.271$ $4596-06$ 3         14 $1477$ $21.4$ $1.386-03$ $14.06$ $1.386-04$ $0.271$ $4596-06$ 3         15 $1477$ $22$ $1.386-03$ $14.06$ $1.386-04$ $0.277$ $4596-06$ 3         16 $1479$ $21.5$ $1.386-03$ $14.06$ $1.386-04$ $0.277$ 3         16 $14470$ $23.5$ $1.386-03$ $14.06$ $1.386-04$ $0.277$ 3         16 $1480$ $23.5$ $1.386-03$ $1.406$ $1.386-04$ $0.277$ 3         19 $1481$ $2.32299999$ $1.386-03$ $1.406$ $1.386-04$ $0.27$ 3         20 $1481$ $2.22299999$ $1.386-03$ $1.406$ $1.386-04$ $0.27$ 3         24 $1481$ $2.2700001$ $1.386-03$ $1.406$ $1.386-04$ $0.27$ 3         24         < | $z^3$ 1/2         1332 $z^2$ $z^{25}$ /re <sup>-103</sup> $z^{26}$ /re <sup>10</sup> $1.09e-04$ $0.27$ $4.59e-06$ 3         13         147         23         1.38e-03         14.06         1.38e-04 $0.27$ $4.59e-06$ 3         15         1477         23         1.38e-03         14.06         1.38e-04 $0.27$ $4.59e-06$ 3         16         1480         23.55         1.38e-03         14.06         1.38e-04 $0.27$ $4.59e-06$ 3         17         1481        
23.299999         1.38e-03         14.06         1.38e-04 $0.27$ $4.59e-06$ 3         18         1481         23.299999         1.38e-03         14.06         1.38e-04 $0.27$ 3         19         1481         23.299999         1.38e-03         14.06         1.38e-04 $0.27$ 3         20         1481         23.299999         1.38e-03         14.06         1.38e-04 $0.27$ 3         20         1481         22.299999         1.38e-03         14.06         1.38e-04 $0.27$ 3         24 <td><math>z_3</math>         12         1332         <math>z_1</math> <math>z_5</math> 16         <math>z_6</math> 16         <math>z_7</math> 158         <math>z_6</math> 16         <math>z_7</math> 158         <math>z_6</math> 16         <math>z_7</math> 16         <math>z_7</math> 145         <math>z_7</math> 145         <math>z_7</math> 140         <math>z_7</math> 140</td> <td><math>2^{20}</math>         132         27         2.57E-03         2.6.18         1.09E-04         0.27         4.56E-06           3         13         147         221         38E-03         14.06         2.16         138E-04         0.27         4.56E-06           3         14         1478         221         1.38E-03         14.06         1.38E-04         0.27         4.56E-06           3         16         1479         231         1.38E-03         14.06         1.38E-04         0.27         1.56E-04         0.21         1.56E-04         0.21         1.56E-04         0.27         1.56E-04         0.21         1.56E-04         0.27         1.56E-04         0.21         1.56E-04         0.21         1.56E-04         0.21         1.56E-04</td> <td>23 <math>12</math> <math>1332</math> <math>2.5</math> <math>2.5</math> <math>2.5</math> <math>1.00E-04</math> <math>0.271</math> <math>1.00E-04</math> <math>0.271</math> <math>1.56E-06</math> <math>0.271</math> <math>0</math></td> <td><math>z_0</math>         12         1332         27.14         2.51-6         2.61-10         1.08E-04         0.271         4.56E-06         &lt;</td> <td><math>z_{2}</math> <math>12</math> <math>1332</math> <math>2.57</math> <math>2.576-03</math> <math>2.613</math> <math>1.096-04</math> <math>0.271</math> <math>1.096-04</math> <math>0.271</math>           3         13         1477         22         1.366-03         14.06         1         1.386-04         <math>0.271</math>           3         14         1.386-03         14.06         1         1.386-04         <math>0.271</math> <math>0.271</math>           3         16         1.477         22.3         1.386-03         14.06         1         <math>0.271</math> <math>0.271</math>           3         16         1.480         23.5         1.386-03         14.06         1         <math>0.271</math> <math>0.271</math>           3         16         1.481         25.208099         1.386-03         <math>14.06</math>         1         <math>0.271</math> <math>0.271</math>           3         19         1.482         25.208099         <math>1.386-03</math> <math>14.06</math>         1         <math>0.271</math> <math>0.271</math>           3         20         1.482         25.208099         <math>1.386-03</math> <math>14.06</math> <math>0.271</math> <math>0.271</math>           3         20         1.483         26.200001         <math>2.576-03</math> <math>2.614</math> <math>0.271</math> <math>0.271</math>           3</td> <td><math>z_{col}</math>         12         1332         <math>z_{col}</math> <math>z_{col}</math></td> <td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td> <td>2 <math>12</math> <math>1332</math> <math>22</math> <math>250E-03</math> <math>2618</math> <math>1.08E-04</math> <math>0.27</math> <math>456E-06</math> <math>0.27</math></td> <td>-2         12         132         2.1         2.51-6.0         2.61 8         1.08E-04         0.27         4.58E-06           3         13         12         1476         2.14         1.35E-04         0.27         4.58E-06         0.27           3         14         1477         22         1.38E-03         14.06         1         1.38E-04         0.27         4.59E-06           3         16         1440         2.31         1.38E-03         14.06         1         1.38E-04         0.27         4.59E-06           3         17         1.481         2.32.936990         1.38E-03         14.06         1         1.38E-04         0.27           3         2.0         1.443         2.5299990         1.38E-03         14.06         1         1.38E-04         0.27           3         2.0         1.443         2.2700001         1.38E-03         14.06         0.27         0.27           3         2.24         1.463         2.2700001         1.38E-03         14.06         0.27         4.56E-06           8         2.3         160         2.7250001         1.38E-03         14.06         1.38E-04         0.27           9         1</td> <td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td> <td><math>z_{2}</math> <math>12</math> <math>1322</math> <math>22</math> <math>1382</math>-10         <math>161</math> <math>1382</math>-40         <math>0.27</math> <math>4562</math>-40         <math>0.27</math></td> <td>3 <math>12</math> <math>1477</math> <math>22</math> <math>1.286-04</math> <math>0.27</math> <math>1.386-04</math> <math>0.27</math> <math>1.386-04</math></td> <td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td> <td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td> <td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td> <td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td> <td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td> <td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td> <td>22 <math>12</math> <math>1132</math> <math>22.5</math> <math>23.6</math> <math>31.6</math> <math>31.6</math><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{c c c c c c c c c c c c c c c c c c c </math></td><td><math display="block"> \begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td><td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td><td><math display="block"> \begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td><td><math display="block"> \begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td><td>22 <math>21/2</math> <math>25/12</math> <math>25/12</math></td></td> | $z_3$ 12         1332 $z_1$ $z_5$ 16 $z_6$ 16 $z_7$ 158 $z_6$ 16 $z_7$ 158 $z_6$ 16 $z_7$ 16 $z_7$ 145 $z_7$ 145 $z_7$ 140 | $2^{20}$ 132         27         2.57E-03         2.6.18         1.09E-04         0.27         4.56E-06           3         13         147         221         38E-03         14.06         2.16         138E-04         0.27         4.56E-06           3         14         1478         221         1.38E-03         14.06         1.38E-04         0.27         4.56E-06           3         16         1479         231         1.38E-03         14.06         1.38E-04         0.27         1.56E-04         0.21         1.56E-04         0.21         1.56E-04         0.27         1.56E-04         0.21         1.56E-04         0.27         1.56E-04         0.21         1.56E-04         0.21         1.56E-04         0.21         1.56E-04 | 23 $12$ $1332$ $2.5$ $2.5$ $2.5$ $1.00E-04$ $0.271$ $1.00E-04$ $0.271$ $1.56E-06$ $0.271$ $0$ | $z_0$ 12         1332         27.14         2.51-6         2.61-10         1.08E-04         0.271         4.56E-06         < | $z_{2}$ $12$ $1332$ $2.57$ $2.576-03$ $2.613$ $1.096-04$ $0.271$ $1.096-04$ $0.271$ 3         13         1477         22         1.366-03         14.06         1         1.386-04 $0.271$ 3         14         1.386-03         14.06         1         1.386-04 $0.271$ $0.271$ 3         16         1.477         22.3         1.386-03         14.06         1 $0.271$ $0.271$ 3         16         1.480         23.5         1.386-03         14.06         1 $0.271$ $0.271$ 3         16         1.481         25.208099         1.386-03 $14.06$ 1 $0.271$ $0.271$ 3         19         1.482         25.208099 $1.386-03$ $14.06$ 1 $0.271$ $0.271$ 3         20         1.482         25.208099 $1.386-03$ $14.06$ $0.271$ $0.271$ 3         20         1.483         26.200001 $2.576-03$ $2.614$ $0.271$ $0.271$ 3 | $z_{col}$ 12         1332 $z_{col}$ | $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | 2 $12$ $1332$ $22$ $250E-03$ $2618$ $1.08E-04$ $0.27$ $456E-06$ $0.27$ | -2         12         132         2.1         2.51-6.0         2.61 8         1.08E-04         0.27         4.58E-06           3         13         12         1476         2.14         1.35E-04         0.27         4.58E-06         0.27           3         14         1477         22         1.38E-03         14.06         1         1.38E-04         0.27         4.59E-06           3         16         1440         2.31         1.38E-03         14.06         1         1.38E-04         0.27         4.59E-06           3         17         1.481         2.32.936990         1.38E-03         14.06         1         1.38E-04         0.27           3         2.0         1.443         2.5299990         1.38E-03         14.06         1         1.38E-04         0.27           3         2.0         1.443         2.2700001         1.38E-03         14.06         0.27         0.27           3        
2.24         1.463         2.2700001         1.38E-03         14.06         0.27         4.56E-06           8         2.3         160         2.7250001         1.38E-03         14.06         1.38E-04         0.27           9         1 | $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | $z_{2}$ $12$ $1322$ $22$ $1382$ -10 $161$ $1382$ -40 $0.27$ $4562$ -40 $0.27$ | 3 $12$ $1477$ $22$ $1.286-04$ $0.27$ $1.386-04$ | $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | 22 $12$ $1132$ $22.5$ $23.6$ $31.6$ <td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td> <td><math display="block"> \begin{array}{c c c c c c c c c c c c c c c c c c c </math></td> <td><math display="block"> \begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td> <td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td> <td><math display="block"> \begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td> <td><math display="block"> \begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td> <td>22 <math>21/2</math> <math>25/12</math> <math>25/12</math></td> | $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | $ \begin{array}{c c c c c c c c c c c c c c c c c c c $ | $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | 22 $21/2$ $25/12$ |

Stabilized soil, spike-corrected emission factors

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Table A.15 - Polygon 18 - CCHD Station pv

fraction
Area (acres)
1/1
1/0
182
<del>1</del> 8
460
473 20.700001
474
475
476
477 26.299999
478
479
480
481
482
483
495
949
950
951
952
957
958
959
965
971
972
973 22.799999
235 20.299999
236
237
238
239
240

P		16	12		n Total			0.24	0.24	0.24	0.28	0.24	0.24	0.24	0.24	0.24	0.24	0.28	0.24	0.24	0.24	0.28	0.24	0.24	0.45	0.45	0.28				0.28	0.24	0.28	0.24	0.24	0.24	0.24	0.28	0.24	0.24	 031
Stabilized		0.16	33.12	Spike	Enission						00.00							0.0				00.0					0.00				00.00		00.00					0.00			
Stabilized				Spike	Li Fractor	4.59E-06					4.59E-06							4.59E-06				4.59E-06					4.59E-06		4.59E-06	4.59E-06	4.59E-06		4.59E-06					4.59E-06			
Stabilized		0.16	33.12	Steady	Emission	00.0	0.0	0.00	0.0	0.0	0.00	0.00	00.00	0.00	0.00	0.0	0.00	0.00	0.00	0.00	0.00	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	0.00	0.0	0.00	0.0	0.00	
Stabilized				.	Appleted in	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.09E-04	1.09E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	
Stable		0.84	173.88	_	Emission	0.04					0.04							0.04				0.04					0.04		0.04	0.04	0.04		0.04					0.04			
Stable					Factor	2.12E-04					2.12E-04							2.12E-04				2.12E-04					2.12E-04		2.12E-04	2.12E-04	2.12E-04		2.12E-04					2.12E-04			
Stable		0.84	173.88	Steady	Emission	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.45	0.45	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	0.24	
Stable					(Factor)	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	2.57E-03	2.57E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	
		fraction	Area (acres)		anta (mah)	22.799999	21.20001	21.6	22.200001	20.299999	21	22.1	22.1	21.4	21.799999	20.9	20.700001	20.299999	21.700001	21.5	22.299999	20.700001	23.6	23.20001	29.6	26.20001	20	21.5	20.6	22	20.9	20.700001	21.6	20.1	21.299999	21.6	21.200001	24.799999	8	22.4	
	acres	-	_		Cim kair		493	494	495	496	696	970	971	972	973	974	975	1332	1333	1334	1335	2149	2150	2151	2152	2153	3501	3502	4676	6242	8030	8031	8065	8067	8072	8073	8074	8180	8181	8182	
	207 a	0.84	0.16		100 100 100 100 100 100 100 100 100 100	12	13	14	15	16	6	10	11	12	13	14	15	12	13	4	15	13	14	15	16	17	21	22	20	2	14	15	F	e	80	6	10	20	21	ิส	
1999	vacant land area	stable fraction	unstable fraction		E David		21	21	21	21	10															31					ŀ	-							7		
SA PM-10	9	Excel 5.0			A COMPANY		ł	1	-	-	2	2	2	2	2	2	2	2	2	7	2	e	e	3	3	3	5	9	7	6	12	12	12	12	12	12	12	12	12	12	

Table A.16 - Polygon 16 - CCHD Station sa

Stabilized soil, spike-corrected emission factors

Table A.17 - Polygon 3 - CCHD Station sl 1

Stabilized soil, spike-corrected emission factors

					<b>Fotal</b>	<ul> <li>tons</li> </ul>	1.79	1.55	1.55	1.79	1.79	2 A 7
Stabilized		0.16	210.4	Spike	Emission	- uou	0.00			0.00	0.00	
Stabilized				Spike	Factor	(ion/ac)	4.59E-06			4.59E-06	4.59E-06	
Stabilized Stabilized Stabilized Stabilized		0.16	210.4	Steady	Factor Emission	(tonactin) 106 (ondac)	0.03	0.03	0.03	0.03	0.03	
Stabilized				Steady	Factor	(tion/ac/hr)	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	
Stable		0.84	1104.6	Spike	Emission	ton	0.23			0.23	0.23	
Stable				Spike	Factor Emission Factor Emission	(toniac)	2.12E-04			2.12E-04	2.12E-04	
Stable		0.84	1104.6	Steady	Emission	- lon	1.52	1.52	1.52	1.52	1.52	
Stable				Steady	Factor	(ton/ac/hr)	1.38E-03	1.38E-03	1.38E-03	1.38E-03	1.38E-03	
		fraction	Area (acres)			wind (mph) (cer/ac/hr)	20.799999	23.700001	21.6	21.1	20.1	
	acres					Cum hour	2149	2152	2153	3677	8180	
	1315 acres	0.84	0.16			Hour	13	16	17	5	20	
1999	vacant land area	stable fraction	unstable fraction			St Day	31	31	31	3	7	
SL PM-10		Excel 5.0 s	_			Montha	e	e	9	9	12	

.

WJ PM-10	1999				Stable	Stable	Stable	Stable	Stabilized	Stabilized	Stabilized	Stabilized	
Polygon 13	vacant land area	1522.5	acres										
Excel 5.0	stable fraction	0.84		fraction		0.84		0.84		0.16		0.16	
	unstable fraction	0.16		Area (acres)		1278.9		1278.9		243.6		243.6	
					Steady	Steady	Spike	Spike	Steady	Steady	Spike	Spike	
					- Factor	516		i i	Factor	Emission	Factor	Emission	🐺 Total 🐳
Month	Dav 1	A Hour	Cum hour	wind (mph)	(((ioniacino))	ton	(ton/ac)	ton	(ton/ac/m)	ton and	(ton/ac)	ton a	tons
	1 21	1 12	492			1.76	2.12E-04	0.27	1.38E-04	0.03	1.09E-04	0.03	2.10
	2	9 16	952	20.799999	1.38E-03	1.76	2.12E-04	0.27	1.38E-04	0.03	1.09E-04	0.03	2.10
	2 21	14	1238	20.20001	1.38E-03	1.76	2.12E-04	0.27	1.38E-04	0.03	1.09E-04	0.03	2.10
	2	11	1331	20.9	1.38E-03	1.76	2.12E-04	0.27	1.38E-04	£0.03	1.09E-04	0.03	2.10
	2 25	5 12	1332	29.700001	2.57E-03	3.29			1.09E-04	0.03			3.31
		5 13	1333	25.799999		3.29			1.09E-04	0.03			3.31
	3 9	9 13	-	23.799999	1.38E-03	1.76	2.12E-04	0.27	1.38E-04	0.03	1.09E-04	0.03	2.10
	3	9 14	-	23.20001	1.38E-03	1.76			1.38E-04	0.03			1.80
	3	0 15	1887	20.700001	1.38E-03	1.76	2.12E-04	0.27	1.38E-04	0.03	1.09E-04	0.03	2.10
	3 31	10	2146	21.5	1.38E-03	1.76	2.12E-04	0.27	1.38E-04	0.03	1.09E-04	0.03	2.10
	3 31	14		21.5	1.38E-03	1.76			1.38E-04	0.03			1.80
	3 31	1 16		21.5	1.38E-03	1.76			1.38E-04	0.03			1.80
	3 31	17	2153	22	1.38E-03	1.76			1.38E-04	0.03			1.80
10	0 16	5 10	Ö	20.299999	1.38E-03	1.76	2.12E-04	0.27	1.38E-04	0.03	1.09E-04	0.03	2.10
12	3	1	8065	20.299999	1.38E-03	1.76	2.12E-04	0.27	1.38E-04	0.03	1.09E-04	0.03	2.10
12	2 7	7 20	8180	21.20001	1.38E-03	1.76	2.12E-04	0.27	1.38E-04	0.03	1.09E-04	0.03	2.10
12	2 7	7 21	8181	21.5	1.38E-03	1.76			1.38E-04	0.03			1.80
12	2 7		8182	22	1.38E-03	1.76			1.38E-04	0.03			1.80
12	8	3	8185	20	1.38E-03	1.76			1.38E-04	0.03			1.80
12	2 21	1 13	8509	20.9	1.38E-03	1.76	2.12E-04	0.27	1.38E-04	0.03	1.09E-04	0.03	2.10
												-	

42.27

Total

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# Stabilized soil, spike-corrected emission factors

Table A.18 - Polygon 13 - CCHD Station wj

Stabilized Stabilized		0.16	251.84	Spike Spike	Fáctor Emission Total	(ioniac) ton tons		4.59E-06 0.00 2.14	1.86	1.86	1.86	1.86	1.86	4.59E-06 0.00 2.14	1.86	1.86	1.86	4.59E-06 0.00 2.14						
Stabilized Stal		0.16	251.84	Steady S	Emission	ton 👘 (to	0.03	0.03 4.5	0.03 4.5	0.03 4.5	0.03 4.5	0.03 4.5	0.03 4.5	0.03	0.03	0.03	0.03	0.03	0.03 4.5	0.03	0.03	0.03	0.03 4.5	000
Stabilized				Steady	Factor	(torvacht)	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	1.38E-04	
Stable		0.84	1322.16	Spike	H	l ton	4 0.28	4 0.28	4 0.28	4 0.28	4 0.28	4 0.28	4 0.28						4 0.28				4 0.28	
Stable		4	9	Spike		(ton/ac)	2 2.12E-04	2 2.12E-04	2 2.12E-04	2 2.12E-04	2 2.12E-04	2 2.12E-04	2 2.12E-04	2	2	2	2	2	2 2.12E-04	2	2	2	2 2.12E-04	
Stable		0.84	1322.16	Steady	Q.H	- 16 Kr.	3 1.82		3 1.82		3 1.82	3 1.82	3 1.82	3 1.82	3 1.82	3 1.82	3 1.82	3 1.82	3 1.82	3 1.82	3 1.82		3 1.82	
Stable				Steady	Eactor	(ton/ac/tir)	4 1.38E-03	9 1.38E-03	9 1.38E-03			1 1.38E-03	Γ	1 1.38E-03		6 1.38E-03	9 1.38E-03	4 1.38E-03	9 1.38E-03		9 1.38E-03		6 1.38E-03	
		fraction	Area (acres)			(hdm) (mph)	20.4		21.299999	21.6	21	21	21.1	20.1		24.6		21.4	21.299999		20.799999		21.6	
	acres					Cum hour	481	611	626	1335	1622	1886	2125	2126	2150	2151	2152	2153	2269	2270	2273	2274	2351	
	1574	0.84	0.16			Hour	1	11	23	15	14	14	13	14	14	15	16	17	13	14	17	18	23	
1999	vacant land area	stable fraction	unstable fraction			Day 1	21	36	6	55	5	8	8	8	31	31	31	31	5	5	5	2	80	
WW PM-10	ſ					Month	1	1	7	7	0	(m	0	e	e	e	e e	e	4	4	4	4	4	

Table A.19 - Polygon 2 - CCHD Station ww

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			Intal Acres	Run date
1	123	18	655	29-Nov-99
2	123	19	681	29-Nov-99
3	123	20	655	29-Nov-99
4	123	21	657	29-Nov-99
5	123	22	188	29-Nov-99
6	123	23	1	29-Nov-99
7	123	26	82	29-Nov-99
8	123	27	572	29-Nov-99
9	123	28	476	29-Nov-99
10	123	29	413	29-Nov-99
11	123	30	620	29-Nov-99
12	123	31	438	29-Nov-99
13	123	32	435	29-Nov-99
14	123	33	575	29-Nov-99
15	123	33	459	29-Nov-99
16	123	35	296	29-Nov-99
17	123	6	315	29-Nov-99
18	124	7	645	29-Nov-99
10	124	13	626	29-Nov-99
20	124	13	627	29-Nov-99
20	124	14	639	29-Nov-99
21		15	633	29-Nov-99
22	124 124	10	646	29-Nov-99
			647	29-Nov-99
24	124	18 19	632	29-Nov-99
25	124		646	29-Nov-99
26	124		640	29-Nov-99
27	124	1		
28	124			
29	124			
30	124			
31	124			
32	124			
33	124			
34	124			
35	124			the second se
36	124			
37	124			
38	124		the second se	
39	124		A second s	
40	124			
41	124			
42	124			
43	125			
44	125			
45	125			
46	125			
47	125			
48	125			
49	125			and the second se
50	125	5 6	3 301	l 29-Nov-99

193		SCALOG	ToplyAcces	Rundate
51	125	9	516	29-Nov-99
52	125	10	598	29-Nov-99
53	125	11	518	29-Nov-99
54	125	12	527	29-Nov-99
55	125	13	504	29-Nov-99
56	125	14	341	29-Nov-99
57	125	15	259	29-Nov-99
58	125	16	237	29-Nov-99
59	125		505	29-Nov-99
60	125		623	29-Nov-99
61	125			29-Nov-99
62	125			
63	125			29-Nov-99
	125			
64				
65	125			
66	125			
67				
68	125			
69				
70				
71				and the second sec
72				
73				
74				
75				
76				and the second s
77				
78				
79			1 533	
80	) 120		2 52	and the second se
81	·		3 57:	
82	2 12			the second se
83	3 12		and the second s	
84	1 12		and the second se	
8	5 12	and the second sec	4 64	the second se
86	5 12			
8	7 12	6 2	3 52	
88	3 13	7	1 67	and the second se
8	9 13	7 1	2 52	
90	0 13	7 1	3 5	the second se
9	1 13	7 1	4 5	7 29-Nov-99
9			5 33	
9			.0 47	7 29-Nov-99
9			1 63	2 29-Nov-99
9			2 65	4 29-Nov-99
9			3 43	and the second sec
9			the second se	8 29-Nov-99
9				6 29-Nov-99
9			26 49	
10			7 65	the second s

		Science	Totel Actions	Rundale
101	137	28	629	29-Nov-99
102	137	29	638	29-Nov-99
103	137	33	684	29-Nov-99
104	137	34	682	29-Nov-99
105	137	35	590	29-Nov-99
106	137	36	162	29-Nov-99
107	138	1	100	29-Nov-99
108	138	2	175	29-Nov-99
100	138	3	141	29-Nov-99
110	138	4	187	29-Nov-99
111	138	5	506	29-Nov-99
112	138	6	405	29-Nov-99
113	138	7	260	29-Nov-99
114	138	8	184	29-Nov-99
115	138	9	147	29-Nov-99
	130	10	147	29-Nov-99
116 117		10	23	29-Nov-99
	138		71	29-Nov-99
118	138	12		29-Nov-99
119	138	13	116	
120	138		52	29-Nov-99
121	138		171	29-Nov-99
122	138		63	29-Nov-99
123			3	29-Nov-99
124	138		5	29-Nov-99
125		the second se	96	
126	138		46	
127	138		47	
128	138		87	29-Nov-99
129				
130	138		16	
131	138		· · · · · · · · · · · · · · · · · · ·	
132				
133				1
134				
135	138	1		and the second se
136				
137	138			
138	138	33	11	29-Nov-99
139	138	35	9	29-Nov-99
140	138	36	8	29-Nov-99
141	139			
142	139	2	287	
143		) 3	206	29-Nov-99
144	139	4	529	29-Nov-99
145	139	5	240	29-Nov-99
146			107	29-Nov-99
147			275	29-Nov-99
148			206	29-Nov-99
149				
150			397	29-Nov-99

a de la		Statester	Tolal Acres	Rundate
151	139	11	170	29-Nov-99
152	139	12	327	29-Nov-99
153	139	13	78	29-Nov-99
154	139	14	88	29-Nov-99
155	139	15	154	29-Nov-99
156	139	16	212	29-Nov-99
157	139	17	520	29-Nov-99
158	139	18	369	29-Nov-99
159	139	19	109	29-Nov-99
160	139	20	198	29-Nov-99
161	139	21	149	29-Nov-99
162	139	22	67	29-Nov-99
163	139	23	80	29-Nov-99
164	139	24	10	29-Nov-99
165	139	25	71	29-Nov-99
166	139	26	23	29-Nov-99
167	139	27	63	29-Nov-99
168	139	28	59	29-Nov-99
169	139		55	29-Nov-99
170	139		7	29-Nov-99
171	139		8	29-Nov-99
172	139	32	_	29-Nov-99
173	139		191	29-Nov-99
174	139		58	29-Nov-99
175	139		25	29-Nov-99
176	139		L	29-Nov-99
177	140			29-Nov-99
178	140			29-Nov-99
179	140		1	29-Nov-99
180	140			29-Nov-99
181	140		168	29-Nov-99
182	140			1
183	140			the second se
184	140		330	29-Nov-99
185				
186				
187				
188				
189				
190				
191				
192			the second se	
193				
194				
195				· · · · · · · · · · · · · · · · · · ·
196	4			
197				
198				
199				
200				
	1 1 1 1			

MENS		Section	NTO FINATO (CEN	Ringdate
201	140	32	22	29-Nov-99
202	140	33	44	29-Nov-99
203	140	34	178	29-Nov-99
204	140	35	49	29-Nov-99
205	160	26	563	29-Nov-99
206	160	27	652	29-Nov-99
207	160	31	631	29-Nov-99
208	160	32	626	29-Nov-99
209	160	33	607	29-Nov-99
210	160	34	226	29-Nov-99
211	160	35	3	29-Nov-99
212	161	2	258	29-Nov-99
213	161	3	135	29-Nov-99
214	161	4	29	29-Nov-99
215	161	5	44	29-Nov-99
216	161	6	6	29-Nov-99
217	161	7	67	29-Nov-99
218	161	8		29-Nov-99
219	161	9		29-Nov-99
220	161	10		29-Nov-99
221	161	11	28	29-Nov-99
222	161	14		29-Nov-99
223	161	15		29-Nov-99
224	161	16	the second se	29-Nov-99
225	161	17		29-Nov-99
226	161	18		29-Nov-99
227	161	19		29-Nov-99
228	161			29-Nov-99
229	161			29-Nov-99
223	161			
230	161			29-Nov-99
232	161			
232	161			
233	161			
234	161			1
235	161		1	1
230	161			
237	161			
230				
239	161			the second se
240	161			
242	161		the second se	
242				
243	162		330 I 37	
244			2 11	
245	162		3 5	
240			4 13	
			5 5	the second se
248			B 10	
249 250			7 11	the second se
250	10	د ا		201101-00

### Clark County Assessor Data Vacant parcels by Section 1/2 acre and greater

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252         162         9         76           253         162         10         34           254         162         11         15           255         162         12         16           256         162         13         74           257         162         14         8           258         162         15         86           259         162         16         83           260         162         17         68           261         162         18         2           262         162         19         97	29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99
253         162         10         34           254         162         11         15           255         162         12         16           256         162         13         74           257         162         14         8           258         162         15         86           259         162         16         83           260         162         17         68           261         162         18         2           262         162         19         97	29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99
254         162         11         15           255         162         12         16           256         162         13         74           257         162         14         8           258         162         15         86           259         162         16         83           260         162         17         68           261         162         18         2           262         162         19         97	29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99
255         162         12         16           256         162         13         74           257         162         14         8           258         162         15         86           259         162         16         83           260         162         17         68           261         162         18         2           262         162         19         97	29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99
255         162         12         16           256         162         13         74           257         162         14         8           258         162         15         86           259         162         16         83           260         162         17         68           261         162         18         2           262         162         19         97	29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99 29-Nov-99
257         162         14         8           258         162         15         86           259         162         16         83           260         162         17         68           261         162         18         2           262         162         19         97	29-Nov-99 29-Nov-99 29-Nov-99
257         162         14         8           258         162         15         86           259         162         16         83           260         162         17         68           261         162         18         2           262         162         19         97	29-Nov-99 29-Nov-99
258         162         15         86           259         162         16         83           260         162         17         68           261         162         18         2           262         162         19         97	29-Nov-99 29-Nov-99
260         162         17         68           261         162         18         2           262         162         19         97	29-Nov-99
260         162         17         68           261         162         18         2           262         162         19         97	
261         162         18         2           262         162         19         97	29-Nov-99
	29-Nov-99
285 163 6 52	29-Nov-99
	29-Nov-99

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301         163         22         16         29-Nov-99           302         163         23         8         29-Nov-99           303         163         24         97         29-Nov-99           304         163         25         206         29-Nov-99           305         163         26         131         29-Nov-99           306         163         27         174         29-Nov-99           307         163         28         257         29-Nov-99           308         163         29         561         29-Nov-99           310         163         31         650         29-Nov-99           311         163         32         624         29-Nov-99           312         163         35         527         29-Nov-99           314         163         35         527         29-Nov-99           315         163         36         426         29-Nov-99           317         164         2         543         29-Nov-99           316         164         1         425         29-Nov-99           320         164         14         700         29-Nov-99 </th <th></th> <th>26.018</th> <th>Section</th> <th></th> <th>STATISTICS IN</th>		26.018	Section		STATISTICS IN
302         163         23         8         29-Nov-99           303         163         24         97         29-Nov-99           304         163         25         206         29-Nov-99           305         163         26         131         29-Nov-99           306         163         27         174         29-Nov-99           307         163         28         257         29-Nov-99           308         163         29         561         29-Nov-99           309         163         30         617         29-Nov-99           310         163         31         650         29-Nov-99           311         163         34         528         29-Nov-99           312         163         35         527         29-Nov-99           314         163         35         527         29-Nov-99           315         163         36         426         29-Nov-99           315         163         36         426         29-Nov-99           316         164         1         425         29-Nov-99           320         164         14         700         29-Nov-99	301	163		Charles and the second second second second	KIRCOMMENDED AND DED ARCHER IN DED
303         163         24         97         29-Nov-99           304         163         25         206         29-Nov-99           305         163         26         131         29-Nov-99           306         163         27         174         29-Nov-99           307         163         28         257         29-Nov-99           308         163         29         561         29-Nov-99           310         163         30         617         29-Nov-99           311         163         32         624         29-Nov-99           312         163         33         556         29-Nov-99           313         163         34         528         29-Nov-99           314         163         35         527         29-Nov-99           315         163         36         426         29-Nov-99           317         164         2         543         29-Nov-99           318         164         1         425         29-Nov-99           320         164         12         211         29-Nov-99           321         164         13         615         29-Nov-9					
304         163         25         206         29-Nov-99           305         163         26         131         29-Nov-99           306         163         27         174         29-Nov-99           307         163         28         257         29-Nov-99           308         163         29         561         29-Nov-99           310         163         31         650         29-Nov-99           311         163         32         624         29-Nov-99           312         163         33         556         29-Nov-99           313         163         34         528         29-Nov-99           314         163         35         527         29-Nov-99           315         163         36         426         29-Nov-99           314         163         62         29-Nov-99           315         163         36         22         29-Nov-99           316         164         1         567         29-Nov-99           320         164         12         211         29-Nov-99           321         164         13         615         29-Nov-99					
305         163         26         131         29-Nov-99           306         163         27         174         29-Nov-99           307         163         28         257         29-Nov-99           308         163         29         561         29-Nov-99           309         163         30         617         29-Nov-99           310         163         31         650         29-Nov-99           311         163         32         624         29-Nov-99           312         163         33         556         29-Nov-99           313         163         34         528         29-Nov-99           314         163         35         527         29-Nov-99           315         163         36         426         29-Nov-99           316         164         1         567         29-Nov-99           317         164         2         543         29-Nov-99           318         164         3         62         29-Nov-99           320         164         14         700         29-Nov-99           321         164         23         620         29-Nov-99					
306         163         27         174         29-Nov-99           307         163         28         257         29-Nov-99           308         163         29         561         29-Nov-99           309         163         30         617         29-Nov-99           310         163         31         650         29-Nov-99           311         163         32         624         29-Nov-99           312         163         33         556         29-Nov-99           313         163         34         528         29-Nov-99           315         163         36         426         29-Nov-99           316         164         1         567         29-Nov-99           317         164         2         543         29-Nov-99           318         164         3         62         29-Nov-99           320         164         12         211         29-Nov-99           321         164         13         615         29-Nov-99           322         164         14         700         29-Nov-99           323         164         26         637         29-Nov-99					
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318         164         3         62         29-Nov-99           319         164         11         425         29-Nov-99           320         164         12         211         29-Nov-99           321         164         13         615         29-Nov-99           322         164         14         700         29-Nov-99           323         164         23         620         29-Nov-99           324         164         24         561         29-Nov-99           325         164         25         647         29-Nov-99           326         164         26         637         29-Nov-99           327         164         36         654         29-Nov-99           328         175         1         318         29-Nov-99           330         176         2         615         29-Nov-99           331         176         3         618         29-Nov-99           332         176         4         645         29-Nov-99           333         176         7         679         29-Nov-99           334         176         6         650         29-Nov-99 <td></td> <td>1</td> <td>-</td> <td></td> <td></td>		1	-		
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338         176         10         609         29-Nov-99           339         176         11         497         29-Nov-99           340         176         12         611         29-Nov-99           341         176         13         523         29-Nov-99           342         176         14         568         29-Nov-99           343         176         15         541         29-Nov-99           344         176         16         501         29-Nov-99           345         176         17         563         29-Nov-99           346         176         18         643         29-Nov-99           347         176         19         585         29-Nov-99           348         176         20         585         29-Nov-99           349         176         21         573         29-Nov-99					
339         176         11         497         29-Nov-99           340         176         12         611         29-Nov-99           341         176         13         523         29-Nov-99           342         176         14         568         29-Nov-99           343         176         15         541         29-Nov-99           344         176         16         501         29-Nov-99           345         176         17         563         29-Nov-99           346         176         18         643         29-Nov-99           347         176         19         585         29-Nov-99           348         176         20         585         29-Nov-99           348         176         21         573         29-Nov-99					
340         176         12         611         29-Nov-99           341         176         13         523         29-Nov-99           342         176         14         568         29-Nov-99           343         176         15         541         29-Nov-99           344         176         16         501         29-Nov-99           345         176         17         563         29-Nov-99           346         176         18         643         29-Nov-99           347         176         19         585         29-Nov-99           348         176         20         585         29-Nov-99           349         176         21         573         29-Nov-99					the second se
341         176         13         523         29-Nov-99           342         176         14         568         29-Nov-99           343         176         15         541         29-Nov-99           344         176         16         501         29-Nov-99           345         176         17         563         29-Nov-99           346         176         18         643         29-Nov-99           347         176         19         585         29-Nov-99           348         176         20         585         29-Nov-99           349         176         21         573         29-Nov-99			1		
342         176         14         568         29-Nov-99           343         176         15         541         29-Nov-99           344         176         16         501         29-Nov-99           345         176         17         563         29-Nov-99           346         176         18         643         29-Nov-99           347         176         19         585         29-Nov-99           348         176         20         585         29-Nov-99           349         176         21         573         29-Nov-99		1			
343         176         15         541         29-Nov-99           344         176         16         501         29-Nov-99           345         176         17         563         29-Nov-99           346         176         18         643         29-Nov-99           347         176         19         585         29-Nov-99           348         176         20         585         29-Nov-99           349         176         21         573         29-Nov-99					
344         176         16         501         29-Nov-99           345         176         17         563         29-Nov-99           346         176         18         643         29-Nov-99           347         176         19         585         29-Nov-99           348         176         20         585         29-Nov-99           349         176         21         573         29-Nov-99					A
345         176         17         563         29-Nov-99           346         176         18         643         29-Nov-99           347         176         19         585         29-Nov-99           348         176         20         585         29-Nov-99           349         176         21         573         29-Nov-99					
346         176         18         643         29-Nov-99           347         176         19         585         29-Nov-99           348         176         20         585         29-Nov-99           349         176         21         573         29-Nov-99					29-Nov-99
347         176         19         585         29-Nov-99           348         176         20         585         29-Nov-99           349         176         21         573         29-Nov-99	346			643	29-Nov-99
348         176         20         585         29-Nov-99           349         176         21         573         29-Nov-99	347			585	29-Nov-99
349 176 21 573 29-Nov-99					29-Nov-99
350 176 22 244 29-Nov-99	349	<u> </u>			

	1 (1 (1 (1 ))) 1 (1 (1 (1 )))	Section.	<b>GRADADOS</b>	ARUn date
351	176	23	433	29-Nov-99
352	176	24	483	29-Nov-99
353	176	25	543	29-Nov-99
354	176	26	634	29-Nov-99
355	176	27	604	29-Nov-99
356	176	28	626	29-Nov-99
357	176	29	612	29-Nov-99
358	176	30	320	29-Nov-99
359	176	34	601	29-Nov-99
360	176	35	461	29-Nov-99
361	176	36	626	29-Nov-99
362	177	1	151	29-Nov-99
363	177	2	169	29-Nov-99
364	177	3	88	29-Nov-99
365	177	4	315	29-Nov-99
366	177	5	330	29-Nov-99
367	177	6	360	29-Nov-99
368	177	7	456	29-Nov-99
369	177	8	366	29-Nov-99
370	177	9	205	29-Nov-99
371	177	10	163	29-Nov-99
372	177	10	103	29-Nov-99
373	177	12	111	29-Nov-99
374	177	13	29	29-Nov-99
375	177	13	373	29-Nov-99
376	177	14	87	29-Nov-99
377	177	10	273	29-Nov-99
378	177	10	316	29-Nov-99
379	177	18	549	29-Nov-99
380	177	10	6	29-Nov-99
381	177	20		29-Nov-99
382	177	20	276	29-Nov-99
383	177	21		29-Nov-99
384	177	23	190	29-Nov-99
385				
386				29-Nov-99
387				
388	177			
389			<u> </u>	
390	177			29-Nov-99
391			the second s	29-Nov-99
392			637	29-Nov-99
392				29-Nov-99
393		32		29-Nov-99
394				
395				
390				
397			107	and the second sec
390				
			Lawrence	
400	178	3	213	29-140V-99

(ID)	100	SCIENTERS	STATISTICS STATES	Sea Run Stalle St
401	178	4	172	29-Nov-99
402	178	5	50	29-Nov-99
403	178	6	84	29-Nov-99
404	178	7	5	29-Nov-99
405	178	8	12	29-Nov-99
406	178	9	64	29-Nov-99
407	178	10	100	29-Nov-99
408	178	11	446	29-Nov-99
409	178	12	486	29-Nov-99
410	178	13	305	29-Nov-99
411	178	14	284	29-Nov-99
412	178	15	339	29-Nov-99
413	178	16	290	29-Nov-99
414	178	17	19	29-Nov-99
415	178	18	18	29-Nov-99
416	178	19	145	29-Nov-99
417	178	20	103	29-Nov-99
418	178	21	223	29-Nov-99
419	178	22	502	29-Nov-99
420	178	23	253	29-Nov-99
421	178	24	313	29-Nov-99
422	178	25	572	29-Nov-99
423	178	26	633	29-Nov-99
424	178	27	623	29-Nov-99
425	178	28	471	29-Nov-99
426	178	29	107	29-Nov-99
427	178	30	351	29-Nov-99
428	178	31	318	29-Nov-99
429	178	32	605	29-Nov-99
430	178	33	636	29-Nov-99
431	179	4	319	29-Nov-99
432	179	5	520	29-Nov-99
433	179	6	631	29-Nov-99
434	179	7	460	29-Nov-99
435	179	8	121	29-Nov-99
436	179	9	334	29-Nov-99
437	179	16	531	29-Nov-99
438	179	17	121	29-Nov-99
439	179	18	100	29-Nov-99
440	179	19	49	29-Nov-99
441	179	20	126	29-Nov-99
442	179	21	199	29-Nov-99
443	179	27	73	29-Nov-99
444	179	28	310	29-Nov-99
445	179	29	65	29-Nov-99
446	179	30	92	29-Nov-99
447	179	31	493	29-Nov-99
448	179	32	516	29-Nov-99
449	179	33	309	29-Nov-99
450	179	34	402	29-Nov-99

entransa ana	uptant carle wh	Clear South and showing a	The support of the su	Run date
451	189	3	252	29-Nov-99
452	1 <del>9</del> 0	5	605	29-Nov-99
453	190	6	262	29-Nov-99
454	190	7	290	29-Nov-99
455	190	8	595	29-Nov-99
456	190	17	287	29-Nov-99
457	190	18	634	29-Nov-9
458	190	19	333	29-Nov-9
459	190	20	35	29-Nov-9
460	191	1	303	29-Nov-9
461	191	2	179	29-Nov-9
462	191	3	459	29-Nov-9
463	191	4	555	29-Nov-9
464	191	5	537	29-Nov-9
465	191	6	633	29-Nov-9
466	191	8	510	29-Nov-9
467	191	9	546	29-Nov-9
468	191	10	588	29-Nov-9
469	191	11	608	29-Nov-9
470	191	12	275	29-Nov-9
471	191	13	648	29-Nov-9
472	191	14	651	29-Nov-9
473	191	15	634	29-Nov-9
474	191	16	631	29-Nov-9
475	191	17	530	29-Nov-9
476	191	20	593	29-Nov-9
477	191	21	644	29-Nov-9
478	191	22	621	29-Nov-9
479	191	23	629	29-Nov-9
480	191	24	675	29-Nov-9
			148,575	

l area (acres	total vacant	vacant arca (acros)	SECTION	1300K	whic station number.	Reconcioned
		149	21	139	1	277
		67		139	1	296
R.L.		23	26	139	1	331
		63	27	139	1	309
		59	28	139	1	310
		191	33	139	1	349
		58	34	139	1	348
63		25	35	139	1	347
		0		140	2	247
		350	14	140	2	253
		284	15	140	2	256
		193	20	140	2	298
		110	21	140	2	279
		87	22	140	2	263
		29	23	140	- 2	261
		0	24	140	2	257
· · · · · · · · · · · · · · · · · · ·		0	25	140	2	299
· · ·		95	26	140	2	300
· · · · · · · · · · · · · · · · · · ·		179	20	140	2	301
		48		140	2	302
		81	20	140	2	303
		22	32	140	2	340
		44	32	140	2	337
		178	33	140	2	338
		49	34	140	2	339
			35	140	2	335
<u> </u>		0	· · · · · · · · · · · · · · · · · · ·	161	2	381
		258	1	161	2	383
			3	161	2	382
		135		161	2	384
		29	4			385
	······································	44	5	161	2	432
		68	8	161	2	
0.40		45	9	161	2	431
2,49		169	10	161	2	429
		16		138	3	283
		0		138	3	316
		8		138	3	353
		275		139	3	224
		206		139	3	227
		520		139	3	235
		369		139	3	236
		109	19	139	3	271
		198	20	139	3	270
		149	21	139	3	276
		59	28	139	3	311
	-	55	29	139	3	312
		7		139	3	313
		8	31	139	3	352

rea (acres)	total vacant area	vacant area (acres).	SECTION	<b>:0</b> 0:0	wind station number.	Report Home
		22	32	139	3	351
		191	33	139	3	350
		58	34	139	3	356
		5	3	162	3	394
		13	4	162	3	395
······		5	5	162	3	396
		10	6	162	3	397
• <u>•</u> •••		11	7	162	3	443
		8	8	162	3	440
		76	9	162	3	441
		34	10	162	3	442
·····	l	33	1	163	3	398
2,510		65	12	163	3	444
		0	1	123	4	5
		0	2	123	4	
	······································	0	3	123	4	2
	······································	0	4	123	4	3
		0	5	123	4	3
		0	6	123	4	<del></del>
_	<u></u>	0		123		
<u> </u>	·····	0			4	32
<u></u>	2	0		123	4	29
	Construction of the second	0	and the second s	123	4	27
		0		123	. 4	28
	<u>}</u>			123	4	31
	<u>}</u>			123	4	30
	<u></u>	0		123	4	56
<u></u>		C		123	4	55
		C				53
		0			4	52
		0				54
	<u></u>	655			4	57
#******		681				83
						78
<u> </u>						79
		and the second				82
						80
	<u></u>		and the second sec	1	the second se	81
				1		108
						109
	a de la companya de l				4	107
	and the second se				4	106
	and the second s			1	4	110
<u></u>	and the second se			123	4	111
	<u></u>		3 31	123	4	138
	1		3 32	123		137
	5					134
	)					135
						136

Releana Gran	wind station number.	BOOK	SECTOR	vacant area (acres)	tolal vacant area (acres
133	4	123	36	0	
8	4	124	1	0	
9	4	124	2	0	
10	4	124	3	0	
12	4	124	4	0	
11	4	124	5	0	;
13	4	124	6	315	
38	4	124	7	645	
37	4	124	8	0	
36	4	124	9	0	g
34		124	10	0	
35	4	124	11	0	
33	4	124	12	0	
58	4	124	13	626	
59	4	124	14	627	1
61	4	124	15	639	[
60	4	124	16		
62	4	124		646	2,
65	4	124			
91	4	124			
88		124			<u></u>
86	4			647	<u></u>
87	4				
85	4				······································
84	4	124			<u> </u>
		124		· · · · · · · · · · · · · · · · · · ·	<u></u>
112	4				
113	4				
116	4				<u>, , , , , , , , , , , , , , , , , , , </u>
115	4				······································
114	4				
145	4				
143	4				A CONTRACTOR OF THE OWNER
144	4				
140	4				
139	4				
166	4				
167	4	1			
168	4				
169	4	-		Letter and the second s	
174	4				
198	4		and the second se		
197	4			and the second	
195	4				
229	4		the second se		
162	4		the second se	and the second sec	
161	4				
160	4				
163	4	140	) 4	119	)

l area (acres)	lofal vacant	(acant area (acres)	Sjaoss(ø). (	<b>ICCK</b>	Ainte satention nutring and	Record loff
		297	5	140	4	164
		219	6	140	4	165
		168	7	140	4	194
		223	8	140	4	193
		0	9	140	4	191
		315	10	140	4	192
		330	11	140	4	190
		0	12	140	4	189
		0	13	140	4	220
·		350	14	140	4	221
	,	284	15	140	4	223
		343	16	140	4	225
		322	17	140	4	226
		214	18	140	4	228
		193	20	140	4	260
		110	21	140	4	258
25,92		87	22	140	4	259
		446	11	178	5	714
		486	12	178	5	712
	*****	305	13	178	5	717
		284	14	178	5	718
		339	15	178	5	737
······································		502	22	178	5	755
		253	23	178	5	754
		313	24	178	5	753
	······································	572	25	178	5	786
		633	26	178	5	787
		623	27	178	5	788
		636	33	178	5	837
		0	34	178	5	822
		0	35	178	5	821
		0		178	5	820
		460	7	179	5	711
		121		179	5	708
		334		179	5	706
	·····	0	10	179	5	705
<u></u>		0		179	5	704
<u></u>		0		179	5	703
	)	0		179	5	707
	· · · · · · · · · · · · · · · · · · ·	0		179	5	709
		0		179	5	710
	<u>.</u>	531		179	5	713
		121	the second se	179	5	715
	·	100		179	5	716
	Construction of the local division of the lo	49		179	5	710
	2	126		179	5	751
	<u></u>	199		179	5	751
		0		179	5	730

Recipierren altere	wind schon utimidely	5(9)6)K	SEGION	Waterint area (agres)	total vacant area (acres).
748	5	179	23	0	
747	5	179	24	0	
780	5	179	25	0	
781	5	179	26	0	
782	5	179	27	73	
783	5	179	28	310	
784	5	179	29	65	1
785	5	179	30	92	<u></u>
819	5	179	31	493	ĵ
818	5	179	32	516	·····
817	5	179	33	309	,
816	5	179	34	402	
815	5	179	35		§
813	5	179	36		
849	5	189		0	
h			1		
850	5	189			<u>}</u>
851	5	189			
852	5	189	· · · · · · · · · · · · · · · · · · ·		<u> </u>
853	5	189			£
854	5	189			
874	5	189			han
873	5				
872	5				al a second and a se
871	5				a de la companya de la
870	5		1		
869	5				
889	5				and the second s
890	5	189			
891	5	189	15	And the second sec	
892	5	189	16	S C	
894	5	189	17	C C	)
895	5	189			
914	5	189	19		)
913	5	189	20		)
912	5	189	21		
911	5	189	22	2 (	)
910	5			3 (	
909	5				)
928	5				)
929	5				)
930	5				
931	5				And the second s
932	5				
933	5			and the second	
953	5			And the second s	)
952	5				
952	5				)
		108			)

Record id#	Wind station number.	BOOK	SECTION	vacant area (acres)	iteral vacantrarea (acres)
949		189	35		
948	5	189	36	0	
855	5	190	1	0	
856	5	190	2	0	
857	5	190	3	0	
858	5	190	4	0	
893	5	190	8	595	<u></u>
878	5	190	9		<u></u>
877	5	190	10	0	(
876	5	190	11	0	<u>.</u>
875		190	12	0	
896	5	190	13	0	
897	5	190	14	0	
898	5	190	15		Construction of the second
899	5	190	16	0	· · · · · · · · · · · · · · · · · · ·
900	5	190	10	287	/
921	5	190	20		
918		190	21	0	
917	5	190	21	0	
916		190	23		
915		190	23		
934		190	24		
934		190	25		
935	······································	190	20	0	
937	5	190	28		
938	5	190	29		in a second s
947	5	190	30	1	
959		190	31	0	
958		190	32		
957	5	190	33		
956		190	34		
955		190	· · · · · · · · · · · · · · · · · · ·		
954					
330					
365					
341				22	
386		161			
387					
434	1				· · · · · · · · · · · · · · · · · · ·
433					
485					Å
486				1	
526			19	1	
527	6	161			
564	6	161	29	51	
565	6	161	30	36	
425		162			
435				16	

area (acres)	total vacant a	vacant area (acres).	SECTION	Bolek	wind station number	Repaid C#
		74	13	162	6	487
		39	24	162	6	528
722		26	25	162	6	569
		50	36	139	7	370
		81	29	140	7	326
		60	30	140	7	334
		56	31	140	7	343
		22	32	140	7	342
		6	6	161	7	388
2		37	1	162	7	389
		11	2	162	7	411
33		16		162	7	436
		0	36	140	8	371
		0	1	160	8	373
		0	2	160	8	374
		0	3	160	8	375
	( <u></u>	0	4	160	8	376
~~	( <u> </u>	0	5	160	8	378
	in the second	0	6	160	8	379
		0	7	160	8	424
	/	0	8	160	8	423
		0	9	160	8	422
	<u></u>	0	10	160	8	421
		0	11	160	8	417
	· · · · · · · · · · · · · · · · · · ·	0	12	160	8	418
	l 1 1 1 1 1	0	15	160	8	473
		0	16	160	8	474
	· · · · · · · · · · · · · · · · · · ·	0	10	160	8	474
	<u></u>	0	18	160	8	478
	è	0	10	160	8	519
		0		160	8	518
		0	1	161	8	380
	(	258		161	8	404
		135	2	161	8	416
	Lange and the second	68		161	8	469
	2	45		161		409
	· · · · · · · · · · · · · · · · · · ·	45			8	
	<u></u>			161		428
		28	11	161	8	427
		0	12	161	8	426
	· · · · · · · · · · · · · · · · · · ·	0		161	8	479
	<u> </u>	321		161	8	480
	<u>.</u>	290	15	161	8	482
		108		161	8	483
	1 · · · · · · · · · · · · · · · · · · ·	34	17	161	8	484
		11		161	8	525
·	the second s	130		161	8	523
		4		161	8	522
		227	23	161	8	521

nt area (acres	total vacant	vacant area (actes)	SECHION	(e)e)k	lind station number.	
		0	24	161	8	520
		493	25	161	8	559
<u> </u>		440	26	161	8	560
· · · · · · · · · · · · · · · · · · ·		287	27	161	8	561
		141	28	161	8	562
		51	29	161	8	563
3,27		36	30	161	8	582
		11	7	162	9	466
		8	8	162	9	464
,		76	9	162	9	463
		34	10	162	9	462
		74	13	162	9	515
		8	14	162	9	496
		86	15	162	9	491
n		83	16	162	9	494
		68	10	162	9	493
		2	18	162	9	400
<u></u>		97	10	162	9	533
<u> </u>		63	20	162	9	531
		65	20	162	9	532
		76	21	162	9	534
		5	22	162	9	530
,,,,,,,		39				530
			24	162	9	
		26	25	162	9	572
-		47	26	162	9	566
		53	27	162	9	567
		386	28	162	9	570
		185	29	162	9	571
		133	30	162	9	573
		452	31	162	9	614
	Ś	298	32	162	9	615
		359	33	162	9	613
		465		162	9	612
<u> </u>		358	35	162	9	611
		125		162	9	608
		65		163	9	467
	<u></u>	39	and a second sec	163	9	495
		97	24	163	9	535
		169	2	177	9	647
		88	3	177	9	648
		315	4	177	9	649
		330	5	177	9	651
		360	6	177	9	650
		456	7	177	9	685
		366	8	177	9	686
		205	9	177	9	684
		163	10	177	9	682
	(	123	11	177	9	679

Record 10#	wind station number.	BIO(OK)	SECTOR	Materin Sanera (Sacres).	(olal vacantarea (acres)
727	9	177	15		
728	9	177	16	273	
730	. 9	177	17	316	
729	9	177	18	549	
765	9	177	19		
764	9	177	20	316	
763	9	177	21	276	
797	9	177	28	398	
796	9	177	29	509	
799	9	177	30	613	······································
833	9	177	31	637	<u></u>
832	9	177	32	542	
408	10	160	1	0	the second s
458	10	160	10	0	
420	10	160	11	0	<u> </u>
419	10	160	12	0	
471	10	160	13		in the second
470	10	160	13	0	
470	10	160	15		1
472	10	160	16		
510	10	160	10	0	
524	10	160	19		
516	10			0	) 
516		160	20		\$ <b></b>
	10	160	21	0	<u>}</u>
513	10	160	22	0	· · · · · · · · · · · · · · · · · · ·
511	10	160	23	0	(
512	10	160	24	0	2
552	10	160	25	0	<u>}</u>
551	10	160	26		
553	10	160	27	652	<u></u>
554	10	160		and the second se	<u> </u>
555	10	160	29		<u></u>
556		160		A REAL PROPERTY AND A REAL	
601	10	160			
599		160			
598		160			
597	10	160			
596		160		and the second	
595		160			
549		161			<u> </u>
558		161	and the second		
568		161			
593	And the second	161	£	and the second se	
603	10	161			
602	10	161	36		
637	10	178			
638	10	178		286	
674	10	178		446	the definition of the definiti

	Wind station numbers		STREEK!	wacant area (acres).	notel valeantrarea (aleres)
672	10	178	12	486	
631	10	179	1	0	
632	10	179	2	0	
633	10	179	3	0	
634	10	179	4	319	
635	10	179	5	520	
636	10	179	6	631	
673	10	179	7	460	
671	· 10	179	8	121	
670	10	179	9	334	
669	10	179	10	0	
668	10	179	11	0	
667	10	179	12	0	8,54
196	11	139	3	206	
187	11	139	4	529	<u> </u>
186	11	139	5	240	
219	11	139	7	275	
205	11	139	8	206	
202	11	139	9	199	<u>.</u>
199	11	139	10	397	
217	11	139	11	170	
222	11	139	12	327	
230	11	139	13	78	
231	11	139	10	88	)
232	11	139	15	154	1
233	11	139	16	212	janaan ar
234	11	139	10	520	
269	11	139	20	198	l
268	11	139	20	130	<u>}</u>
267	11	139	21	67	
266	11	139	23	80	
265	11	139	23	10	
307	11	139		71	* 
306	11	139		23	and the second
308		139		63	
255	11	140		322	
255	11				
		140		214	
264	11	140		123	
262	11	.140	20	193	
281	11	140		110	
304	11	140	29	81	
305	11	140	30	60	
550		162	19	97	<u> </u>
574	12	162	30	133	
616		162	31	452	
481	12	163	7	3	
475		163		15	
468	12	163	9	250	20 1

Record id#	wine station number.	ato(o), s	SECTION	vacani area (acres).	tolal vacant area (agres
465	12	163	10		
461	12	163	11	71	
460	12	163	12	65	·
497	12	163	13	39	
499	12	163	14	11	
498	12	163	15	135	
504	12	163	16		
502	12	163	17	125	
503	12	163	18		
541	12	163	19		3
540	12	163	20	296	
539	12	163	21	129	
538	12	163	22	120	
537	12	163	23	8	· · · · · · · · · · · · · · · · · · ·
536	12	163	23		
575	12	163	24	1	
576	12	163	25		
577					
	12	163	27	174	
579	12	163	28		
578	12	163	29		
580	12	163	30	617	è <del></del>
622	12	163	31	650	
620	12	163	32		
621	12	163	33		
619	12	163	34		
618	12	163	35	· · · · · · · · · · · · · · · · · · ·	
617	12	163	36		
517	12	164	13		) 
557	12	164	23		
542	12	164	24		
581	12	164	25	647	
585	12	164	26	637	
600	12	164			
630	12	164	33		
628	12	164	34	0	
627	12	164	35	0	
623	12	164	36	654	
661	12	175	1	318	
662	12	175	2		
665	12	175	3	0	
664	12	175	4		
666	12	175	5	0	
702	12	175			
698	12	175	8		
697	12	175	9		<u> </u>
696	12	175	10		
695	12	175	11		
694	12				

Record WH	wind station number	FORK	SEDTION	vacani area (acres).	1 (olfa) v soanti arrea (arere-
739	12	175	13	0	
740	12	175	14	0	
742	12	175	15	0	
741	12	175	16	0	
743	12	175	17	0	1
744	12	175	18	0	ç <del>anın</del>
778	12	175	10	0	<u> </u>
779	12	175	20	0	
776	12	175	21	0	· · · · · · · · · · · · · · · · · · ·
777	12	175	22	0	· · · · · · · · · · · · · · · · · · ·
774	12	175	23	0	
775	12	175	23	0	t
811	12	175	24	0	
810					· · · · · · · · · · · · · · · · · · ·
	12	175	26	0	
809	12	175	27	0	
808	12	175	28		
812	12	175	29	0	/
813	12	175	30	0	
847	12	175	31	0	
846	12	175	32	0	)
845	12	175	33		<u>}</u>
844	12	175	34		
842	12	175	35		· · · · · · · · · · · · · · · · · · ·
843	12	175	36	0	
653	12	176	1	587	
654	12	176	2	615	
655	12	176	3	618	
656	12	176	4	645	
657	12	176	5	641	
658	12	176	6	650	
693	12	176	7	679	
692		176		382	
691	12	1			
690					
689					a second se
688					
732	··· · · · ·				
733					
734					
735					á
736					And the second s
738					
730				and the second state of th	······
772					
771	12				
770					
769				and the second sec	
768	12	176	24	483	2 2

area (aeres	total vacant		Section	BOOK	wind station number	Recordin#
		543	25	176	12	801
		634	26	176	12	802
		604	27	176	12	803
		626	28	176	12	805
		612	29	176	12	806
		320	30	176	12	807
		0	31	176	12	841
		0	32	176	12	840
		0	33	176	12	839
		601	34	176	12	838
		461	35	176	12	836
		626	36	176	12	835
		360	6	177	12	652
		456	7	177	12	687
		549	18	177	12	731
		600	19	177	12	767
		613	30	177	12	800
		637	31	177	12	834
		633	6	191	12	868
34,56		0	7	191	12	888
		46	20	138	13	297
		47	21	138	13	294
		87	22	138	13	293
		42	23	138	13	292
		16	24	138	13	291
		0	25	138	13	314
		13	26	138	13	315
		92	27	138	13	317
		216	28	138	13	318
		175	29	138	13	319
		68		138	13	359
		169		138	13	363
		197		138	13	360
		11		138	13	358
		0		138	13	357
		9		138	13	355
		8		138	13	354
		33		163	13	399
		85	the second se	163	13	400
		115			13	400
		130			13	401
<u></u>	the second s	45			13	402
		52			13	403
		3			13	430
<u></u>		15			13	440
,		250			13	449
		230	<u></u>		13	451
		71			13	447

8 4 + (s) (s) (s) (s) 3	wind station number	ଅ(ଜୀତ) , ଜ	SECTION	vacant area (acres).	igial vacani area (acres)
445	13	163	12	65	2,177
592	14	161	27	287	
591	14	161	28	141	
590	14	161	29	51	
589	14	161	30	36	
607	14	161	31	190	
610	14	161	32	107	
605	14	161	33	116	
604	14	161	34	495	
609	14	161	35	208	
594	14	162		26	
645	14	162		358	
606	14	162	+	125	
642	14	177		151	
646		177		169	
699		177			
677	14	177		123	
680		177			
723		177			
726		177			
725					
746		177			
766		177			)
760		177			<u></u>
761		177			<u></u>
760					
700		+	**		<u></u>
790	· · · · · · · · · · · · · · · · · · ·				
795					
798					A
804					
848					
831					/
830					
829			1		
828				A CONTRACTOR OF A CONTRACTOR O	descent and the second s
827					Contraction of the second s
639					
640				200	
641				and the second s	
644				5 50	
643				and the second sec	
681			the second se	7 5	
				3 12	
683				64	and the second sec
678					
676					
675	5 14 9 14				

Record id#	wind station number	BOOK	SECTION	vacant area (acres)	tota vacant area (acres)
720	14	178	15		
721	14	178	16	290	<u>, , , , , , , , , , , , , , , , , , , </u>
724	14	178	17	19	
722	14	178	18	18	andan ang ang ang ang ang ang ang ang ang a
758	14	178	19	145	
759	14	178	20	103	
757	14	178	21	223	
756	14	178	22	502	
789	14	178		623	
790	14	178		471	
792	14	178			
791	14	178			
826	14	178			
825	14	178			
824	14	178	1	636	
823	14	178			
859	14	190			
860	14	190			
861	14	190	· · · · · · · · · · · · · · · · · · ·		
881	14	190			
880	14	190			······································
879	14	190			
901	14	190			
903	14	190			······································
920	14	190			
922	14	190			
939	14	190			<u></u>
940	14	190			
960				-	in a second s
862					
863	14				
864					
865					
866	· · · · · · · · · · · · · · · · · · ·				in the second
867					Contraction of the second s
887	And the second				
886	the second se				
884					
885				and the second sec	i i i i i i i i i i i i i i i i i i i
883					
882			and the second sec		
902					
902					
904					
905					Sector and the sector of the s
903					
907	the second se				2
908					

t area (acres)	lolal vacani	acant area (acres)	SECTION	ook:	wine station number	Reconcident
		593	20	191	14	926
		644	21	191	14	924
		621	22	191	14	925
		629	23	191	14	923
		675	24	191	14	919
		0	25	191	14	943
		0	26	191	14	942
		0	27	191	14	941
		0	28	191	14	944
		0	29	191	14	946
		0	30	191	14	945
		0	31	191	14	966
		0	32	191	14	965
		0	33	191	14	963
	,	0	34	191	14	964
		0	35	191	14	962
30,558		0	36	191	14	961
		58	34	139	15	377
		25	35	139	15	372
<u></u>		37	1	162	15	413
		11	2	162	15	392
		5	3	162	15	393
		34	10	162	15	439
		15	11	162	15	438
		16	12	162	15	437
		74	13	162	15	488
		8	14	162	15	489
369		86	15	162	15	490
		71	25	139	16	333
	<u> </u>	23	26	139	16	336
<u></u>		25	35	139	16	345
<u> </u>		50	36	139	16	346
<u></u>		81	29	140	16	328
	<u> </u>	60	30	140	16	332
<u> </u>		56		140	16	344
		37	1	162	16	390
41	· · · · · · · · · · · · · · · · · · ·			162	10	390
		315		124	10	14
	the second se	645		124	17	39
		647		124	17	64
·····		632		124	17	90
		646				
·····		471		124	17 17	104
		608		124		121
				124	17	120
		288		124	17	149
		239	and the second sec	124	17	148
		286 613		<u>125</u> 125	<u> </u>	15 16

Record	wind station number:	Eleek	(SECTON	vacaal area (acres) horal vacant area	(acres)
17	17	125	3	596	
18	17	125	4	308	
19	17	125	5	496	
20	17	125	6	603	
45	17	125	7	610	
44	17	125	8	301	
43	17	125	9		•••••
41	17	125	10	598	
42	17	125	11	518	
40	17	125	12	527	
63	17	125	13	504	
70	17	125		341	
71	17	125		259	
67	17	125		237	
66	17	125			
68	17	125		· · · · · · · · · · · · · · · · · · ·	
94	17	125	· · · ·		<u>,</u>
92	17	125			
93	17	125			
97	17	125			<u> </u>
96	17	125			
89	17	125			
119	17	125			
125	17	125			
118	17	125			
117	17	125			<u></u>
122	17	125			
123	17	125			
151	17	125			
147	17	125			
146	17	125			
141	17				
142					
150					
21					
21				A second se	
23		(			
24	the second secon				
25					
26					
51	1				
50	+				
49					
47	the second s				
47				فيجب المرابقة المتحدين والمرابقة المتحدين والمتحد والمحدود	<u> </u>
46		1			<u>,</u>
69				and the second	
72					

Record lot	wind station number	CololX.	SIZONION	vacant'area (acres) total vacant area (acre
74	17	126	15	0
73	17	126	16	0
75	17	126	17	0
76	17	126	18	0
102	17	126	19	0
101	17	126	20	0
99	17	126	21	0
100	17	126	22	0
98	17	126	23	0
95	17	126	24	649
124	17	126	25	564
126	17	126	26	0
127	17	126	27	0
128	17	126	28	0
129	17	126	29	0
155	17	126	33	0
154	17	126	34	0
153	17	126	35	0
152	17	126	36	529
179	17	137	1	673
180	17	137	2	0
181	17	137	3	0
213	17	137	11	0
210	17	137	12	529
244	17	137	12	51
178		137	13	100
170	17	138	2	
171	17	138	3	141
170	17	138	4	141
173	17	138		· · · · · · · · · · · · · · · · · · ·
172	17	138		405
Contractor and the second s			6	260
207	17	138		
200		138	8	
201		138		
203		138		
204		138		
209		138		
242		138	13	
238		138	14	
237		138	15	
241		138	16	
240		138	17	3
243		138	18	
282		138	19	
280		138		
278		138		47
272		138		
273	17	138	23	42

Record off	wind station number	BOOK	SECTION	vacantiarea (acres)	total vacant area (acres)
274	17	138			
175	17	139	5	240	
176	17	139	6	107	
208	17	139	7	275	
206	17	139	8	206	
239	17	139	18		· · · · · · · · · · · · · · · · · · ·
275	17	139	19	109	<u> </u>
77	18	126	18	0	
103	18			0	<u></u>
105	18	126			
132	18	126		0	
130	18	126	1		
131	18	126		0	\$
158	18	126		0	· · · · · · · · · · · · · · · · · · ·
157	18	126			
156	18	126			
159	18	126			
188	18	120	2		
182	18				
183	18	137	4		
184	18				S
185	18	137		······································	
214	18	1	7		
214	18		8		<u>}</u>
215		137		1	· · · · · · · · · · · · · · · · · · ·
210	18	137			<u></u>
211	18	137		0	the second s
212		+			
210	- · · · · · · · · · · · · · · · · · · ·				
246					<u></u>
248					
249					
251	18				
250					ly
290					5
289					
288					
287					And the second se
286					
285					
320					
323					
324					
325					
327				and the second sec	A CONTRACT OF A
329				and the second	
369					<u>}</u>
368	18	137	32	0	

Record id#	wind station number	BOOK	SECRICIN	vacant area (acres)	tolal vacant area (acres
367	18	137	33	684	
366	18	137	34	682	
364	18	137	35	590	
361	18	137	36	162	
254	18	138	18	5	
284	18	138	19	96	
295	18	138	20	46	
322	18	138	29	175	
321	18	138	30	68	
362	18	138	31	169	
405	18	163	5	45	
405	18	163	6	52	
450	18	163	7	32	
505	18	163	18	192	
407					
	18	164	1	567	
409	18	164	2	543	
410	18	164	3	62	
412	18	164	4	0	
414	18	164	5	0	
415	18	164	6	0	· · · · · · · · · · · · · · · · · · ·
459	18	164	7	0	
457	18	164	8	0	
456	18	164	9	0	
455	18	164	10	0	······································
454	18	164	11	425	·
453	18	164	12	211	
506	18	164	13	615	
501	18	164	14	700	
500	18	164	15	0	
507	18	164	16	0	
508	18	164	17	0	
509	18	164	18	0	
548	18	164	19	0	
543	18	164	20	0	
544	18	164	21	0	
545	18	164	the second se		
546	18	164	23	620	
547	18	164			
586	18	164	26		· · · · · · · · · · · · · · · · · · ·
587	18	164	27	O	
584	18	164			
583	18	164	29		
588	18	164		· · · · · · · · · · · · · · · · · · ·	
624		164	31	0	· · · · · · · · · · · · · · · · · · ·
625	18	164	32		
626	18	164	33		
629	18	164	34	* 0	
663	18				

Table B-2

### Grid cells within or touched by each Theissen polygon Wind station number = Theissen polygon number

Record d# wind sta	lon mumber le		<b>STICK WACT</b>	area (acres) i total vac	ant area (acres)
660	18	175	5	0	
659	18	175	6	0	· · · · · · · · · · · · · · · · · · ·
701	18	175	7	0	
700	18	175	8	0	
745	18	175	18	0	14,057

Total area, including duplicate sections

183,345

183,345

Duplicate grid cells in each Theissen polygon (wind station) - based on study area# assigned to more than one Table B-3 Theissen polygon (wind station)

Resident and a second state of the second state of		12(0)(6)/6	CEOPOLS	A CHEMICILC SHOP (SP)	fotal du plicate area	comection
1	226	139	22	67		
1	227	139	21	149		a- , , , , , , , , , , , , , , , , , , ,
1	248	139	26	23	······································	
1	250		27	63	· · · · · · · · · · · · · · · · · · ·	
1	251	139	28	59		
1	272		35	25		
1	274		34	58	······································	
1	275	139	33	191	635	31
2	195		14	350	035	31
2	195			284		
2						
	219		21	110		
2	220		22	87		
2	221	140	20	193	······································	
2	246		29	81		
2	270	140	32	22	· · · · · · · · · · · · · · · · · · ·	
2	297	161	3	135		
2	298		2	258		
2	300	161	5	44		
2	328	161	10	169		
2	329	161	9	45		
2	330	161	8	68	1846	92
3	184	139	8	206		
3	186		7	275	10-16-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-	
3	204	139	17	520		
3	205	139	18	369		
3	200	139	21	149		
3	228	139	20	198		
3	220	139	19	109		
3	232	139		109		
3				59	······································	
	251	139			······································	
3	274		34	58		
3	275	139		191		
3	278	138		8		
3	304	162	3	5		
3	308			33		
3	334		10	34		
3	335	162	8	8		
3	336	162	9	76		
3	337	162	7	11		
3	338	163	12	65	2390	119
4	13			315		
4	37	124		645		
4	62	124		647		
4	84	124				
4	86	124		632		
4	106	124		471		
	106	124		239		
4						
4	154	139		206		
4	155 160	139 139		529		
4		120	5	240		

### Duplicate grid cells in each Theissen polygon (wind station) - based on study area# assigned to more than one Theissen polygon (wind station) Table B-3

STRONTIN			Najar San Statist	1000	STUDIARESUMMEND	
NULTION IN	New apparenties in	170 and 1	<u>SEG Rent</u> 11	139		
·		397		139	177 178	4
			10			4
· <u></u>		350	14	140	195	4
		284	15	140	196	4
	·····	322	17	140	198	4
		214	18	140	199	4
		78	13	139	200	4
		110	21	140	219	4
		87	22	140	220	4
355	7102	193	20	140	221	4
	,	334	9	179	503	5
		121	8	179	504	5
		486	12	178	505	5
		460	7	179	506	5
		446	11	178	507	5
		284	14	178	537	5
<u></u>		339	15	178	538	5
		502	22	178	568	5
		623	27	178	598	5
		636				
			33	178	629	5
		595	8	190	678	5
		287	17	190	696	5
257	5148	35		190	716	5
		81	29	140	246	6
		22	32	140	270	6
		56	31	140	271	6
		44	5	161	300	6
		6	6	161	301	6
		37	1	162	302	6
		68	8	161	330	6
<u> </u>		16	12	162	332	6
		34	17	161	360	6
		74	13	162	362	6
		11	20	161	390	6
- <u></u>		39				6
		51	24	162	392	
				161	420	6
		36	30	161	421	6
30	601	26		162	424	6
·		81		140	246	7
		60		140	247	7
		22		140	270	7
		56		140	271	7
		50	36	139	273	7
		6	6	161	301	7
		37		162	302	7
- <u>-</u>		11		162	303	7
17	339	16	- 12	162	332	7
		135		161	297	8
		258	2	161	297	8
		169		161	328	8
		45		161	328	8

Duplicate grid cells in each Theissen polygon (wind station) - based on study area# assigned to more than one Table B-3 Theissen polygon (wind station)

	Makes Humples			Vacant area (acres)	n (cher a du pliner (cher no en	CONCECTION
8	330	161	8	68		
8	360	161	17	34		
8	390	161	20	11		
8	416	161	25	493		
8	417	161	26	440		
8	418	161	27	287		
8	419	161	28	141		
8	420	161	29	51		
8	421	161	30	36	2168	108
9	334	162	10	34	2.00	
9	335	162	8		,	
9	336	162		76		
9	330	162		11		
9	338	163		65		
				74	·····	
9	362	162				
9	363	162	1	8		
9	364	162	15	86		
9	368	163		39		
9	392	162	24	39		
9	396	162	19	97		
9	398	163		97	······	
9	424	162	25	26		
9	427	162	30	133		
9	450	162	36	125		
9	453	162	35	358		
9	456	162	31	452		
9	483	177	2	169		
9	486	177	6	360		
9	509	177	11	123	·	
9	513	177	10	163	······································	
9	516	177	7	456		
9	543	177	15	87		
9	545	177	16	273		<u>, , , , , , , , , , , , , , , , , , , </u>
9	546	177	18	549		
9	575	177		276		
9	577	177			· · · · · · · · · · · · · · · · · · ·	
9	605	177	29			
9	606	177				
9	607	177	30			
9	636	177	32		7400	074
9	637	177	31	637	7483	374
10	416	161				
10	417	161	26			
10	418	161		287		
10	447	161		208		
10	477	178				
10	503	179				
10	504	179				
10	505	178				
10	506	179		460		
10	507	178	11	446	3561	178

Duplicate grid cells in each Theissen polygon (wind station) - based on study area# assigned to more than one station)

	Table B-	3	Theiss	en polygon	(wind a
8. Th	in selional	STUDYAREAM (Unicue)	BOOK	SECTION	Maidan
	11	154	139	3	
	11	155	139	4	
	4.4	400	400	E	

ite area correction	single in the logic and	Vacani alea (acres)	SECTION	হিত্তি[র্ম	STUDYAR HAR ONION	Vindistations
		206	3	139	154	11
	· · · · · · · · · · · · · · · · · · ·	529	4	139	155	11
		240	5	139	160	11
		327	12	139	176	11
		170	11	139	177	11
		397	10	139	178	11
		206	8	139	184	11
		275	7	139	186	11
		322	17	140	198	11
		214	18	140	199	11
,		78	13	139	200	11
		520	17	139	204	11
		110	21	140	219	11
		193	20	140	221	11
		67	22	139	226	11
		149	21	139	227	11
		198	20	139	228	11
		81	29	140	246	11
		60	30	140	247	11
		23	26	139	248	11
		71	25	139	249	11
4499 225	44	63	27	139	250	11
		65	12	163	338	12
		71	11	163	339	12
		117	10	163	340	12
		3	7	163	341	12
		15	8	163	342	12
		250	9	163	343	12
		39	13	163	368	12
		192	18	163	374	12
		615	13	164	376	12
		97	19	162	396	12
		97		163	398	12
		561	24	164	404	12
				164	408	12
<u></u>				162	427	12
				164	437	12
		452		162	456	12
		360	6	177	486	12
		456	7	177	516	12
			18	177	546	12
			19	177	577	12
			30	177	607	12
		637	31	177	637	12
7812 390		633	6	191	667	12
		87		138	230	13
		42		138	230	13
			23	138	231	13
<u> </u>		47	24	138	232	13
		47	21	138	233	13
	1					

Duplicate grid cells in each Theissen polygon (wind station) - based on study area# assigned to more than one Table B-3 Theissen polygon (wind station)

irrection	tal duplicate alea. Go		e zomori	3.00	Subby/Action Coulder)	und stational
		68	30	138	260	13
	· · · · · · · · · · · · · · · · · · ·	8	36	138	278	13
		169	31	138	284	13
<del></del>		33	1	163	308	13
	·····	45	5	163	312	13
	· · · · · · · · · · · · · · · · · · ·	52	6	163	313	13
		65	12	163	338	13
		71	11	163	339	13
	· · · · · · · · · · · · · · · · · · ·	117	10	163	340	13
•••••	······································	3	7	163	341	13
	A	15	8	163	342	13
655	1309	250	9	163	343	13
		287	27	161	418	14
		141	28	161	419	14
·······		51	29	161	420	14
	······	36	30	161	421	14
		26	25	162	424	14
		208	35	161	447	14
·····		125	36	162	450	14
		358	35	162	453	14
		286	2	178	433	14
<del></del>		169	2	177	483	14
		446	<u>_</u> 11	178	507	14
		123	11	170	507	14
<u> </u>		123	10	177	509	14
		284	10	178	513	14
		339	14	178	538	14
····			15	170	530	14
		273			545	14
		502	16	177	568	14
			22	178		14
		276	21	177	575	
		623	27	178	598	14
<b>.</b>		509	29	177	605	14
<del> </del>		398	28	177	606	14
		636	33	178	629	14
		542	32	177	636	14
		637	31	177	637	14
		633	6	191	667	14
		595	8	190	678	14
		287	17	190	696	14
4538	9075	35	20	190	716	14
		25	35	139	272	15
		58	34	139	274	15
		37	1	162	302	15
		11	2	162	303	15
		5	3	162	304	15

## Duplicate grid cells in each Theissen polygon (wind station) - based on study area# assigned to more than one Table B-3

						Saulas A El Externation de la	
			16	12	162	332	15
			34	10	162	334	15
		·[	74	13	162	362	15
			8	14	162	363	15
17	354		86	15	162	364	15
			81	29	140	246	16
			60	30	140	247	16
			23	26	139	248	16
			71	25	139	249	16
			56	31	140	271	16
		1	25	35	139	272	16
<u> </u>			50	36	139	273	16
			37		162	302	16
	414			1			
20	414		11	2	162	303	16
			315	6	124	13	17
			645	7	124	37	17
			647	18	124	62	17
			646	20	124	84	17
			632	19	124	86	17
			471	29	124	106	17
		)	239	32	124	134	17
		)	240	5	139	160	17
			206	8	139	184	17
			275	7	139	186	17
			529	12	137	188	17
<u> </u>			369	18	139	205	17
<del>_</del>			5	18	138	203	17
			51	13	137	211	17
			109				
				19	139	229	17
			87	22	138	230	17
			42	23	138	231	17
			16	24	138	232	17
			47	21	138	233	17
			46	20	138	234	17
285	5713	5	96	19	138	235	17
		9	529	12	137	188	18
		5	5	18	138	211	18
		1	51	13	137	212	18
		3	46	20	138	234	18
		3	96	19	138	235	18
			175	29	138	258	18
			68	30	138	260	18
			169	31	138	284	18
<u></u>			45	5	163	312	18
				6	163	312	18
<del>-</del>							
				7	163	341	18
			192	18	163	374	18
			615	13	164	376	18
			561	24	164	404	18
			620 637	23 26	164	408 437	18
193	3864				164		18

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# Field sampling summary

	General comments	rieid sampling summary
	Following the proposed Clark County rule section 41.7.2.2. the	the
	Ball drop -> % nonerodible -> TFV test sequence is heirarchical	chical.
	A 999 code indicates that a test was not needed and not performed	erformed
	because of an earlier result in the heirarchy.	
	In some cases, the tests were performed even when not needed	seded.
Ball dron	If Ball drop = pass (P). then a visible crust is present: the site is stable (0) and %non-erodible. TFV	te is stable (0) and %non-erodible. TFV
_	_	
Flat veg	If Ball drop = fail (F), then do count of % flat vegetation & non-erodible elements, per section 41.9.5	on-erodible elements, per section 41.9.5
	page 41-15. This method counts both flat vegetation and other non-erodible elements	ther non-erodible elements
	If % flat + non-erodible > 50% then site is stable, and TFV test is not	V test is not
	usually performed	
	If 0% non-ecodible <= 50% then do TEV test by signing to datermine	, determine
	mode of soil particle size distribution & compute TFV in cm/sec	comisec
TFV	The TFV test is carried out per section 41.9.4.1, pp 41-12 and 41-13,	and 41-13,
	If sieve analysis test shows TFV > 100 cm/sec, then site is stable	stable
	If sieve analysis test shows TFV <= 100 cm/sec, then	
	run Rock Test	
Dock Tant		
KOCK I ESI	KOCK LESS ROCK LESS METHOD	F
	The method used by UNLV does not conform to 41.9.7 Rock Test	ock lest
	Method in proposed Clark County rule 41. UNLV attempted to	jd to
	develop a faster, more quantitative procedure than 41.9.7	
	UNLV sampled all rocks to depth of 1 cm from a random cast	ast
	of the 1 square foot quadrat	
	Rocks were poured into a 1 cm sieve, and rocks not passing	D
	1 cm sieve were poured into a cake pan, and shaken into	
	a single layer in one corner to determine areal coverage of	
	rock elements. Dimensions of rock layer were measured with	Ith
	a ruler, and the area calculated, then divided by two to compute	Ipute
	frontal area of the rocks. The frontal area was then divided by the area sampled	by the area sampled
	by the dust pan (generally 1 square foot) to get the % area	
	II % FOCK ITONIAL AFEA EXCEEDS 10% LITER SIGNE.	
adjust TFV	adjust TFV if rock frontal area is less than 10%, then adjust TFV using	
	the percent frontal area result per 41.9.4.1 Table 2	
	If adjusted IFV > 100 cm/sec, stells stable	
	IT adjusted IFV < 100 cm/sec, stels unstable	

] ■ ] Table B-4

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Field sampling summary

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AND A CONTRACT OF	<b>TOWNSHIP</b>	RANGE	SECHON	ALCONTRACTOR				Attende Rothen Mathematican (en according to the constraint of the bar
Bonanza Rd/Fogg	20 S	62 E	न्न	67,500	4.	9.09	/9/	-
Spanish Dr./Clayton (East End)	20 S	62 E	म्र	186,000	4	31	3	-
Spanish Dr./Clayton (West End)	20 S	62 E	8	225,000		14.5	90	-
Stewart Ave/Fogg	20 S	62 E	ä	41,250	LF.	25.6	76.7	0
Mabel/Fogg (A)	20 S	62 E	ष्ठ	240,625	Ŀ	49.3	8	-
Mabel/Fogg (B)	20 S	62 E	34	68,750	u.	23	8	-
Mabel/Fogg (C)	20 S	62 E	æ	151,250		17.5	53.3	
Mabel/Fogg (D)	20 S	8 8	म्र	89,375	NA	27	666	-
Mabel/Beesley	20 S	82 E	म्र	60,000	L	46.3	8	-
Sunrise Mt. Drive	20 S	62 E	¥	250,000	P	23	666	0
Havenwood/Town Center Dr.(SW)	21 S	29 E	12		u.	86	<b>666</b>	0
Havenwood Development (cons)	21 S	29 E	12		A/A	76	666	0
Town Critr btwn. Havenwood Desert Primrose Ln	21 S	29 E	12			55.5	666	0
Havenwood/Town Center Dr. (SE)	215	ш 20 25	12		L	78.5	666	0
Mcl and McConn	21.5	61 E	25		d	666	666	0
McConcil-Jarrison	21.5	ы 1 1 1 1 1 1 1 1	22		4	30.7	116.1	0
Reno/Harrison	215	64 E	22		. 14	40	117.9	0
Most of Only off of Dussed	24 0	л п 1 п	2 4		. 11	23	666	C
West of Oak off of Kussell	210	ы 11 Ц 10 Ц	3 2		_ 11	16.5	36	
0141111 UN F 8405	010	1 1	36	000 026	- u	202	150	
HD/HOST KG.	213	ц н Б	20	200,000		44.0	88	
Russell Rd./Polans	S 12	ים 10	8	000'071'1	<b>.</b>	8 8	222	
West Sunset/Polaris	21 S	61 E	32	174,000	<b>a</b> .	666	666	<b>.</b>
West Sunset/Crystal*	21 S	<u>6</u> Ш	32	195,000	NA	666	666	RN
Russell Rd btwn. I-15 and LV Blvd	21 S	61 E	33	6,600,000	N/A	666	666	NR
West Sunset btwn. LV Blvd and Windv Rd.	21 S	61 E	32	350,000	NA	666	<b>8</b> 86	N/R
Post/Crvstal	21 S	61 E	32	195,000	a.	666	666	0
Las Vegas Blvd Marm Springs Rd.	22 S	61 E	ø	8.820.000	Ľ.	55.5	666	0
Bine Diamond Rollindristrial	225	61 E	80	750.000	L	51.3	666	•
Valley View/Fidorado	202	9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 00	445 500	. 11	49.5	<b>6</b> 86	0
Windmill V Rhv *	20.5	ы 1 П 1 П	0	2.310.000	N/A	666	666	NNR
Calleria Dr /Discoll Dd	24.0	ы В П	33	285,000	0	666	666	0
Defrick Lationics Dr. (A)	24.0	3 E	3 8	307 500		18.3	117.99	0
	2 1 2	38	38	242 242	. 0	000	000	c
	210	1 U 2 8	38		_ 14	53.5	88	
	613	28	38		-	2.00	E2 E7	
Russell off of US 95 Hwy. (D)	21 S	ц 22 22	38	000'042	L	24	/0.20	
Patrick Ln./Stephanie	21 S	ы 62 г	3	38,003		0.00	555 6	
Pecos/Oquendo	21 S	61 F	8	000,75	<u>ــــــــــــــــــــــــــــــــــــ</u>	8	2000	
McCleod/Harrison	21 S	61 E	g	136,250	٩	666	866	0
McCleod/Post	21 S	61 E	36	265,000	NA	88	<b>666</b>	666
Patrick Ln./Oquendo	21 S	61 E	36	877,500	¢.	666	<b>666</b>	0
Patrick Ln off of Eastern	21 S	61 E	36	384,688	۵.	666	666	0
Walnut/Craig Rd. (1)	20 S	61 E	-		۵.	999	666	0
Washburn/Pecos	20 S	61 E	-		٩	666	666	0
Walnut/Craio Rd. (2)	20.5	61 E	+-		Q.	666	666	0
Crain Rd/Statz	20.5	61 E	+		٩	666	666	0
i ske Mosed Mohave (South   of)	22 5	14	ſ		LL.	76	666	0
I ake Mead/Muhave (North I of)	22.5	8	S.		٤.	74	<b>666</b>	0
Decahir/Rethwav(1)	215	61 E	3		C.	666	666	0
Decentre/Baltway (2)	21S	61 E	31		٩	666	666	0
Poceturi/Summed (A)	21.5	Я Е	31	709 938	a	666	666	0
Docetur/Sunset (A)	215	ы 1 1 1 1	3 6	2001001	. 0	666	666	0
Devaul/Outrade (D)	24 5	а 1 п	3	338.000	. Ш	535	666	0
Aviila/Sunset (A)	215	ы 1 1 1 1 1 1	3	222	. a	666	666	0
		11	5				0000	
			•	-			222	2

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Ĩ	Table B-4			Fleid sampl	Field sampiing summary			
過三5,2,3,3,5	Network	TOWNSHIP (		INCINUMERS (		Kaon Montes In the Branch Street	<b>JEV(GNS)</b> A	one with the second states and the second se
124	Decatur/Ranch House	19 S	61 E	8	٩.	666	<b>86</b> 6	0
124	Decatur/Centennial Pkwy	19 S	61 E	8	N/A	55.7	666	o
124	Willus/Ranch House	19 S	61 E	8	a.	666	666	0
124	Willus/Ranch House (C)	19 S	61 E	ଚ୍ଚ	N/A	53.3	<b>666</b>	0
125	Grand Canyon/Bath (A)	19 S	90 Ш	19	٩.	102	666	0
138	Fort Apache/Lone Mountain	20 S	ш 09 Ш	5	e.	84	886	0
138	Bonita Vista/Stange	20 S	90 E	2	٩	20	886	0
140	Cheyenne/Lamb	20 S	62 E	17	٩	666	666	0
140	Alto/Nellis	20 S	62 E	17	۵.	666	<b>666</b>	0
140	Lamont/Carey	20 S	62 E	17	<b>e</b>	666	<b>666</b>	0
140	Lamb/Carey	20 S	62 E	17	٩.	666	<b>666</b>	0
139	Lone Mountain/Clayton	20 S	61 E	S	٩	666	666	0
139	Craig/Ruselier	20 S	61 E	ŝ	٩	666	886	0
139	Simmons/Lone Mountain	20 S	61 E	5	P	666	666	0

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Field sampling summary

BOOK #		Herren Vectorian (%) AVSUALE ( <del>vest</del> i (nomu)) E 7	Notes and the second
₽!		0.1	
140	Spanish Dr./Clayton (East End)	5.7	
4	Spanish Dr./Clayton (West End)	5.7	
140	Stewart Ave/Fogg	5.7	
140	Mabel/Fogg (A)	5.7	
140	Mabel/Fogg (B)	5.7	
140	Mabel/Fogg (C)	5.7	
<b>1</b> 40	Mabel/Fogg (D)	5.7	N/A = ball drop test difficult to interpret
140	Mabel/Beesley	5.7	
140	Sunrise Mt. Drive	5.7	
164	Havenwood/Town Center Dr.(SW)	1.1	
164	Havenwood Development (cons)	1.1	N/A = ball drop test difficult to interpret
164	Town Cntr btwn. Havenwood Desert Primrose Ln	1.1	
164	Havenwood/Town Center Dr. (SE)	1.1	
162	McLeodMcCong	23.8	
162	McCong/Harrison	23.8	
162	Reno/Harrison	23.8	
162	West of Oak off of Russell	23.8	
162	Shamrock/Pecos	23.8	
162	1-15/Post Rd.	3.4	
162	Russell Rd /Polaris	3.4	
162	West Sunset/Polaris	3.4	Completely Bladed/Active Construction
162	West Sunset/Crystal*	3.4 0	
162	Russell Rd btwn. I-15 and LV Blvd	3.4	Active Construction/Completely Bladed/No Access/Area Approximated
162	West Sunset btwn. LV Blvd and Windy Rd.	0 666	Area approximated/Gravel Lot/Visual Pass
<u>5</u>	Post/Crystal	3.4	
177	Las Vegas Blvd. Warm Springs Rd.		Small portion of Area Sampled/Total Area Uniform
177	Blue Diamond Rd/Industrial		
171	Valley View/Eldorado		Small Area Sampled/Total Area Uniform
177	Windmil/LV Blvd *	0	Total Area Uniform/Visual Pass
161	Galleria Dr./Russell Rd	5.6	Small Area Sampled/Total Area Uniform
161	Patrick Ln/Galleria Dr. (A)	5.6	Dumping found in small areas
161	Patrick Ln/Galleria Dr. (B)	5.6	
161	Russell off of US 95 Hwy. (C)	5.6	
161	Russell off of US 95 Hwy. (D)	5.6	
161	Patrick Ln./Stephanie	5.6	Large portion of area covered by dumping
162	Pecos/Oquendo	16.2	
162	McCleod/Harrison	16.2	Active dumping taking place in small section of area
162	McCleod/Post	16.2 0	Highly vegetative area-visual pass
162	Patrick Ln./Oquendo	16.2	
162	Patrick Ln off of Eastern	16.2	
139	Walnut/Craig Rd. (1)		
139	Washburn/Pecos		
139	Walnut/Craig Rd. (2)		
139	Craig Rd/Statz		
170	Lake Mead/Mohave (South Lot)		
170	Lake Mead/Mohave (North Lot)		
3	Decatur/Beitway(1)	28.9	

Table B-4

## Field sampling summary

LOCATION PHOTO VEG COVEL (%) VISUAL (yeset; no=0)					8) 28.9	Park		House	nial Pkwy	Ouse	ouse (C)	Bath (A)	ne Mountain						Clayton		Mountain
	Decatur/Beltway (2)	Decatur/Sunset (A)	Decatur/Sunset (B)	Arville/Sunset (A)	Arville/Sunset (B)	Hinson/Industrial Park	Willus/Ann	Decatur/Ranch House	Decatur/Centennial Pkwy	Willus/Ranch House	Willus/Ranch House (C)	Grand Canyon/Bath (A)	Fort Apache/Lone Mountain	Bonita Vista/Stange	Cheyenne/Lamb	AltoNellis	Lamont/Carey	Lamb/Carey	Lone Mountain/Clayton	Craig/Ruselier	Simmons/Lone Mountain
BOOK HE	162	162	162	162	162	162	124	124	124	124	124	125	138	138		140	140	140	139	139	139

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Table	B-5
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aercent coverage			orthophotos ex township S	
3.	33	61	20	139
1.	34	61	20	139
1.	33	62	20	140
5.	34	62	20	140
1.	35	62	20	140
9.	33	63	20	140
	10	62	21	100
41.	16	62	21	161
26.	23	62	21	161
39.	23	62	21	161
<u></u>	20	62	21	161
<u> </u>				
	31	62	21	161
<u> </u>	32	62	21	161
5.	33	62	21	161
4.	34	62	21	161
9.	35	62	21	161
30.	36	62	21	161
10.	3	61	21	162
21.	7	61	21	162
9.	8	61	21	162
51.	10	61	21	162
5.	15	61	21	162
7.	21	61	21	162
12.	23	61	21	162
23.	25	61	21	162
7.	26	61	21	162
5.	27	61	21	162
17.	29	61	21	162
4.	30	61	21	162
28.	31	61	21	162
3.	32	61	21	162
1.	33	61	21	162
1.	34	61	21	162
1.	35	61	21	162
16.	36	61	21	162
0.		60	21	163
0.		60	21	163
1.		60	21	163
0.		60	21	163
0.		60	21	163
0.		60	21	163
0.		60	21	163
	and the second se	60	21	163
		60	21	163
3.		59		163
<u>3.</u> 1.	12	59	<u>21</u> 21	164
	30			
	10	59	21 22	164
<u> </u>	10	60 60	22	176 176

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Orthophotos examined manually for vegetative coverage										
DOGK STOR	sowing inpage	tentre several	section	percent coversoe water						
176	22	60	27	1.4						
178	22	62	32	0.3						
178	22	62	33	NA						
179	22	63	5	4.3						
179	22	63	6	7.3						
minimum				0.0						
arith mean				9.73						
standard de	ev .			11.78						
maximum				51.20						
geom mea	n - 1 std dev			0.95						
geom mea	n			4.64						
geom mea	n + 1 std dev			22.66						
number of sections exceeding 20% coverage 9										
number of sections analyzed										